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EMU CRITICAL ITEMS LIST

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Date: 4/24/2002

IAME		FAILURE		
/N TY	CRIT	MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
		106FM03		
RESTRAINT 4000,	2/1R	Loss of	END ITEM:	A. Design -
TEM 106 (1) LEFT		primary axial	Loss of	4000:
(1) RIGHT		restraint/gimba	primary axial	The glove wrist primary restraints are fabricated from 5/8" wide polyester
0106-88936-11/12 (2)		l support. Defective Material,	load restraining capability.	webbing having a minimum tensile strength of 600 lbs. Front and rear axial restraints are attached to 6.0 ounce dacron fabric reinforcements and 3.0 ounce dacron restraint fabric with bar stitching at each end joined with a double ro of stitching formed from size "E" polyester thread. Side axial restraints are
RESTRAINT PHASE /I, ITEM 106 (1)		Abraded thread or webbing.	GFE INTERFACE: Load will be	attached to the wrist restraint flange seam with size "F" polyester thread. Sewing thread conforming to V-T-285D type II class I is used to fabricate and
JEFT (1) RIGHT		Loss of gimbal swivel screw.	transferred to	attach primary webbings and fabric reinforcements. Lock stitch type 301 per FH
0106-812146-01/02 (2)		Defective gimbal swivel.	secondary restraint/gimba l support.	STD-751A secures fabric reinforcements and front/rear primary webbings. Zig s stitch type 304 attaches the side primary webbings. All stitching is terminat on the restraint exterior with a surgeon's knot which is coated with urethane adhesive. Size 16 needles are utilized for stitching to prevent fabric/webbin
			MISSION:	damage. Front/rear and side axial restraints pulled to destruction during desi
0106-812146-03/04			None with loss of primary	verification testing exhibited minimum ultimate strengths of 315 lbs./430 lbs. and 502 lbs. respectively, demonstrating factors of safety of 2.3/7.4 and 3.1
(2)			restraint/pivot . Terminate	against the respective S/AD limit load of 136.2 lbs., 58.2 lbs., and 162 lbs. min.
			EVA with loss of secondary	Abraded thread and webbing are precluded by design as a function of the abras
			restraint/	protection afforded to the glove restraint by the TMG. Abrasion of the
			secondary	restraint webbing caused by relative motion is reduced by the use of a gimbal
			restraint gimbal support.	swivel to attach the webbings to the gimbal ring. The swivel is coated with a dry film lubricant (Dow Corning 321) to assure free movement.
			CREW/VEHICLE: None with	Loss of a gimbal swivel screw is precluded by adherence to standard engineerin torque requirements for screw installation and the use of thread locking
			single failure. Loss	adhesive. The gimbal swivel is fabricated from 17-4 PH stainless steel heat treated to H1050. Components are subjected to radiographic (casting) and
			of crewman with failure	magnetic particle (machined) to preclude defective material/parts. Tensile testing of the wrist gimbal swivel demonstrated a minimum safety fact
			of secondary restraint/ secondary	of 3.1 without yielding against a S/AD limit load of 162 lbs.
			restraint	Phase VI:
			gimbal support.	The glove wrist design carries the axial loads through the use of a lower primary webbing, a middle primary webbing, an upper primary fabric sheath and
			TIME TO EFFECT /ACTIONS: Minutes.	two gimbal rings. This mode addresses the lower and middle primary webbings which have redundant secondary webbings.
			Milliuces.	The lower primary is fabricated from a 7/8" wide Spectra webbing, one gimbal
			TIME	swivel, Kevlar thread and two stainless steel brackets. The webbing is route
			AVAILABLE:	through the gimbal swivel and overlapped back on itself. The webbing is join with a backtack using 200 denier Keylar thread. The Keylar stitching is cover
			Days.	with a backtack using 200 denier Kevlar thread. The Kevlar stitching is cove with a Teflon fabric abrasion layer. The end of the webbing opposite the swi
			TIME REQUIRED: Hours.	forms a loop through which the lower bracket is passed. The upper bracket th indexes over top the webbing loop centered on the lower bracket. The lower
			REDUNDANCY SCREENS:	primary webbing has minimum tensile strength of 755 lbs demonstrating a minim safety factor of 3.5 against the limit load of 214.5 lbs.
			A-PASS	The middle primary is fabricated from a 5/8" wide polyester webbing, two glov
			B-N/A	gimbal swivels and Kevlar thread. The primary also includes a Teflon abrasio

