CIL

EMU CRITICAL ITEMS LIST

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NAME P/N QTY CRIT SIZING RING ITEM 1/1 103 (1) LEFT (1) RIGHT 	103FM10U	FAILURE EFFECT END ITEM: Suit gas leakage to ambient. GFE INTERFACE: Depletion of primary 02 supply and SOP. Rapid depressurizatio	anodize. A static in a groove and is of two spring load are made of 7075-T of stainless steel	made of 70 lip seal pr made of a p led sequentia 73 Aluminum . The threa	rovided for pressure retention. The seal is seat polyurethane compound. The locking system consis al locks and one manual lock. The locking latche Alloy and the spring and retaining screws are ma
QTY CRIT SIZING RING ITEM 1/1 103 (1) LEFT (1) RIGHT 10146-05	T CAUSES 103FM10U External leakage beyond SOP make-up capability. Contamination wear or deterioration of lip seal. Defective material;	END ITEM: Suit gas leakage to ambient. GFE INTERFACE: Depletion of primary O2 supply and SOP. Rapid	A. Design - The sizing ring is anodize. A static in a groove and is of two spring load are made of 7075-T of stainless steel "one way" initiati	made of 70 lip seal pr made of a p led sequentia 73 Aluminum . The threa	rovided for pressure retention. The seal is seat polyurethane compound. The locking system consis al locks and one manual lock. The locking latche Alloy and the spring and retaining screws are ma
03 (1) LEFT 1) RIGHT 0146-05	External leakage beyond SOP make-up capability. Contamination wear or deterioration of lip seal. Defective material;	Suit gas leakage to ambient. GFE INTERFACE: Depletion of primary O2 supply and SOP. Rapid	The sizing ring is anodize. A static in a groove and is of two spring load are made of 7075-T of stainless steel "one way" initiati	: lip seal p made of a p led sequentia 73 Aluminum The threa	rovided for pressure retention. The seal is seat polyurethane compound. The locking system consis al locks and one manual lock. The locking latche Alloy and the spring and retaining screws are ma
03 (1) LEFT 1) RIGHT 0146-05	<pre>leakage beyond SOP make-up capability. Contamination wear or deterioration of lip seal. Defective material;</pre>	Suit gas leakage to ambient. GFE INTERFACE: Depletion of primary O2 supply and SOP. Rapid	The sizing ring is anodize. A static in a groove and is of two spring load are made of 7075-T of stainless steel "one way" initiati	: lip seal p made of a p led sequentia 73 Aluminum The threa	rovided for pressure retention. The seal is seat polyurethane compound. The locking system consis al locks and one manual lock. The locking latche Alloy and the spring and retaining screws are ma
		depressurizatio	The sizing ring is made of 7075-T73 Aluminum Alloy is finished with Typ anodize. A static lip seal provided for pressure retention. The seal in a groove and is made of a polyurethane compound. The locking system of two spring loaded sequential locks and one manual lock. The locking are made of 7075-T73 Aluminum Alloy and the spring and retaining screws of stainless steel. The threaded portion of the sizing ring is designe "one way" initiation of threaded engagement to ensure proper alignment		
		n of SSA beyond SOP makeup capabilities. MISSION: Loss of EVA.	The sizing ring threads were determined by analysis to have strength of 3224 lbs and a yield strength of 2718 lbs. At 4 operating pressure) the S/AD limit load is 438 lbs., giving safety factor of 7.4 for ultimate and 6.2 for yield. At 5.5 pressure) and 8.8 psid (max BTA operating pressure) the sizi safety factors for ultmate of 7.9 and 10.2 respectively. Th safety factor for hardware at 4.4 psid is 2.0 for ultimate a At both 5.5 psid and 8.8 psid the S/AD minimum safety factor for ultimate.	eld strength of 2718 lbs. At 4.4 psid (normal limit load is 438 lbs., giving the sizing ring a mate and 6.2 for yield. At 5.5 psid (max failure TA operating pressure) the sizing ring provides 7.9 and 10.2 respectively. The S/AD minimum 4.4 psid is 2.0 for ultimate and 1.5 for yield.	
		CREW/VEHICLE: Loss of crewman.	Normal rotation loads result in arm bearing rotation which precludes torque induced loads into the sizing rings. The threaded portion of the sizing ring is coated with a dry film lubricant allow smooth travel of the ring when being mated.		
		TIME TO EFFECT /ACTIONS: Seconds.			
		TIME AVAILABLE: N/A	B. Test - Acceptance: The sizing ring is verification.	subjected t	to testing per ATP 10146 at Airlock with ILC sou
		TIME REQUIRED: N/A	<pre>PDA: the following tests are conducted at the Arm Assembly level in accordance of ILC Document 0111-710112: 1. Initial leak test at 4.3 +/-0.1 psig to verify leakage less than 24.0 scc/min. 2. Proof pressure test at 8.0 + 0.2 - 0.0 psig to verify no structural dat Destruction of the second second</pre>		
		REDUNDANCY SCREENS: A-N/A			
		B-N/A C-N/A	24.0 scc/min.		test at 4.3+/-0.1 psig to verify leakage less th -0.1 psig to verify leakage less than 24.0 scc/m
			duplicate 458 hour	s operationationation	lly tested manned during SSA certification to al life (Ref. ILC Report 0111-711330). The equirements of significance to the sizing ring, on:
			Requirement	S/AD	Actual
			Elbow/Cycles Engage/Disengage Don/Doff Pressure Hours	49660 300 98 458	 102000 800 400 916

