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THE FOLLOWING PAGES ARE CHANGES

TO BASIC DOCUMENT

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DIVISION OF NORTH AFTERICAN AVIATION, INC.

FOREWORD

This Design Information Report was prepared in compliance with AF04(695)-306, Part I, Item 2b as amended by Item VI of Request for Service Order 306-64-03.

ABSTRACT

This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LR101-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

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DESIGN INFORMATION REPORT FOR THE LV-2A PROPULSION SYSTEM (YLR79-NA-13 Main Engine and LR101-NA-11 Vernier Engines)

ROCKETDYNE

A DIVISION OF NORTH AMEFICAN AVIATION, INC.

6633 CANOGA AVENUE CANOGA PARK, CALIFORNIA

Contract AF04(695)-306

Part I, Item 2b as Amended by Item VI of Request For Service Order 306-63-01

PREPARED BY

Rocketdyne Engineering Canoga Park, California

APPROVED BY

Griffin

Atlas/Thor/Auriter Program Manager

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REVISIONS

DATE 30 July 1963

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A DIVISION OF NORTH AMERICAN AVIATION. INC.

FOREWORD

This Design Information Report was prepared in compliance with AFO4(695)-306, Part I, Item 2b as amended by Item VI of Request for Service Order 306-63-01.

ABSTRACT

This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LR101-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

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INTRODUCTION

The function of this report is to compile in handbook form the various items of engine design information in which the customer has expressed prime interest. It is also intended as an aid to design and to ensure compatibility of missile structure and the LV-2A propulsion system.

This report is not intended to supersede or duplicate existing model specification or Rocketdyne Field Service manuals.

Additions and revisions will be issued periodically to maintain this report on a current basis.

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SECTION I: PROPULSION SYSTEM DESCRIPTION AND OPERATING REQUIREMENTS

PROPULSION SYSTEM DESCRIPTION

The LV-2A propulsion system (Fig. 1) is composed of a booster main engine (Air Force designation YLR79-NA-13) and two vernier engines (Air Force designation LR101-NA-11) which provide roll control and finite impulse adjustment at the end of flight. The complete propulsion unit is a liquid bipropellant system and operates on liquid oxygen and RJ-1 hydrocarbon fuel. The main engine has a maximum over-all length of 142.587 inches and a maximum envelope diameter of 76.117 inches. The engine is rated to deliver a thrust of 170,000 pounds under sea-level conditions for a mainstage duration of 175 seconds. An additional 2120 pounds total thrust is developed by the two vernier engines during pump-fed operation and 1660 pounds total thrust during tank-fed operation for approximately 9 seconds after main engine cutoff.

Both the main and vernier engines are of the single-start, fixed-thrust type with no provision for restarting the engines or for intermediate thrust control. System propellant flowrates are controlled exclusively by orificing. All thrust chambers are gimbal-mounted for trajectory control and adjustment. The main engine thrust chamber is provided with a baffled injector. Ignition in all chambers is by means of hypergolic fluid. The entire propulsion system is controlled by an electrical system and a pneumatic system. Nitrogen gas is used in the latter system to operate all pneumatically controlled valves. Electrical power to control the engines is supplied from an external source until the missile is airborne, after which the missile's electrical system supplies the required electrical power.

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The turbopump for the main engine provides one accessory drive pad to be used for the attachment of missile accessories. The accessory drive pad is capable of delivering 100 horsepower for the intended flight duration. The accessory drive pad conforms to the Air Force-Navy Aeronautical Design Standard AND20002-X11-K, with the following exceptions:

- 1. Maximum speed is 4200 rpm; minimum speed is 3650 rpm.
- 2. Direction of rotation is counterclockwise facing the accessory drive pad.
- 3. No provision is made for lubrication of accessories.

One single-element heat exchanger for gasifying liquid oxygen to be used as LOX tank pressurant is installed in the turbopump exhaust duct.

A list of propulsion system installation drawings is given in Table 1.

A schematic of the main engine and details of the control orifice locations are shown in Drawings 104653 and 408113. Control orifice locations for the LR101-NA-11 vernier engines are shown in Drawing 350670.

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TABLE 1

LV-2A PROPULSION SYSTEM INSTALLATION DRAWINGS

YLR79-NA-13 Main Engine

Engine Assembly Drawing	104651
Major Component Installation	104652
Start System Installation	308451
Gas Generator and Exhaust Installation	308452
Propellant Feed System Installation	407226
Electrical Equipment Installation	502101
Pneumatic System Installation	556351
Lube System Installation	556352
Loose Equipment List	6516 0 1

LR101-NA-11 Vernier Engine

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Engine Assembly Drawing	350655
Gimbal Body Installation	350660
Propellant Feed System Installation	350665
Orifice and Accessory Installation	350670
Loose Equipment List	350674
Electrical Installation	350675

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(1) I. ORIFICE DIANETER TO BE DETERMINED BY PAO201-109. IDENTITY ALTERED PARTS PER RADIO4-010 TO REFLECT THE CRIFICE DIAMETER

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A. (* 0000 NAS-26301 SWITCH MS29724-4 PACKING $\langle \cdot \rangle$





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CUSTOMER CONNECT INFORMATION

This portion of the report contains information related to LV-2A propulsion system installation, weight distribution, instrumentation, electrical requirements, and general operating requirements and limitations.

ALLOWABLE INSTALLATION MISALIGNMENTS

}

The coordinate system used by Rocketdyne for designating reference axes and their origins is given in Fig. 2. Data are intended for use in the orientation of the LV-2A propulsion system in the Thor missile boattail.

Table 2 lists the customer connect points, coordinates the expected flight deflections of each point, and the allowable installation misalignments of the LOX and fuel pump inlet bellows for the main engine. The recommended maximum installation misalignment is based upon an inlet bellows approximately 13.5 inches long with an axial spring rate of 600 lb/in. and a maximum lateral spring rate of 500 lb/in. The recommendations assume that:

1. The bellows spring rates will be verified by laboratory test.

2. No liners are present in the bellows unless tests prove that there is a possibility of the liners "bottoming" or "hanging up" when subjected to maximum deflections resulting from the sum of allowable installation misalignment and turbopump and missile deflections.

