

GRUMMAN

Grumman Corporation

CRITICAL ITEMS LIST

ABBREVIATURE: MANIPULATOR FOOT RESTRAINT

PREPARED BY: L. HAHN & F. PERAZZO

REPORT NO: R425 27-R-1

REVISION: A

ASSEMBLY PART NO: SCD 2340100

DATE: 17 MAY 1966

FMEA REF REV	NAME, QTY & DRAWING REF DESIGNATION	CRIT	FAILURE MODE AND CAUSE	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
C1	Astronaut-to-MFR Tether QTY (one each lower & upper) Dwg C95-126 (lower) Dwg C95-127	1/1	C1 - (a) Structural failure of cable or hook due to defective material or, (b) Hook fails open due to contamination, galling or broken latch spring	END ITEM Loss of safety restraint for EVA Crew member GFE INTERFACE N/A MISSION N/A CREW/VEHICLE Possible loss of crewmember due to separation from orbiter	A. Design In addition to considering the launch loads discussed under cases A1 and B1, the MFR has been designed to accommodate the following conditions in the deployed configurations: - Astronaut handling loads of one hundred pounds in any direction. - Inertial response loads of MFR to RMS runaway accelerations (2 G //sec/sec linear accel. y, or z axes and 0.5 rad/sec/sec Roll accel about x axes) - RMS constrained motion load of 300 pounds ultimate, any point, any direction. - 140 pound couple by each foot to footplate assembly - 343 pound load applied to any tether/heel assembly. - The design minimizes orbital EVA thermal stresses by utilizing aluminum as the one basic structural material, coated with a low absorption thermal control coating per Grumman spec GSS-MFR-PS-001 Using the above load spectrum design safety margin of 1.14 for deformation and 1.40 for failure have been achieved. All springs are corrosion resistant and will be cycled a small fraction of nominal cyclic life in the 20 mission life of the MFR. Fatigue life based upon random response loads with appropriate stress concentration factors has been established using a scatter factor of 4.0 (e.g., 80 mission fatigue life based upon S-N curves) All materials are per table 1 and 2 of MSFC SPEC-522A, to reduce stress corrosion, and are certified for traceability/quality.

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ASSY NOMENCLATURE: MANIPULATOR FOOT RESTRAINT

PREPARED BY: L. HAHN & F. PERAZZO

REPORT NO. 040 BT R 2

REVISION: A 2

ASSEMBLY PART NO: 050 2040100

DATE: 8 JULY 1988

FMEA REF	REV	NAME, QTY & DRAWING REF DESIGNATION	CRIT	FAILURE MODE AND CAUSE	FAILURE EFFECT	RATIONALE FOR ACCEPTANCE
C1		Astronaut-to-MFR Tether QTY (one each lower & upper) Dwg C95-126 (lower) Dwg C95-127	U/I	C1 - (a) Structural failure of cable or hook due to defective material or, (b) Hook fails open due to contamination, galling or broken latch spring	<u>END ITEM</u> Loss of safety restraint for EVA Crew-member <u>GFE INTERFACE</u> N/A <u>MISSION</u> N/A <u>CREW/VEHICLE</u> Possible loss of crewmember due to separation from orbiter	<u>B. TEST HISTORY</u> 1. Acceptance test per procedure 300-94 01 at Grumman (7/7/83) before and after all tests. ATP includes functional tests of all operating functions and a general visual inspection. 2. Stress test per procedure 300-104 01 at Grumman (7/7/83). Demonstrated function and play less than 5 inch for five pound load in any direction and deflection less than 3 inches lateral and 2 inches longitudinal for 1 hundred pound loads. 3. Vibration and shock test per procedure 300-98 01 at Grumman (7/7/83). Demonstrated ability to withstand design levels without structural failure with no significant resonance. Several screws required the application of lockie. 4. APC/MFR ultimate load tests per STS03-0944 at Rockwell (9/83). Loads applied in 14 steps, each comprising 10% of final load no yield was observed at the ultimate load of 1.4 x limit. 5. Thermal vacuum test at JSC (7/29/84). MFR was operated at ambient temperature, plus 234 F and -137 F (average lowest achievable chamber temp) at an average vacuum of .00008 torr. 6. Center of gravity test at JSC (12/2/84) 7. Moment of inertia swing test at JSC (7/8/85) <u>C. INSPECTION</u> 1. NAVPRO inspects at production end items at completion of final assembly. 2. Anodic hard coated aluminum parts inspected for compliance to MIL-A-8625 C by DGAS. Certificate of compliance available at Grumman Detpage. 3. Thermal Control Coating process is controlled by inspections (post piece, cure, post coating and cure), and sample testing for coating thickness, coating adhesion and emission/absorption. <u>D. FAILURE HISTORY</u> None (per FRACA database). The MFR has been successfully utilized on five missions, STS 11, 13, 51A, 51L and 81C. <u>E. TURNAROUND</u> Inspection per 528/PIA 05004 N/C III DEC 1987 includes a functional test of all MFR operating functions and a general visual inspection. <u>F. OPERATIONAL USE</u> 1. Operational Effect of Failure - Crewman may separate from orbiter (worst case). Task delayed, increasing overall EVA time. 2. Crew Action - Orbiter crew required to maneuver orbiter to bring crewmember, who may tether back to MFR via waste tether. 3. Crew Training - standard training - to remain in foot platform during MFR operations which increases chance of separation. 4. Mission Constraints - none. 5. In Flight Checkout - Tether will be inspected prior to its use. This will minimize the chance of failure during EVA.