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NAME P/N QTY		FAILURE MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTAN		
<u></u>						
		106FM03	C-PASS	the middle. The webbir swivels is then covered primary webbing has a m	ng is stitched using a ba d in Teflon fabric for ab	h the swivels and overlapped in artack. The webbing between the brasion resistance. The middle of 490 lbs demonstrating a load of 214.5 lbs.
				protection afforded to restraint webbing cause	the glove restraint by t ed by relative motion is ebbings to the gimbal rin	sign as a function of the abrasion the TMG. Abrasion of the reduced by the use of a gimbal ng. The swivel is coated with
				torque requirements for adhesive. The gimbal s treated to H1050. Comp magnetic particle (mach testing of the wrist gi	r screw installation and swivel is fabricated from conents are subjected to nined) to preclude defect	adherence to standard engineering the use of thread locking in 17-4 PH stainless steel heat radiographic (casting) and tive material/parts. Tensile d minimum safety factor of 2.0 s.
				B. Test -		
				Acceptance: 4000:		
				The glove primary restr during fabrication of e		the S/AD limit load of 162 lbs
				Phase VI: The glove primary restr during fabrication of e		the S/AD limit loads of 214.5 lbs
				ILC Document 0111-70028	3 (4000 glove) or 0111-71	assembly level in accordance with 10112 (Phase VI glove): ig to verify no structural damage.
				of 13.2 psig during SSA times the BTA maximum of Recertification to 5.5	A certification (Ref. Doc operating pressure based psi was by test and anal successfully tested (man	Subjected to an ultimate pressure cument 0111-77511). This is 1.5 on 8.8 psig. Lysis (Ref. ILC EM 84-1108). Ined) during SSA certification to
					eflecting requirements of ited during certification	E significance to the 4000 Glove 1:
				4000: Primary Axial Restraint Requirements S/	AD Actual	
					276 29,484	
				- ,		

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°∕N		FAILURE					
ΤY	CRIT	MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE			
		106FM03					
		10011105		Wrist Rotations 28,216	29,484		
				Finger Cycles 56,550			
				Pressurized Hours 615			
				Pressurized Cycles 376	576		
				Don/Doff Cycles 192	192		
				The following usage reflect restraint was documented du			
				Secondary Axial Restraint			
				Requirements S/AD	Actual		
				Wrist Flex/Ex 4186	16120		
				Wrist Add/Abd 4186	21700		
				Finger Flex/Ext 8372	56420		
				Wrist Rotation 4186	25420		
				Pressure Cycles 32	196		
				Phase VI:		ofully tootod (married)	during
				The glove restraint assemble			
				certification testing to du			
				Report for the Phase VI Glo reflecting requirements of			
				documented during certifica			
				certification while the act			
				restraint in the Hamilton &			
				Requirements	S/AD	Actual	
					S/AD	Actual	
				Glove Joint Cycles			
				Glove Joint Cycles Flex/Ext (fingers)			
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles	45142	39169	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd	 45142 17104	 39169 14830	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext	45142 17104 12646	 39169 14830 10830	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations	45142 17104 12646 20112	 39169 14830 10830 17393	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours	45142 17104 12646 20112 229	 39169 14830 10830 17393 198	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps:	45142 17104 12646 20112 229 ig 97	 39169 14830 10830 17393 198 99	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps:	45142 17104 12646 20112 229 ig 97 ig 37	 39169 14830 10830 17393 198 99 63	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps:	45142 17104 12646 20112 229 ig 97 ig 37	 39169 14830 10830 17393 198 99	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ	45142 17104 12646 20112 229 ig 97 ig 37 ig 16 49 cessfully subj	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ psig during Certification ?	45142 17104 12646 20112 229 ig 97 ig 37 ig 16 49 cessfully sub resting (Ref.	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate ILC doc 0111-712701).	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ psig during Certification T the maximum BTA operating p	45142 17104 12646 20112 229 ig 97 ig 37 ig 16 49 cessfully sub resting (Ref.	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate ILC doc 0111-712701).	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ psig during Certification 5 the maximum BTA operating p C. Inspection -	45142 17104 12646 20112 229 ig 97 ig 37 ig 16 49 cessfully sub resting (Ref.	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate ILC doc 0111-712701).	
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ psig during Certification 7 the maximum BTA operating p C. Inspection - 4000/Phase VI:	45142 17104 12646 20112 229 ig 97 ig 16 49 cessfully sub resting (Ref. pressure based	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate ILC doc 0111-712701). d on 8.8 psig.	This is 1.5 ti
				Glove Joint Cycles Flex/Ext (fingers) Wrist Joint Cycles Add/Abd Flex/Ext Rotations Pressurized Hours Pressurized Cycle @ 4.3 ps: 5.3 ps: 6.6 ps: Don/Doff Cycles The glove assembly was succ psig during Certification 5 the maximum BTA operating p C. Inspection -	45142 17104 12646 20112 229 ig 97 ig 37 ig 16 49 cessfully sub Testing (Ref. pressure based	 39169 14830 10830 17393 198 99 63 18 49 jected to an ultimate ILC doc 0111-712701). d on 8.8 psig.	This is 1.5 ti n approved suppl

are documented from procurement through shipping by the supplier. ILC incoming receiving inspection verifies that the materials received are as identified in the procurement documents, that no damage has occurred during shipment and that supplier certifications have been received which provide traceability information.