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FORM R 18-G-18

TABLE 2

LV-2A PROPULSI

DEFLECTIONS AND ALLOWABLE INST

Customer Connect	Coord (Drav	linates, ring No.	inches 104654)	Approximat	e Flight Deflection
Points	x	Y	Z	$\Delta \mathbf{x}$	ΔΥ
Geometrical center of triangle formed by the three thrust missile attach points.	0.000	0.000	0.000		
Mount Attach to Missile	28.919	0.000	16.697		
Mount Attach to Missile	-28.919	0.000	16.697	will defle	ct radially (outboa
Mount Attach to Missile	0.000	0.000	-33,393	L	
Turbopump, LOX Inlet Elbow	0.000 ±0.187	6.500 ±0.132	-7.776 ±0.187	±0.12	+0.12 to -0.37
Turbopump, Fuel Inlet Elbow	0.000 ±0.187	5.250 ±0.132	23.963 ±0.187	±0.12	+0.31 to -0.12
Forward Pitch Actuator Attach Point (Center of Bearing)	0.000 ±0.12	12.407 ±0.12	-28.703 ±0.12		
Aft Pitch Actuator Attach Point (Center of Bearing)	0.000 ±0.37	43.375 ±0.37	-24.000 ±0.34		
Forward Yaw Actuator Attach Point (Center of Bearing)	-24.000 ±0.34	43.375 ±0.12	0.000 ±0.12	Deflection	 s of actuator attac
Aft Yaw Actuator Attach Point (Center of Bearing)	-28.703 ±0.12	74.341 ±0.12	0.000 ±0.12		
Forward Attach Lug, Heat Exchanger	6.12 ±0.12	51.27 ±0.12	40.69 ±0.12	The three lenclosed by	heat exchanger atta v these lugs must n
Forward Attach Lug, Heat Exchanger	6.12 ±0.12	51.27 ±0.12	40.69 ±0.12	closed by	the three thrust at
Aft Attach Lug, Heat Ex- changer (Center of Slot)	0.00 ±0.12	66.25 ±0.12	41.32 ±0.12		

*Refer to note 1 on drawing 104654. The total transverse misalignment shall not exceed (R-5214

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TABLE 2

LV-2A PROPULSION SYSTEM

AND ALLOWABLE INSTALLATION MISALIGNMENTS

Δγ	Δz	Δx	ΔΥ	ΔΖ	θX	θΥ	θz
							į
ist mount-to- radially (out	nissile attach board) 0.044 =	1 points a ±0.010 (NA	are within 0.01(A-13) inch durin) inch of t ng flight.	rue positio	n. The at	tach points
+0.12 to -0.37	+0.25 to -0.12	±0.50*	0.50 Tension or Compression	±0.50	±3*	0	±3
+0.31 to -0.12	+0.25 to -0.12	±0.50*	0.75 ± 0.50 Tension	±0.50	±3*	0	±3
actuator at	 tach points do	not affe	ct the missile	structure,			
t exchanger a hese lugs mus	ttach lugs are t not deflect	mated wi more than	th the missile. 0.37 inch rela	. The cent ative to th	roid of the e centroid	triangula of the are	r area a en-
toree thrust	attach points	•• 					
		1	}				

shall not exceed 0.50 inch.

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TABLE 2 (Continued)

Customan Connect	Coord (Draw	inates, ir ing No. 10	iches)4654)	Approxima	te Flight Deflect	cions, i
Points	X	Y	Z	Δx	ΔΥ	Δz
Oxygen Outlet, Heat Exchanger	-7.93 ±0.12	51.37 ±0.12	30.87 ±0.12	Deflects	with missile	
Aft End Heat Exchanger	0.00 ±0.12	69.43 ±0.12*	34.57 ±0.12	Deflects	 with missile 	
LOX Supply to Vernier Engine	30.63 ±0.12	47.07 +0.34 -0.27	-2.48 +0.47 -0.49	±0.12	+0.31 to -0.12	±0.
Fuel Supply to Vernier Engines	28.15 +0.29 -0.31	40.85 +0.27 -0.28	-6.82 +0.33 -0.31	±0.12	+0.25 to -0.12	±0.
Main Oil Discharge	1.33 ±0.12	29.73 ±0.12	14.72 ±0.12	±0.12	+0.19 to -0.12	±0.
Fuel Start Tank Vent Valve Vent	20.19 ±0.12	12.53 ±0.12	0.18 ±0.12	±0.12	+0.25 to -0.12	±0.:
LOX Start Tank Vent Valve Vent	24.70 ±0.12	6.54 ±0.12	-14.06 ±0.12	±0.12	+0.19 to -0.12	±0.]
High-Pressure Gaseous Nitrogen Supply	8.65 ±0.12	11.35 ±0.12	-26.45 ±0.12	±0.12	+0.19 to -0.12	±0.1
Center Tachometer Mount Pad (No gasket)	-0.40 ±0.12	20.07 ±0.12	-3.76 ±0.12	±0.25	+0.12 to -0.25	±0.2
Center Hydraulic Pump Mount Pad (No gasket)	3.96 ±0.12	24.85 ±0.12	-1.26 ±0.12	±0.25	+0.12 to -0.25	±0.2
LOX Seal Drain	-2.00 ±0.12	30.17 ±0.12	15.98 ±0.12	±0.25	+0.19 to -0.12	±0.3
0il Seal Drain	-3.50 ±0.12	29.90 ±0.12	15.87 ±0.12	±0.12	+0.25 to -0.12	±0.3
Pressure Takeoff from Pneumatic Manifold	15.08 ±0.12	7.40 ±0.12	-15.17 ±0.12	±0.12	+0.19 to -0.12	±0.1

*Refer to note 7 on drawing 104654

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TABLE	2
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(Continued)

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ΔΥ	Δz	<u>∆ x</u>	ΔY	Δz	θx	θγ	θz
with missile		The cust applied shall be missile	tomer connect except that e designed an and maximum	points are f necessary to d installed f flight deflect	to be connect support it to provide s tions.	cted with n s weight. for both ma	no load The parts aximum
+0.31 to -0.12	±0.12	Turbine (a) 5	Exhaust Syst The aft flang shall be para four degrees.	em e of the turk llel with the	dine exhaus e heat excha	t duct asse anger flang	embly ge within
+0.25 to -0.12	±0.12	(b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	The distance The misalignm shall not exc	between the t ent of the ce eed 0.38 inch	two flanges enterline of	shall be 0 f the two f	0.31 ±0.25 inc Clanges
+0.19 to -0.12	±0.37						
+0.25 to -0.12	±0.12	8					
+0.19 to -0.12	±0.12						
+0.19 to -0.12	±0.12						
+0.12 to -0.25	±0.25				3. -		
+0.12 to -0.25	±0.25				1		
+0.19 to -0.12	±0.37					\mathbf{C}	
+0.25 to -0.12	±0.37					L	2~, 1,7 2,7
+0.19 to	±0.12						9

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TABLE

•1

(Contin

Customer Connect	Coord (Draw	inates, in ing No. 1	nches 04654)	Approxim	ate Flight Deflecti
Points	X	Y	Z	$\Delta \mathbf{x}$	ΔY
Electrical Ground Connection	17.25*	11.40	17.48	±0.19	+0.25 to -0.12
Missile Interconnection	17.25	14.05	17.55	±0.19	+0.25 to -0.12
Missile Power Connection	19.35*	13.25	17.55	±0.19	+0.25 to -0.12
Vernier LOX Vent Valve Con- trol Solenoid Exit	14.33 ±0.12	21.18 ±0.12	-3.41 ±0.12	±0.12	+0.19 to -0.12
Vernier Engine Propellant Valve Control Solenoid Exit	15.92 ±0.12	23.31 ±0.12	-4.33 ±0.12	±0.12	+0.19 to -0.12
Lube Tank Vent and Overflow	-19.23 ±0.12	2.59 ±0.12	5.27 ±0.12	±0.06	±0.06
Lube Tank Horizontal Drain					

