CIL

EMU CRITICAL ITEMS LIST

#### 5/30/2002 SUPERSEDES 12/31/2001

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NAME		FAILURE		
P/N		MODE &		
QʻI'Y	CRIT	CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
	· – – – -	104FM28W		
LEG RESTRAINT AND BLADDER ASSEMBLY ITEM 104 (1) LEFT (1) RIGHT	1/1	External gas leakage beyond SOP make-up capability.	END ITEM: Suit gas leakage to ambient.	A. Design - The leg bladder assembly is formed from a series of patterned pieces of urethane coated nylon oxford fabric, seamed together by dielectric heat, to which flanges are also heat sealed. The bladder seams are reinforced by heat sealed overtaping to enhance structural integrity. The solution coated bladder is
0104-810467-02 (2)		Separation of seam or puncture in bladder. Defective material	GFE INTERFACE: Depletion of primary O2 supply and SOP. Rapid depressurizatio	protected internally in known areas of high wear, by an additional heat sealed abrasion layer. Externally, the bladder is protected by the restraint fabric and TMG layers. The bladder is entirely supported by the leg restraint assembly. The bladder is thereby not subjected to any of the loads (man or pressure induced) experienced by the lower torso restraint.
		abrasion.	n of SSA beyond SOP makeup	Seam design creates a structure at least as strong as the base bladder. Thus, seam separation is precluded.
			capability.	There are two types of bladder fabric. One is constructed of a base nylon fabric with a solution coated urethane. The other is constructed of the same
			Loss of EVA.	
			CREW/VEHICLE: Loss of crewman.	The following paragraph applies to the solution coated hylon. Testing has shown that the bladder fabric minimum tensile strength is 105 lbs/inch (fill) and 140 lbs/inch (warp). The tearing strength is 3.5 lbs/inch in fill and 6.0 lbs/inch in warp. Nominally, hoop load is absorbed by the bias direction of the bladder fabric. However, the safety factors are based on the fabric yarns (fill yarns)
			TIME TO EFFECT /ACTIONS: Seconds.	which have the least strength. Based on a predicted hoop load of 17.2 lbs/inch at 4.4 psid (normal operating pressure), the minimum safety factor for hoop stress is 6.2. At 5.5 psid (max failure pressure) and at 8.8 psid (max BTA operating pressure) the safety factors are 4.9 and 3.0, respectively. The S/AD
			TIME AVAILABLE: N/A	minimum safety factor for softgoods at 4.4 psid is 2.0. At both 5.5 and 8.8 psid, the S/AD minimum safety factor is 1.5. Testing has demonstrated that the breaking strength of the bladder seams meets or exceeds that of the bladder fabric.
			TIME REQUIRED:	
			N/A REDUNDANCY SCREENS: A-N/A B-N/A C-N/A	The following paragraph applies to the laminate coated nylon. Testing has shown that the bladder fabric minimum tensile strength is 180 lbs/inch in the warp direction and 170 lbs/inch in the fill direction. The tearing strength is 3.5 lbs/inch minimum in both directions. Based on a predicted hoop load of 17.2 lbs/inch, the minimum safety factor for hoop stress is 9.8 against a S/AD design minimum ultimate safety factor of 2.0 at 4.4 psid (normal operating pressure). At 5.5 psid (max failure pressure) and at 8.8 psid (max BTA operating pressure) the safety factors are 7.9 and 4.8, respectively. The S/AD minimum safety factor for softgoods at 4.4 psid is 2.0. At both 5.5 and 8.8 psid, the S/AD minimum safety factor is 1.5. Testing has demonstrated that the breaking strength of the bladder fabric
				The presence of shrapion layers, restraint and TMC, slong with the shuri-sal
				properties of the bladder, make inadvertent puncture or abrasion unlikely.
				B. Test - Acceptance: As required by the Table of Operations (T/O) for the fabrication of the bladder assembly, heat seal samples and adhesive seam samples (flange overtape) are
				tensile tested and peel tested, respectively, to verify seam acceptability. Heat seal samples for test are taken at the start of each work shift and immediately