CIL EMU CRITICAL ITEMS LIST			5/30/2002 SU	PERSEDES 12/31/2001	Page 4 Date: 4/24/2002
NAME P/N QTY	CRIT	FAILURE MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE	
		106FM03			
				The following MIP's are performed during the glove a process to assure that the failure causes are precis	
				4000/Phase VI: 1. Visual inspection of the thread and webbing upon restraint webbing pull test for signs of defective of 2. Verification of the presence of screws during an torquing of the gimbal swivel screw. 3 (4000 only). Verification of the application of 1 During PDA, the glove is visually inspected for strup proof pressure test per ILC Document 0111-70028 (400 (Phase VI glove).	threads and material. oplication of Loctite and Lubrication to swivels. actural damage following
				D. Failure History - B-EMU-106-A023 (8/21/90) - Screws which attach gimba 4000 series glove not flush with washer surfaces due specification washer countersink angle which allower washer surfaces. Inspection of washer countersink h countersink angle with an angle gauge instead of a s	e to a wider, out-of- d screw heads to extend above hole changed to measure the
				B-EMU-106-A043 (03/01/99) - Remote Powered Heated Glove Assembly (RPHGA) right of did not operate freely. Three of four swivels were galling as a result of lubricant depletion. No corr flight testing per FEMU-R-001 provide for detection procedure dictates inspection after each 56 hours or time). A large margin exists between the maximum to between inspections (63 hours MPT) and the demonstra hours MPT). Note: This failure dos not apply to Phase	binding due to severe rective action required. Pre- of swivel binding, and f MPT (manned pressurized ime which can be accumulated ated worst case interval (350
				B-EMU-106-A045 (6/7/99)- Gimbal swivel binding. Minor galling on inboard, or gimbals. Since eventual galling is inherent in the glove, several screens, including the FEMU-R-001 doo galling before it becomes serious. At NASA's reques observations of gimbal galling will be documented on Failure investigations will only be warranted for g the existing Functional Operation of Softgoods test apply to Phase VI gloves.	design of the 4000 series cument, exist to detect st, future visual n Discrepancy Reports. alling severe enough to fail
				D = EMRI 106 = 0.07 (7/10/00)	

B-EMU-106-A047 (7/14/99) -Tracked by B-EMU-106-A045

B-EMU-106-A048 (7/14/99) -Tracked by B-EMU-106-A045

B-EMU-106-A046 (7/14/99) -Tracked by B-EMU-106-A045

J-EMU-106-A003 (6/24/99) -Tracked by B-EMU-106-A045

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NAME		FAILURE		
P/N QTY	CRIT	MODE & CAUSES	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
		106FM03		
				B-EMU-106-A050 (8/23/99) - Tracked by B-EMU-106-A045
				B-EMU-106-A051 (8/24/99) - Tracked by B-EMU-106-A045
				B-EMU-106-A052 (8/24/99) - Tracked by B-EMU-106-A045
				Phase VI: B-EMU-106-T002 (2/29/00) - Primary restraint found frayed during glove bladder change-out. Caused by improper installation. Restraint bracket pinched PAR webbing as bracket was torqued during installation of restraint/bladder to glove disconnect. ILC ECO's 002 -117, 118, & 119 update EMU Maint. Manuals to include warnings at installation.
				J-EMU-106-A009 (5/19/01) - During STS-104 pre-flight processing, it was noted that the glove thumb side slotted gimbal pivot had excessive gap between washer and gimbal interface. Glove gimbal washer mis-oriented at assembly. Work instructions revised to ensure correct assembly.
				E. Ground Turnaround - 4000/Phase VI: During ground turnaround, in accordance with FEMU-R-001, the glove assembly is visually inspected (pressurized and unpressurized) with TMGs removed for; structural integrity, material damage or degradation and loose or missing screws. Also, during structural and leakage tests the proper operation of the gimbal swivel is verified. Every 56 hours (4000) of manned pressurized time the glove restraint is subjected to a complete visual inspection which includes visual inspection of the thread and webbing during which the gimbal swivels are inspected, lubricated and Loctite and screw torque are verified.
				F. Operational Use - 4000/Phase VI: 1. Crew Response - Pre/post-EVA : If detected by glove elongation, troubleshoot problem. If no success, use spare gloves if available. Otherwise, no go for EVA. EVA : If detected by glove elongation, terminate EVA.
				2. Training - No training specifically covers this failure mode.
				3. Operational Considerations - Generic EVA Checklist, JSC-48023, procedures Section 3 (EMU Checkout) and 4 (EVA prep) verify hardware integrity and systems operational status prior to EVA. Real Time Data System allows ground monitoring of EMU systems.

EXTRAVEHICULAR MOBILITY UNIT

SYSTEMS SAFETY REVIEW PANEL REVIEW

FOR THE

I-106 GLOVE ASSEMBLY

CRITICAL ITEM LIST (CIL)

EMU CONTRACT NO. NAS 9-97150

Prepared by: __________ Project Engineering

Approved by:

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