*Refer to note 9 on drawing 104654

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FORM R 18-G-18

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ROCKETDYNE A DIVISION OF NORTH AMERICAN AVIATION. INC . , **"**'

TABLE 2

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(Continued)

te Flight Deflect	ions, inches	Allowab	le Installat	ion Misalig	nment With R	espect to E	ngine, inche
ΔY	Δ z	x	ΔY	$\Delta \mathbf{z}$	θχ	θy	$\Theta_{\mathbf{Z}}$
+0.25 to -0.12	±0.19	These v inlet b maximum	alues are ba ellows with transverse	sed on inle an axial spi spring rate	t bellows wh ring rate of of 500 lb/in	ich have an 600 lb/in. n.	axial and a
+0.25 to -0.12	±0.19						
+0.25 to -0.12	±0.19						
+0.19 to -0.12	±0.12						
+0.19 to -0.12	±0.12						
±0.0 6	±0.06						
					J		



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WEIGHT DISTRIBUTION AND FLUID VOLUMES

Weight, balance, inertia, and fluid volume information for the LV-2A propulsion system configurations is presented in Tables 3 and 4.

This data may be used in determining missile deadweight distribution, structural requirements, basic loads, stability, performance, and control requirements.

CUSTOMER CONNECT AND INSTRUMENTATION DRAWINGS

The locations of connections that are necessary for the operation of the LV-2A propulsion system in the missile are shown in Drawings 104654 and 350723 . Locations shown include those for supply connections, drain and vent connections, and flush and purge connections. Structural attachments and accessory pad information are shown, as well as gimbal bearing alignment and lubrication points.

The instrumentation tap locations on the main vernier engines that are available for use appear in Drawings 702827 and 350050 .

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TABLE3

CENTER OF GRAVITY, MOMENT OF INERTIA, AND WEIGHTS FOR MAIN ENGINE (RJ-1 FUEL)

Propulsion system weights and centers of gravity* (including vernier engines)

Condition	Weight, pounds	Y Arm, inches	X Arm, inches	Z Arm, inches
Dry	2116	100.2	100.4	103.3
Wet	2690			102.3

*Reference point (gimbal bearing) is (100,100,100).

Moments of inertia of the propulsion system about axes through its center of gravity, wet and dry, with corresponding radii of gyration

Condition	Weight, pounds	Y Roll	X Pitch	Z Yaw
Dry Radii of gyration	2116	167 slug sq ft 19.1 inches	616 slug sq ft 36.7 inches	626 slug sq ft 37.0 inches
Wet Radii of gyration	2690	223 slug sq ft 19.6 inches	782 slug sq ft 36.7 inches	816 slug sq ft 37.5 inches

Moment of inertia of the gimballed mass about the gimbal axes (verniers not included)

Condition	Weight,	Y Roll,	X Pitch,
	pounds	slug sq ft	slug sq ft
Dry	828	32	311
Wet	1057	44	416

Longitudinal (Y axis) location of center of gravity of the gimballed mass in inches aft of the gimbal axis.

> Dry = 29.0 inches Wet = 29.2 inches

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TABLE 4

MAIN ENGINE FLUID VOLUME DATA

Component	Fuel Volume, cu in.	Liquid Oxygen Volume, cu in.	Oil Volume, cu in.
Thrust Chamber	3987	935	
Main Ducts	1111	1614	
Turbopump	950	945	
Lubrication System			3927
Start System	1319	1454	
Vernier Engines (2)	106	46	
Miscellaneous Units	120	183	

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#### ELECTRICAL SYSTEM

Twenty-five to 30 volts dc (to the main engine electrical relay box) will be maintained until 0.5 second after all starting sequences have been completed, and 20 to 30 volts dc thereafter. The power required is 800 watts maximum for starting, and 300 watts is required for flight operation. The command cutoff signal shall have a minimum current capacity of 0.30 ampere and shall be sustained for a minimum of 0.10 second. Electrical supply for the heaters during preflight is 115 volts ac at 60 to 400 cps. The maximum ground power supply shall be 3000 watts.

Nominal power requirement profile charts are presented in Fig. 3, 4, and 5. Drawing 900100 is the electrical system schematic for the LV-2A propulsion system.

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# CONTROL PANEL

#### CONTROL-MONITOR

### INTERCONNECTING BOX

# GROUND & EXTERNAL EQUIPMENT

ENGINE RELAY BOX (REF)

(REF WIRING DIAGRAM 500360) ENGINE JUNCTION BOX (REF) (REF WIRING DIAGRAM 500368)

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### ENGINE ACCESSARY SECTION (REF)

CONTROL PANEL POWERSUPPLY 200 2101-2 OBSERVER 63070 120 V.A.C. E CUT-OFF 74007 TADIE ANDIE MISSILE. E POWER P4011 J4011 74000 P4015 J4015 5 51010 INTERCONNECTING BOX POWER MONITOR JEK-3/E477-1 120 V.A.C. 2 GIOOO 3 PH GOCY 904445 J4031 P4031 74033 (A4033) J4035 P4036 PROP. TRANSFER AUXILLARY SYSTEM PNUEMATIC TEST PANEL > TO GROUND CIRCUITS TO J403. 903395 (904425 :FO JI8,J25 (500352 RERE) (500356 J"BOX) BOX 520 500356 500 952 500352 D.A.C., > 5" BOX SIGNALS & R. B. 01.R79-MISSILE 2 POWER 10 55, (500352 A (500356 : - **3** 633 -500361-- 500362 (XLR79-MA-3) (XLR79-NA-9) EQUIPMENT START TANKS PRESSURIZING 501281-((REF) (XLR79-NR-11) --V. E. PROP ' 500360) AL. CONTROL BOX (REF) VALVE 500368) 1.0X 747 CONTROL VALVE (XLRYS FUEL É GAS GEN CONTROL 21 SECTION (REF) VALM. ...

