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Subsystem: <u>HPOTP B500 - 4750000-700</u>	Prepared by: <u>M.T. Spencer</u>	Issue Date: <u>December 23, 1993</u>
Functional Assy: <u>Pump Section B50001</u>	Approved by: <u>R.L. Pugh</u>	Rev. Date: <u>December 08, 1995</u>
CIL Item: <u>0105</u>		
CIL Item Code: <u>0105</u> FMEA Item Code: <u>0105</u> Function: <u>Direct LOX Coolant</u> System/Subsystem: <u>HPOTP B500 - 4750000-700</u>		Analyst: <u>M.T. Spencer</u> Approved by: <u>R.L. Pugh</u> Rev. No.: _____ Rev. Date: <u>December 08, 1995</u> Effectivity: _____ Hazard Ref.: <u>See Listings Below</u>
Operating Phase	Failure Mode, Description and Effect	Criticality

Operating Phase:
p,s,m,c

Failure Mode:

Loss of coolant flow control.

Failure Cause(s):

- A. In 83 ABO Fracture or plugging of center tube due to vibration, thermal growth, contamination, or material/mfg defect.
- B. In 244 Fracture or wear of the pre-burner impeller damper due to vibration, rub, thermal growth, erosion, contamination, or material/mfg defect.
- C. In 28 Plugging of the pre-burner impeller cooling passages due to contamination, or FOD.

Failure Effect:

Loss or contamination of cooling flow could result in brg failure with rotor shift/rub leading to fire.

System:

Uncontained engine damage

Mission/Vehicle:

Loss of vehicle

Redundancy Screens:

Does not apply since it is a single point failure

Criticality:

1

Hazard Ref:

- A) C1S/A/M/C (AT)
1A1.1.8.2.1.1.2.8
- B) C1S/A/M/C (AT)
1A1.1.8.2.1.1.2.8
- C) C1S/A/M/C (AT)
1A1.1.8.2.1.1.2.8

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Part Name/No.	Design Considerations	Document Ref
<p>/In 93 Center tube</p>	<p>FAILURE CAUSE A. The bore tube Assy serves as a transfer tube to direct cooling flow to the turbine end prior to start for roller brg inner race control to prevent coring. LOX enters the center of the bore tube through holes in the shaft inboard of the turbine side inducer. The turbine side end face of this inducer is slotted to allow flow to enter the shaft. The LOX flows down the center of the bore tube to the turbine end, reverses direction, and then flows along the outside of the bore tube and the inside of the shaft. The coolant is then routed back into the bore tube end exits to the LOX drain.</p> <p>The bore tube is threaded into the shaft at the pump end and retained with a lock. Two equally spaced lugs on the lock fit into both shaft and bore tube slots preventing relative rotation. This spring lock allows ball bearing coolant to flow with minimal restriction. MP35N material was used for the spring lock for it's high strength to modulus ratio.</p> <p>Once start is accomplished, most of the tube flow will cease.</p> <p>All brazed joints are gold-nickel (PWA-SP 19) alloy, and tube fittings are Haynes 214 (PWA-SP 1130) nickel alloy for high resistance to ignition. Use of this alloy should significantly reduce the concern for ferrous metal being introduced into the LOX environment. Flub rings of KEL-F 81 are used as compliant seals which also provide damping to prevent any high frequency fretting.</p> <p>Mission life for the tube is greater than 1000 cycles.</p> <p>Vibration analysis is documented in FR-20730-2 & 4.</p> <p>This part meets CEI requirements.</p>	
<p>/In 244-02 Preburner damper</p>	<p>FAILURE CAUSE B. The hydrodynamic damper provides stable rotor dynamics. Flow control is enhanced by the use of a roughened stator. The damper surface is machined to have a convergent taper between the damper and rotor land. The seal is mated to the bearing support with 6 bolts and tight fitting dowel pins and a radial snap fit which all combine to stiffen both parts and reduce deflections. The pins (/In 246) are AMS 5844 material for it's high strength.</p> <p>Seal material used is Nickel 200 (PWA-SP 6000) with silver plate (AMS 2410) for LOX compatibility.</p> <p>The mission life is greater than 1000 cycles.</p>	
<p>/In 29 Preburner Impeller</p>	<p>FAILURE CAUSE C. The Preburner Impeller is splined to the shaft, and provides the mating surfaces for the various seals, damper, and mounting of the pump and ball bearing (PEBB).</p> <p>Machined passages in the impeller hub provide cooling flow to the cavity formed between the impeller and the rod (/In 35), and from here is transferred to the pump and ball bearing inner race. Cooling flow is enhanced by the downstream 2 tooth K.E. seal (/In 20), and the abradable seal land brazed to the support (/In 244-03).</p> <p>Material is Inconel 718, which is PWA-SP 1146, and has a proven history in a LOX environment (LOX testing of this material appears in Appendix 52 of the P&W MCL Manual). The heat treatment, microstructure and chemistry all enhance operation at cryogenic temperatures.</p> <p>Mission life for the P/B Impeller is greater than 1000 cycles.</p> <p>This part meets CEI requirements.</p> <p>This part is manufactured using chemical milling (PWA-SP 108), and finishing ECMR (87-5) processes.</p>	

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DVS testing number 4.1.4.1.3.1 thru .3 require spin, burst, and resonance testing. As of 04/91, resonance testing (FR 20730-10), and spin and burst tests (FR 20729-40) have been completed.