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		104FM28W				
				after each machine change, tool change, machine setting change and/or each material lay-up or material lot change.		
				Heat seam samples are made using production tooling and from the same portion of the roll as the material being heat sealed in production. Peel test samples are produced and tested for each bladder assembly production lot.		
				Following fabrication, each bladder assembly is assembled into a test restraint and subjected to a leakage test at 4.3 psig to verify leakage less than 6.0 scc/min.		
				PDA: The following tests are conducted at the LTA level in accordance with ILC Document 0111-710112: 1. Initial leak test at 4.3 +/- 0.1 psig to verify leakage less than 46.5 scc/min. 2. Proof pressure test at 8.0 + 0.2 - 0.0 psig to verify no structural damage 3. Post-proof pressure leak test at 4.3 +/- 0.1 psig to verify leakage less than 46.5 scc/min. 4. Final leak test at 4.3 +/- 0.1 psig to verify leakage less than 46.5 scc/m		
				When delivered as a separable component of the LTA, the following tests were conducted at the Leg Assembly level in accordance with ILC Document 0111-710112: 1. Initial leakage at 4.3 +/- 0.1 psig to verify leakage less than 6.0 scc/min. 2. Proof pressure test at 8.0 + 0.2 - 0.0 psig to verify no structural damage. 3. Post-proof pressure leak test at 4.3 +/- 0.1 psig to verify leakage less than 6.0 scc/min. 4. Final leakage at 4.3 +/- 0.1 psig to verify leakage less than 6.0 scc/min.		
				Certification: The bladder assembly (solution coated urethane) was successfully tested (manned) during SSA certification testing to duplicate 458 hours operational life (Ref. ILC Report 0111-711330). The following usage, reflecting requirements of significance to the leg assembly, was documented during certification.		
				Requirement S/AD Actual		
				Knee         Cycles         9078         20000           Don/Doff         98         400           Pressure Hours         458         916           Walking Steps         4320         77760		
				The leg restraint and bladder assembly was successfully subjected to an ultimate pressure of 13.2 psid during SSA certification testing (Ref. ILC Document 0111-711330). This is 1.5 times maximum BTA operating pressure based on 8.8 psid.		
				The bladder assembly (laminate coated urethane) was successfully tested (manned) during SSA certification to duplicate 458 hours of operational life (Ref. ILC Report 712436). The following usage, reflecting requirements of significance to the bladder assembly, was documented during certification:		
				Requirement S/AD Actual		

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NAME P/N		FAILURE MODE &				
QTY	CRIT	CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANC	CE	
		104FM28W			·	
				Knee Cycles 9 Don/Doff Pressure Hours Walking Steps 4	078 98 458 320	18,400 205 983 8,640
				The bladder assembly wa psid during SSA certifi 1.5 times the maximum B	s successful cation testi TA operating	ly subjected to an ultimate pressure of 13.2 ng (Ref. ILC Report 0111-712436). This is pressure based on 8.8 psid.
				C. Inspection - Components and material are documented from pro receiving inspection ve the procurement documen supplier certifications information.	d to ILC requirements at an approved supplier ough shipping by the supplier. ILC incoming the materials received are as identified in damage has occurred during shipment and that eceived which provide traceabiltiy	
				<ul> <li>Where applicable, the following MIPs are performed during the LTA manu: process to assure that the failure causes are precluded from the fabric 1. Visual inspection of abrasion layer heat seal for delamination.</li> <li>2. Visual inspection of bladder, before overtaping and flange installe classification of defects criteria.</li> <li>3. Visual inspection of heat seal width.</li> <li>4. Visual inspection of reinforcement tapes and flanges for positioni: bond acceptability.</li> <li>5. Verification of seam acceptability test results.</li> </ul>		
				During PDA, the followi assembly level in accor 1. Visual inspection f 2. Visual inspection f	n points are performed at the lower torso LC Document 0111-710112: degradation. 1 damage following proof pressure test.	
				When delivered as a sep points are conducted at 710112: 1. Visual inspection f	arable compo the leg lev	nent of the LTA, the following inspection el in accordance with ILC Document 0111- degradation.
				D. Failure History - None.	or structura	i damage forfowing proof pressure test.
				E. Ground Turnaround - Tested for non-EET proc for EET processing. Ad manned pressurized time the LTA and subjected t damage.	ditionally, , the leg re o complete v	EMU-R-001, Pre-Flight LTA leakage test. None every 4 years chronological time or 229 hours straint and bladder assembly is removed from isual inspection for material degradation or
				F. Operational Use - Crew Response - EVA: When CWS data conf	irms SOP act	ivation, abort EVA.

Special Training -

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NAME P/N QTY	CRIT	FAILURE MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE		
		104FM28W				
				Standard training covers this failure mode.		
				Operational Consideration - EVA checklist procedures verify hardware integrity and sys status prior to EVA. Flight rules define go/no-go criteri. pressure integrity.	tems operational a related to EMU	

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# EXTRAVEHICULAR MOBILITY UNIT

## SYSTEMS SAFETY REVIEW PANEL REVIEW

FOR THE

I-104 LOWER TORSO ASSEMBLY (LTA)

CRITICAL ITEM LIST (CIL)

EMU CONTRACT NO. NAS 9-97150

Approved by: WASA - SSA/SSMA

M. Snyler HS - Reliability

<u>R. Munford</u> 4/24/02 HS - Engineering Manager

5/2/02 12 N/AS/ACCERT

5.29.02

h 5-30-02

6/04/02 ASAU CTOW

1/3/02 ASAM Program Manager