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.		MS24140-1 MIL-R-6106 XI	Te te	
	CONTACT ARRANGEMENT	MHYX-4003 ALLIED 13	9/9/0/10/11/11/12/12/	CONTA
·	• .	HE-OI (N.C.) GV CONTROLS	H 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ARRANGEM
Ļ		G-V CON TROLS	354	
L L	KII-C 45 IP IT	PART NO MEGR SPECIFICATION MS24140-1 MIL-R-GIOG	N NONC NO MENDINE NO MENDIN	KINO NC
	K13-C2 44 1P 2T K13-C2 44 1P 1T K14-C 44 20 AT	MHYX-4003 ALLNED MIL-R-6106	43 /9	K62-1 34
	KIG-C 43 3P 2T KIG-C 43 IP IT	MS24/43-/	45 45 45	<u>K64-I 31</u>
	(17-C1 43 4P 27 ) (17-C2 43	MYX-4003 ALLIED	44 38 38 39 39 59 38 59 39	K66-J 24
	(22-F 38 (23-C 24		75 35 18 35 41 39 97	K71-0 26 K71-5 21
KK	24-C 37 25-C 40		34 34	K73-C 20 K75-I 25
×	26-C 39		40	K78-7 25
K	<u>co-c/ 34</u> 28-C2 34		36 34 4/ 00 34	KUI-CI 22 KUI-CE 80
. R.	3/-C/ 4/			Kat-C3 22 Kat-C 20
<u>k</u> k	31-C2 41 31-F 21		33 32 31 24 . 25	K05-C 20 K05-C 20
Ŕ	3/-3 22 3/-V 29 7-C 44		/7 80 18	K9/-C1 19 K9/-C2 19
XX	92-0 39 39-C1 40		26 85	K93-C 17 K94-C 35
ĸĸ	99-C2 40 33-V 28		4136 31 33 32 25 34	<u>K95-C 36</u> <u>K96-C 13</u>
K3	19-C2 38 19-C2 38		23 36 36 33 32 31	KIII-T 43 KII2-T 43
1X3  X3	6-CI 36 /P /T M	24/40-1 MIL-R-GIOG	17 36 36 34 33	<u>KIIB-F.</u> <b>4</b> 1
R R	14-C 36 4P 27 M	HYX-4009 ALLIED 12-D-N3 AGASTAF	26 36 35 39	KI31-7 48 KI32-71 42 X/20-71 42
K5	0-C 35 4P 27 M	47X-4003 ALLIED		KI3EF3 48 KI3E-73 48
RS	1-C2 34 MI	YX 4003	34         31         33         32           30         33         23         17	<u> </u>
				K141-77 42 K141-72 42 1
K54	5-1 33 MA	YX-4020	33 33 4/ 30	KI352-V 20
K58		rx-4020	2 2 4/ 30	KI386-V 28 1
K55	9-V 23		33 32 37 23 23 39	K1361-L 26 1
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CONTACT         MIL-R 4 (02)         Contact         Contact         Contact           ARRANGEMENT         MIL-LODO         ALLIED         ////////////////////////////////////	· ;		·		RE/	AY.S.				COIL	·	÷	<u> </u>	<u> </u>	ÓN	TA	77	5			] .	(RFRP)			RESER	VED W
BR2E # 180 - 1         MIL : PE 0002         X202         X202 <thx202< th="">         X20</thx202<>				÷;								-1-	- <u>1</u>	Ť	Ť			Ť.	T	-		X4	PHOT	K201	K301	K401
CONTACT RRANDEMENT       MM12.40.00 (1.10)       ALLIED       1/2       2/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2       1/2 <td></td> <td>• •</td> <td>•</td> <td>ļ</td> <td>MS2</td> <td>4140-</td> <td>• /</td> <td>M</td> <td>1L-R-6106</td> <td>XIX2</td> <td>2/2</td> <td></td> <td>1</td> <td>L</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>X6</td> <td>PIOZ</td> <td>×202</td> <td>K302</td> <td>K402</td>		• •	•	ļ	MS2	4140-	• /	M	1L-R-6106	XIX2	2/2		1	L								X6	PIOZ	×202	K302	K402
UNIALITY     ANULLIED     ////////////////////////////////////	<b>COA</b>		~			× 20.	<u> </u>			15	-		240	+	1			- <del> </del> -	+-	- <del> </del>		X7	P10.3	K203	K309	K403
APPRANGEMENT     2/12-D-M3     16357m1     2/12/25/25/25     2/12     1     1       APF-DU(N-C)     0/10-COMPRESS     2/12     1     1     1     1       APF-DU(N-C)     0/10-COMPRESS     1     1     1     1     1       APF-DU(N-C)     0/10-COMPRESS     1     1     1     1     1       APF-DU(N-C)     0/10-COMPRESS     1     1     1     1     1       C44-1     31     0/10-COMPRESS     1     1     1     1     1       C41-1     1     0/10-COMPRESS     1     1     1     1     1       C41-1     1     0/10-COMPRESS     1     1     1     1     1       C41-1     1     0/10-COMPRESS     1     1     1     1 <td>çon</td> <td>VIACI</td> <td></td> <td></td> <td>MHS</td> <td>×-400 ×X-40</td> <td>20 20</td> <td>AL</td> <td>LIED</td> <td>13/14</td> <td>7/2 )</td> <td>7/17</td> <td>47</td> <td>31/2</td> <td>5/5</td> <td>1</td> <td>1/7</td> <td></td> <td></td> <td></td> <td></td> <td>XIZ</td> <td>PIOS</td> <td>K205</td> <td>K305</td> <td>×405</td>	çon	VIACI			MHS	×-400 ×X-40	20 20	AL	LIED	13/14	7/2 )	7/17	47	31/2	5/5	1	1/7					XIZ	PIOS	K205	K305	×405
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ARRANO	GEME	NT		2112	-D-H	3	. A	SASTAT	AH	2	20	11				r					XEN	P106	X206	¥306	K406
LAP - O(1/N, O.)     EVELONING2 (2-3/2)       TELM NOCULUID     MESSE     Specific (2-3/2)       TELM NOCULUID     MESSE     Specific (2-3/2)       Reset     34     24     27/10       Reset     34     24     27/10       Reset     34     24     27/10       Reset     34     31     30     31       Reset     34     31     30     31       Reset     34     21     30     31     30       Reset     34     21     31     30     31     30       Reset     34     31     30     31     30     31       Reset     34     31     30     31     30     31       Reset     34     31     30     31     31     31       Reset     34     31     30     31     31     31       Reset     34     31     32     31     31     31       Reset     34     34     32     34     31     33       Reset     34     32     34     31     33     31       Reset     34     32     34     33     33     33     33       Reset		r		. 1	HF-C	01 (N.	<u>c.</u> )	<u>G</u> -	V CONTROLS	23	-			-						i - i		K104	PIOT	K207	K307	K407
TEM NOCULAR       CESC       PHET NO       MESR       SPECIFICATION NONE NOVE NOVE NOVE NOVE NOVE NOVE       NEEd       TELE         K8221       34       2P       2112       0.11       Adassa       101       NOTE         K8221       34       2P       2112       0.11       Adassa       101       NOTE       NOTE <td></td> <td></td> <td></td> <td>I</td> <td>HF-C</td> <td>5/(14.6</td> <td></td> <td>6.</td> <td>VCONTHOLS</td> <td>5-3</td> <td>27</td> <td></td> <td></td> <td>+-</td> <td></td> <td></td> <td></td> <td>-+-</td> <td>+-</td> <td>_{</td> <td>1</td> <td>KIOGN</td> <td>PIOS</td> <td>K208</td> <td>×308</td> <td>K400</td>				I	HF-C	5/(14.6		6.	VCONTHOLS	5-3	27			+-				-+-	+-	_{	1	KIOGN	PIOS	K208	×308	K400
TEM NOQUUED, LESS.       PART NO.       MEGR.       SPECIFICATION NORK NORK NORK NORK NORK NORK NORK NO			• 、		• • ••								•					-	•			KIII	KIIO	K210	K310	K410
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	TEM NO	CON LO	a	SC	PHR.	TNO	MFG	ē [	SPECIFICAT	TION	NO	VCW	ØW	C M	DAC	20	NC	VON	CM	owc		KIBB	PIII	K211	K311	K411
664-1       31       40       21       41       31       30       31       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100 <td>K62-I</td> <td>34</td> <td>20</td> <td>27</td> <td>2112</td> <td>D - H3</td> <td>AGASI</td> <td>77</td> <td></td> <td></td> <td>18</td> <td>3</td> <td>3</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>K218</td> <td>5119</td> <td>K2/2</td> <td>K312</td> <td>K412</td>	K62-I	34	20	27	2112	D - H3	AGASI	77			18	3	3									K218	5119	K2/2	K312	K412