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NAME P/N QTY	CRIT	FAILURE MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE	

103FM10U

Two acceptable alternate static seals were developed and passed certification testing (Ref. Certification Report 0111-712694). The following usage, reflecting requirements of significance to the seal, were documented during certification:

Requirement	S/AD	Actual		
Engagement Cycles	300	600		
Pressure Hours	458	916		
Pressure Cycles	194 @	4.3 psid 388		
	74 @	5.3 psid 148		
	32 @	6.6 psid 64		

C. Inspection -

Components and material manufactured to ILC requirements at an Approved Supplier are documented from procurement through shipping by the supplier. ILC incoming receiving inspection verifies that the matrials received are as identified in the procurement documents, that no damage has occured during shipment and that supplier certifications have been received which provides traceability information.

The following MIPs are performed during the arm assembly manufacturing process to assure that the failure causes are precluded from the fabricated item:

- 1. Visually inspect static seal for damage.
- 2. Visually inspect ring for scratches and burrs.

During PDA, the following inspection points are performed at the arm assembly level per ILC Document 0111-710112:

- 1. Inspection for cleanliness to VC level.
- 2. Visual inspection for damage, wear or material degradation.
- 3. Visual inspection for damage following proof-pressure test.

D. Failure History -None.

E. Ground Turnaround -Tested for non-EET processing per FEMU-R-001, Arm Pre-Flight Test Requirements, Structural and Leakage Test. None for EET processing. Additionally, every 4 years chronological time or 229 hours of manned pressurized time, the sizing ring is disassembled, cleaned, inspected, lubricated and reassembled.

F. Operational Use -Crew Response -Pre EVA/Post EVA: Trouble shoot problem, Consider use of third EMU. If no success terminate EVA prep. EMU is no go for EVA. EVA: When CWS data confirms SOP activation, abort EVA.

Training - Standard training covers this failure mode.

Operational Consideration -

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		103FM10U		Flight rules define go/no go criteria related to EMU pressure integrity and regulation. EVA checklist procedures verify hardware integrity and systems operational status prior to EVA. Real Time Data System allows ground monitoring of EMU systems.	

EXTRAVEHICULAR MOBILITY UNIT

SYSTEMS SAFETY REVIEW PANEL REVIEW

FOR THE

I-103 ARM ASSEMBLY

CRITICAL ITEM LIST (CIL)

EMU CONTRACT NO. NAS 9-97150

Prepared by: MS - Project Engineering Approved by: MS - Approved by: MS - Approved by: MS - Project Engineering

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