DVS item 4.1.2.9 for structural design analysis has been completed, and can be found in FR-20729-5, and FR-20730-2, and 10.

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Inspection and Test			
Possible Causes	Significant Characteristics	Inspection and Test	Document Ref
Failure Cause A f/n 83 Center tube	Material Integrity	Material integrity is verified per specification requirements. Contamination control is verified per specification.	AMS 5581, PWA-SP 1130 PWA-SP 38180-4
	Plating Integrity	Plating integrity is verified per specification.	AMS 2403
	Braze Integrity	Braze integrity is verified per specification and drawing requirements. Filler material per AMS 4787 anywhere except turbine end (heat exchanger) Filler material per AMS 4788 anywhere	PWA-SP 18 AMS 4787 AMS 4788
	INSPECTION		
Failure Cause B f/n 244-02 P/B damper	Finished Material	FPI - Items 04, 07, & 08 per QAD FPI - Items 03, 05, & 06 per QAD X-ray per QAD Leak test is verified per print requirements.	SP-FPM Master SP-FPM Master SP-XRM Master
	Assembly Integrity	Cleanliness of components verified per specification.	PWA-SP 80
	Material Integrity	Material integrity is verified per specification Contamination control is verified per specification.	PWA-SP 6000, PWA-SP 1105 PWA-SP 38180-4
	Heat Treat	Heat treating is verified per specification, -02, and -03.	PWA-SP 11-32, PWA-SP 1146
	Plating Integrity	Silver plating is verified per specification, items -02, and -03 Chrome plating is verified per specification, item -03. Plating of f/n 244 is verified per specification	AMS 2410 AMS 2408 PWA-SP 11
	Braze Integrity	Braze integrity is verified per specification, items -02, and -03.	PWA-SP 18
	INSPECTION	I.D. of the pump end ball brg seal end is verified per drawing. The surface profile of the damper and support set (244) and support assembly (-03) is verified per drawing requirements. The I.D. and O.D. of the -03 support is verified per drawing requirements.	

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Failure Cause C
 1/n 2B
 P/B Impeller

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Raw Material	Sonic - Support -02, and -03 per QAD	
Finished Material	FPI - Support assembly item -02, and 244, per QAD FPI - Support -02, and 03 per QAD Sonic - Ring and support assembly-02 only per QAD X-ray - Support assembly item -03 per QAD FPI - Damper & support set, 244, ring & support assy, 244-02, per QAD	SP-FPM Master SP-FPM Master SP-XRM Master SP-FPM Master
Assembly Integrity	Cleanliness of components is verified per specification.	PWA-SP 80
Material Integrity	Material Integrity is verified per specification. Chem milling ECMR Contamination control	PWA-SP 1146 PWA-SP 108 PWA-SP 87-5 PWA-SP 36180-4
INSPECTION		
Raw Material	Sonic - at the detail level per QAD	
Finished Material	FPI - Detail level per QAD FPI - Assembly level per QAD ECI - Detail level per QAD Blade thickness is verified per drawing requirements. Impeller O.D. PEBB seating diameter is verified per drawing requirements. Spine requirements are verified per drawing requirements.	SP-FPM Master SP-FPM Master SP-ECM Master
Assembly Integrity	Vacuum dry, check axial travel, and GN2 purge. Cleanliness of components is verified per specification. Vibration controlled by assembly balance. Balance weights are stated per specification.	REI 013 PWA-SP 80 REI 013 PWA-SP 361
	Tiebolt installed, torqued, and locked to the limits specified in the Table of Limits to ensure joint integrity.	REI 013
Supporting hardware D105c 1/n 02D Seal	Material Integrity	Material integrity is verified per specification
INSPECTION		
Raw Material	Sonic per QAD	

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Final Inspection

Seal diameter is verified per drawing requirements.

All Cause

General Quality Requirements:

Supplier Quality Assurance requirements are included in PW-QA-8076, and include such requirements as first piece layouts. This requires the documentation of dimensions on all characteristics represented on the delivered article.

PWA-SP 300

Inspection Methods Sheets for use in the inspection of purchased parts and assemblies contain the necessary information to insure that the requirements of the QADs, engineering drawings, and referenced documents are satisfied. For shop fabricated parts, the sheets are supplied by Inspection Methods.

The purchase orders for vendor supplied parts must comply with PWA-SP 300, 'Control of Materials Processes and Parts', which requires the vendor to provide material, process, and dimensional information to the Quality Department.

Acceptance

Acceptance test will be conducted as required by contract, to demonstrate specified performance.

DFI SE-13

Waivers

This section would contain a description of any limiting features of CIL hardware
Not applicable at this time

DAR Numbers

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