Sec     Sec <td>K64-I</td> <td>31</td> <td>AP</td> <td>27</td> <td>MHY</td> <td>- 40m</td> <td>A111</td> <td>FD</td> <td></td> <td></td> <td>41</td> <td></td> <td></td> <td>+</td> <td>30</td> <td>37</td> <td></td> <td></td> <td>-<del> </del></td> <td>: {</td> <td>1</td> <td>K 301</td> <td>PIL</td> <td>K213</td> <td>K313</td> <td>K418</td>	K64-I	31	AP	27	MHY	- 40m	A111	FD			41			+	30	37			- <del> </del>	: {	1	K 301	PIL	K213	K313	K418
K46 - 7       24       MHYA - 4003       41       28 64       24       K307       K116       K917         KT1-0       2       41       28       64       11       K307       K116       K917         KT1-0       2       41       K307       K116       K317       K318       K317       K317         KT1-0       2       AHYA - 4003       17       R       21       K337       K318       K318         KT3-C       2       AHYA - 4003       17       R       21       K307       K308       K227       K319         KT3-C       2       AHYA - 4003       27       K307	······	<u> </u>					1		· · · · · · · · · · · · · · · · · · ·			ť	+-	+	+	<b>–</b>					-	K306	PIIS	+	X315	K415
CT1-7       2       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C       C <td>K66-I</td> <td>24</td> <td><u> </u></td> <td></td> <td>MHY</td> <td>x-4003</td> <td></td> <td></td> <td></td> <td></td> <td>41</td> <td>- I</td> <td>2</td> <td>3 8</td> <td>4</td> <td>24</td> <td></td> <td></td> <td>-</td> <td></td> <td>1</td> <td>K307</td> <td>KII</td> <td>1</td> <td>K316</td> <td>K416</td>	K66-I	24	<u> </u>		MHY	x-4003					41	- I	2	3 8	4	24			-		1	K307	KII	1	K316	K416
11/10       21/10       19       24       21       17       18       21       17       18       21       17       18       21       17       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       11       170       18       10       170       18       10       170       18       10       170       18       10       170       18       170       18       170       18       18       18       18       180       18       180       180       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18       18 </td <td>1 1 C</td> <td></td> <td><u>                                     </u></td> <td></td> <td>·</td> <td>4</td> <td><b>├↓</b></td> <td></td> <td>4</td> <td>+</td> <td>4</td> <td>K317</td> <td></td> <td></td> <td>K317</td> <td>K417</td>	1 1 C		<u>                                     </u>		·	4	<b>├↓</b>												4	+	4	K317			K317	K417
277-5       27       MHYX-6003       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0	K71-0	26	<u>+</u>			÷	┟┈┈┥╴	it			23		2-	-+	24	21					- ·	K310	+	K219	×310	K419
$X13 - C_{25}$ $MMT_{1}^{-1} - 403$ $T_{1}^{-1}$ $T_{2}^{-1}$ $T_{1}^{-1}$ $T_{2}^{-1}$ <td>K71-5</td> <td>21</td> <td><u>†</u></td> <td></td> <td>MHY</td> <td>X-4003</td> <td><u>}</u></td> <td></td> <td></td> <td></td> <td></td> <td>17</td> <td>-JR</td> <td>1</td> <td></td> <td>21</td> <td></td> <td>-</td> <td>Ť</td> <td></td> <td></td> <td>1.305</td> <td></td> <td>K220</td> <td>K320</td> <td>K42</td>	K71-5	21	<u>†</u>		MHY	X-4003	<u>}</u>					17	-JR	1		21		-	Ť			1.305		K220	K320	K42
K15-1       25       MHYR-MARCO       C5       25       25       24       1       27       23	K73-C	28	<b></b>		MHY	- 4003						17	1	T	T	21			T	-	].	K340	1	K221	K321	K421
NB-T       25       AHPT-4003       25       APPE	K75-1	25	ļ	<b>[</b> ]	MHY	X-4020	1	÷-			25	2	5 2	94	11	23	23	-+-	-		4	K349	+	K222	K322	K422
00-01       02-0       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01       100-01	K78-T	28	ŧ		MHY	X-4007	<u>}</u> <u>}</u> -		·····			25	-	+	+		n - 4			• +	f ·	K758	·	KPPA	K324	K424
RTH-C1       22       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P       P </td <td></td> <td></td> <td>1</td> <td><u>†</u></td> <td></td> <td>1</td> <td><u> </u></td> <td>+</td> <td>·····</td> <td></td> <td></td> <td></td> <td>-†-</td> <td>t</td> <td>-</td> <td></td> <td>-</td> <td></td> <td>-</td> <td>1</td> <td>1</td> <td>K360</td> <td>1</td> <td>K225</td> <td>K325</td> <td>K425</td>			1	<u>†</u>		1	<u> </u>	+	·····				-†-	t	-		-		-	1	1	K360	1	K225	K325	K425
Kall-C2       22       44       34       22       K400       K227       K297         Kall-C2       20       P       27       K41       34       22       K400       K227       K297         Kall-C2       20       P       27       Mark 4002       K41       K400       K227       K297         Kall-C2       20       P       27       Mark 4002       K414       K228       K400       K227       K208	ROI-CI	22										44	3	6	23		38		1		1 "	K391	1	K226	K326	KACE
Sat C2       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C       2 C <t< td=""><td>KOI-CZ</td><td>22</td><td>4P</td><td>27</td><td>MHY</td><td>- 100-</td><td>ALLIL</td><td>P</td><td></td><td></td><td>17</td><td>27</td><td></td><td>4</td><td>34</td><td>22</td><td>+</td><td></td><td>+-</td><td>-<b>i</b>-</td><td>1.</td><td>K400</td><td></td><td>K227</td><td>K327</td><td>K427</td></t<>	KOI-CZ	22	4P	27	MHY	- 100-	ALLIL	P			17	27		4	34	22	+		+-	- <b>i</b> -	1.	K400		K227	K327	K427
1035 C       20       40       27       MHY2 4009       ALLICD       20       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10	KBP-C3	20	PP	21	2112	DIAS	ACAST		·		14	30				ł			-+-	-+	1 7 2	KALA.		x228	K320	
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KSJ-CI       19       17       14       36       11/19       14       36       11/19       14       36       11/19       14       36       11/19       14       36       11/19       14       36       11/19       14       36       11/19       14       36       11/19       14       14       15       17       35       17       35       17       13/10       15       17       13/10       15       17       13/10       15       17       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10       13/10	×86-C	20	Ļ									20	H	B	Ţ.	Ĺ				ili.		K429		K231	K331	
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204	KA04	1 504	K604	K 104		K904	XIN
305	KAOG	×505	14606	K 105		K.905	XSW
307	K407	X506	×606	K /06		K906	X28
30.8	KADP	1001	X607	<u>  x 107</u>	<u> </u>	K907	X2C
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5/0	X410	K3/0	+	KIIO	······	K910	X3C
212	VA12	<u> </u>	K611	<u>K7//</u>		K911	X4A.
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914	KAIA	K3/3	K613			K913	X4E
215	KA15	VEIE	K6/4	K7/4		K9/4	X5A
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9/7	KA17	125/0	×6/6	K716		K916	X5C
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220	KADO	12/9	K619	K7/9	<u> </u>	K919	
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بالمراجع فيكم متناد ومسيد

		INDIC	ATING LIG	HTS		*			Λ	NIS	CELLANEC	005	
A MO		DESC	FART NO.	MEGR	SPEC		ITEM NO	ZOC	DES	C	PART NO.	MFGR	SF
SIRA	15	WHITE	19-902426	KORRY			CALLCI	46	1P	17	D7271-1-5	SPENCER-THEM	HCOTAT
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<u>5-C</u>	43	WHITE	19-902403				·	<u> </u>					
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20-0	42	GREEN	19-902404				CB-13-C	46			07271-1-25		
21-0	41		19-90-405		1		CA-13C3	46	IP	17	D7271-1-25	SPENCER-THER	MONT
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33. CIRCUITRY TO BE ADDED FOR MES-ISI (SIOCO MD 6) 32. CIRCUITRY TO BE ADDED FOR MES-160 (GLOOD MO 15). 31. REMOVED PER MB3-149

30 ADDED PER MB3 149 29 CIRCUITRY TO BE ADDED FOR MB3-144 (6 1000 MD 14)

28. CIRCUITRY TO BE REMOVED FOR MB3144 (G 000 MDH) 27. CIRCUITRY TO BE INSTALLED FOR HYBRID ENGINE FIRME ( 41000 MD13 \$ 4 3000 MD17)

CARENTRY TO BE INSTALLED FOR LOX YALVE MONITOR 26. CUTOFF (GIONO MDIZ. & G3002 MD5)

25 MYTOOR RELAYS REPLACED ON ALL ENGINE RELAY BORES BY NAS 27103 TYPEI RELAYS CONNECTORS CODED BY REPLACED ON ALL ENG RELAY BOXES BY CONNECTORS CODED . 24 ENGINE

PINS 1. F.C. G. V. WER ARE BUSSED TOGETHER IN JED INTERNALLY 23, 22. PINS Y.T.A. P. S.C.D. ARE BUSSED POSETNER IN JOO INTERNALLY

21. PINS X, 4, C.T. del ARE BISSED TOGETHER IN JEO INTERNALLY 20. PINS D, E,F, G CM ARE BUSSED TOGETHER IN JES INTERMOLLY CHEWITRY TO BE RODED FOR MB3-19. (GIOOD MDH) 19.

CIRCUITRY TO ME REMOVED FOR MESSER (51000MDII) CIRCUITRY TO ME REDED FOR MESSER (5000MDII) 18 17.

16 CHEVITRY 70 AF 80 - FOR MES-24 (5000MDR)

3,174

3.10 1.23

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TO

.0138 TO

.234 10

\$14.10 746 10 

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15. CIRCUITRY TO BE ADDED FOR START TANKS PRESSURIZING CUT-OFF, GROUND POWER FAILURE CUT-OFF & SERMATENOF MISSIE & GIOD

CIRCUITRY TO BE REMOVED FOR START TANKS PRESSURIZING CUFOFF, GROUND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE & SID

- 3. CIRCUITRY TO BE ADDED FOR LAUNCH LOCKOUT. (GODDINDLEUP)
- CIRCUITRY TO BE REMOVED FOR LAUNCH LOCKOUT (GIODADG & UR) 12
- IL CIRCUITRY TO BE ADDED FOR RESET OF XLR 19-NA-TELECOMDA CUP 10. CIRCUITRY TO BE REMOVED FOR STATIC FIRING. (GIOOOMES)
- CIRCUITRY TO BE INSTALLED FOR STATIC FIRING. (GIODO INDS, GODOR 9.
- UNDERLINED CONNECTOR PIN LETTERS 1
  - DENOTE LOWER CASE.

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- 7. REF DWG 900040 SCHEMATIC, 6. REF DWG 900075 BLOCK DIAGRAM
- SYMBOL () INDICATES RECORDER CONNECTIONS 5
- 4 REF DWG SCHEMATIC NO 902500 FOR
- ENGINE SIMULATOR SYMBOL D DENOTES DOUGLAS AIRCRAFT COMPANY CONNECTIONS. З.
- WIRES ARE "20 AWS FOR ALL PANELS & WIRES ARE MIG ANG FOR ALL CABLES

THE COMPLETE REFERENCE SYMBOL DESIG-NATION FOR CONNECTOR'S IS IN 4000 SERIES (EXAMPLE: J 37 IS J 4037) EXCEPT THOSE IN ENGINE RELAY BOX , ENGINE JUNCTION BOX, & ENGINE ACCESSORY SECTION.

NOTE: UNLESS OTHERWISE SPECIFIED



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4.		ZON	ε / ·		<b>A Y</b>	- <del>  .</del>	<del>۳</del> 7	TT MAY BE BEWORKED IT BEOD		PARTS MARE OIL
		3,17	4 1. AD	DED NOTE 26 & CIRCUITRY	3 ECP MB3-67	200	5 SYM.	TOC . I BE REWORKED () HOW	SICP IN/CTICE	DATE SIGNARIE
	4 · ·	. 28	FOR	LOX VALVE MONITOR		1	A		. i. H	
		·		OFF	" " " " "		, <u> </u>			
	·	136	ICT.		3 ECP MB3-103	<i>, , , , , , , , , , , , , , , , , , , </i>	ๆ	CUT-OFF CIRCULTRY	A HOLD 3	7   .
		41		DED NOTE 27 & CHECHITRY		35		2. ADDE- K91-C2 CON	ITACTS 3	3
•			FO	R HYBRID ENGINE FIRING	3-22-61	19		3. ADDED PROP. DEPLE	TION CUT- 3	ECP.930-13
	· ·	N-	0 1 1		3 EC P MBD-JAA			OFF, SLOW BUILD-U	CUTOFF	11-1-5 B BEATTI
		· 42	зн з	DEDWATE 28 \$ 20 \$ concurr		X	+	HIGH TENFERITURE CO.		<i><i><i>L</i>(<i>P</i><b>3</b>)<i>N</i>-0</i></i>
			FOI	RELIGHT LOCK-IN CIRCUIT	8-13-62		B			
· · ·			$\frac{1}{\tau}$			her	5	1. ADDED RESET CIRC		6(7950-13
· ·	-					27		3. CHANGED LAUNCH	LOCKOUT	10-300-H
	•	£31	I. ADDE	D NOTE 30 <b>\$31, CODE</b> \$	- 3 ECP M83-149	ł		CIRCUITRY	<i>.</i>	
			CIRCUI	TRY FOR FLIGHT LOCK	B.J. LUCAS	35	·	5. RELAY KAA-C T.D.F	213 S	CP3204
			IN CIR	CUIT	11-14-62			SEC. WAS 1.5 SEC.		1-5-9 8 BE TTA
			K		ECP M83-/60	1	C			······································
		21	I. ADD	ED NOTE 32 233. CODE	3 ECP MB3-161		H	ADDED NOTES 14 E 15		ECP MAR-E
		ļ.,	RECO	RDING CIRCUIT THROUGH	1 12/13/62		2.	ADDED COMPONENTS L	IST FOR	
	,	A		ROLMONIOR	SPORERY 1			ENGINE RELAY & JUNC ADDED CONTROL-INDI	CHICK BOX	ECPMR3-15
•				*				LUB. TANK HEATER C	RCUITRY	
·				۰. ۱				ADDED AUXILLARY PN TEST PNL CIRCUITRY	ELIMENTIC 3	5 33 59
x		1		•		1	In		•	
								ADDED HOTEL IC LIT	- <u>-</u> -	500 MB3-34
		i -		• •			1"	RELATED CIRCUITRY	<u>به</u>	5 2 CP M05-24
•				er.,			12	ADDED NOTES IN \$ 19;	¢ 3	ECP MB3-19
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	•	•		· .		- F	· 3.		فار	1 CP 3356 77
E ADDED FOR START TANK	KS PRESSURIZ		•	•			3.	500352-11 WAS SOURCE		BCP 3536-77
E ADDED FOR START TAN POWER FAILURE CUT OFF & REMOVED FOR START TH	KS FRESSURIZ SEINANTINOF	LINE MISSILE É I	G1000 BUSI	5 (G1000MD7 fUP)	• • •	, j	3.4	500352-11 WAS SOMERE ADDED SEQUENCE CHO	<b>r</b> 1	ACH 5536-77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TAN POWER FAILURE CUT-OFF & S	KS FRESSURIZ SEFAMATÓNOFI NKS PRESSURI TERAROTION OF A	11. <b>MB</b> MISSILE & 1 121.NIS MISSILE & 1	GROOD BUSL SROOD BUSE	5 (GIOCOMDZĘUP) SIGNOCOMDZĘUP)	• • •		3.	500352-1/ WAS SOURCE ADDED SEQUENCE CHAN	7	100 335.77 100 335.77 100 335.77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TAN POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC	KS FRESSURIZ SEFARATION OF I NKS PRESSURI TEMARATION OF I TROUT (GLODO	LINE MISSILE É IZINIS MISSILE É MISSILE É UP	GAQOO BUSL SIOQO BUSE	5 (510001107 (119) 5 (510001107 (119)			3.	SOO352-1/ WAS SOUGE RODED SEQUENCE CHOM	<b>7</b>	ACR 335.77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC REMOVED FOR LAUNCH LOC REMOVED FOR DESER OF 200	KS FRESSURIZ SEPARATION OF A VKS PRESSURI TERNORTION OF A TROUT (GLOOD CKOUT (GLOOD CKOUT (GLOOD)	11.005 MISSILE & I IZINIS MISSILE & UP MIDE & UP MIDE & UP	61000 BUSL 61000 BUSE	s(skoomoztur) s(skoomoztur) FOR	REFE	RI	5 5	SCO352-1/ WIRS SCHERE ROCKED SURVEAKE CHIM	₩ .Y	107 335,77 107 3 35,77 107 3 3 3,10
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC REMOVED FOR RESET. OF X & REMOVED FOR RESET. OF X & REMOVED FOR RESET. OF X	KS IZAESSURIZ SEIJAHATÓNOFI IERARATÓN OF A IERARATÓN OF A IEROUT (GIODO LE IZ-NA-IGUE RIVS: (GIODO	LING MISSILE ( MISSILE ( M	61000 BUSL \$ <b>1000 BUSE</b> UP)	s (GROOMDZ FUR) S (GROOMD 7 FUR) FOR	REFE	RI	3 4 5 5	SCOBSE-I/ WIRS SOMERE ADDED SURVEYER CHIM	₩ .Y	ECP 535,77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC REMOVED FOR DESET. OF XL & REMOVED FOR STATIC FI INSTALLED FOR STATIC FIRM	KS IZAESSURIZ SEIDAMATÓN OF I TERARRITON OF I TROUT. (GIODO CROUT. (GIODO RIVIS. (GIODO NIG. (GIODOM L	21.005 MISSILE & I IZINIS MISSILE & UP, MISSILE & UP, MISS	61000 BUSE \$1000 BUSE UP) MD3)	s(shoomortur) s(shoomortur) FOR	REFE	RI	3 4 5 5	SCOBSE-I/ MAR SCHERE ADDED SUBJECT COMM	- Y	MES 33
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC REMOVED FOR JEAUNCH LOC & REMOVED FOR STATIC FI INSTALLED FOR STATIC FIR WINECTOR PIN LETTER	KS IZAESSURIZ SEIDAHATÓN OF I TERARRESSURI TROUT (GIODO CKOUT (GIODO LR I 9-NAET (GK RING: (GIODO IN L S	21.005 MISSILE & I IZINIS MISSILE & UP MIDE & UP, MIDE & UP, MIDE & UP, MIDE & UP, DIS, 63002	GIQOO BUSE SIDOO BUSE (UP) MDE)	s(shoomortur) s(shoomortur) FOR	REFE	RI	3 4 5 5	SCOBSE-I/ MAR SOMMER ADDED SURVENCE CHAN	. Y	ACH 533,777
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR STANT TH POWER FAILURE CUT-OFF & S F ADDED FOR LAUNCH LOC REMOVED FOR LAUNCH LOC E ADDED FOR RESET. OF NA E ADDED FOR STATIC FIN INSTALLED FOR STATIC FIN WINECTOR PIN LETTER ER CASE.	KS IZAESSURIZ SEIDAMOTIONOFI NKS PRESSURI IERARPIONOFA TROUT (GIOOO LR IZ-NAFIGK RING: (GIOOOM UG. (GIOOOMI S	LINE MISSILE & MISSILE & MISSILE & MISSILE & MISSILE & MISSILE & MISSILE COMPA SOCIAL	61000 BUSE 51000 BUSE (UP) 1403)	5 (GLOODMOTEUR) S(GLOODMOTEUR) FOR	REFE	RI	3 4 5 5	SCOBSE-I/ MAR SOMMER ADDED SUBJECT COMM	.Y	ACH 533,77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR STANT TH POWER FAILURE CUT-OFF & S & ADDED FOR LAUNCH LOC REMOVED FOR ARSET. OF XL & REMOVED FOR STATIC FIN INSTALLED FOR STATIC FIN WINECTOR PIN LETTER ER CASE OF CASE OF BLOCK DIAGRAM	KS IZAESSLAVZ SEIDAMATONOFI NKS PAESSUA IEMOUTOVOFA TAOUT. (GIOOO LA T3-NA-T(GK RITVG. (GIOOOM NG. (GIOOOME S	21,005 MISSILE & (27)145 MISSILE & UP MISSILE & UP MISSILE & UP MISSILE MISSILE SS & SSOOL	51000 BUSE \$1000 BUSE UP) MOB)	s (GROOMDI (UP) S (GROOMDI (UP) FOR	REFE	RI			.Y	ACT 33
E ADDED FOR START TAN POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S FADDED FOR LAUNCH LOC REMOVED FOR STATIC FI INSTALLED FOR STATIC FIR WINECTOR PIN LETTER ER CASE 040 SCHEMATIC, 075 BLOCK DIAGRAM MCATES RECORDER COM	KS IZAESSURIZ SEIDAMATANOFI NKS PRESSURI IERAQUIONOFA TROUT. (GIODO KRUT. (GIODO IR 13-NA-T(GK RIIVG. (GIODOM NG. (GIODOME S	UME MISSILE & IZINE MISSILE & MISSILE & MISSILE & UDS & UP DOMD4 & MISSI 0000004 & MISSI 0000004 &	51000 BUSE \$1000 BUSE UP) MOB)	s (GROOMDI FUR) S (GROOMDI FUR) FOR	REFE	RI		SCO352-11 MRS SOURCE COM	.Y	ACR 333.77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S REMOVED FOR START LOUGH 200 REMOVED FOR STATIC FI INSTALLED FOR STATIC FIR WINECTOR PIN LETTER ER CASE 040 SCHEMATIC, 075 BLOCK DIAGRAM MATIC NO SO2500 FOR ATOR	KS IZAESSLAVZ SEIDAMATIONOFI NKS PRESSURI IEMOUTINOFA TROUT (GIODON LR 13-NAFT(GK RITVG (GIODON) VIG (GIODON) S NECTIONS R	2/MB MISSILE & L MISSILE & UP MIDE & UP MIDE & UP MIDE & UP MIDE & UP OD MID4 & MISSIN D 5, 63002	51000 BUSE 51000 BUSE (UP) 94032)	s (GROOMDI FUR) S (GROOMDI FUR) FOR	REFE	RI	3 4 5 <b>E N</b>	SCO352-11 MAR SOMER ADDED SEQUENCE CHAR CLE () PA	. Y	ACR 333.77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S REMOVED FOR START TO REMOVED FOR START JO REMOVED FOR START FI INSTALLED FOR START FIR WINECTOR PIN LETTER ER CASE 040 SCHEMATIC, 075 BLOCK DIAGRAM MATIC NO SOLSOD FOR ATOR QTES DOUGLAS AIRCRAF	KS IZAESSURIZ SEIDAMATANOFI NKS PRESSURI IZABUTAVOFA TADUT (GIODO LR 13-NAFTGK RING (GIODOM UNG (GIODOM S S NECTRONS R T	2/ME MISSILE & L MISSILE & UP MIDE & UP MIDE & UP MIDE & UP OD MID4 & DOS 63002	51000 BUSE 51000 BUSE (UP) 94038)	5 (GROOMDZEUR) S(GROOMDZEUR) FOR	REFE	RI		SCOBSE-I/ MAR SOMERE ADDED SEQUENCE CHAR C.E. () NA	. <b>Y</b>	ACR 333.77
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S REMOVED FOR START AU REMOVED FOR STATIC FI INSTALLED FOR STATIC FIR WINECTOR PIN LETTER ER CASE 040 SCHEMATIC, 075 BLOCK DIAGRAM MATIC NO SO2500 FOR ATOR QTES DOUGLAS AIRCRAF	KS FRESSLAVE SEPANATONOF, NKS PRESSUR, TROUT, (GIODO CKOUT, (GIODO LR 19-NA-T(GK RING, (GIODON) S NECTIONS R T	2/ME MISSILE & MISSILE & MIDE & UP MIDE & UP MIDE & UP MIDE & UP OD MID4 & MIDE & UP DO S, 63002	51000 BUSE 51000 BUSE (UP) MOB)	s (GROOMDZEUR) s(GROOMDTEUR) FOR	REFE	RI	3.4 5 5		. <b>∀</b>	ACR 333
E ADDED FOR START TANI POWER FAILURE CUT-OFF & REMOVED FOR START TH POWER FAILURE CUT-OFF & S REMOVED FOR START TO REMOVED FOR START JOE REMOVED FOR START FI INSTALLED FOR START FI INSTALLED FOR START FIR WINECTOR PIN LETTER ER CASE 040 SCHEMATIC, 075 BLOCK DIAGRAM MATIC NO SO2SOD FOR ATOR QTES DOUGLAS AIRCRAF NECTIONS. AND FOR ALL PANELS	KS I-HESSLIRIZ SEIHHATONOF, NKS PRESSUR IENAQUIONOF A TOUT (GIODO LR 19-NA-E(GH RING (GIODON) NG (GIODON) S NECTIONS R T	2/ME MISSILE & MISSILE & MIDE & UP MIDE & UP MIDE & UP MIDE & UP OD MID4 & MIDE & UP DO S, 63002	51000 BUSE 51000 BUSE (UP) 94032)	s (GROCOMOZEUR) s(GROCOMOZEUR) FOR	REFE	RI			. <b>∀</b>	ACR 333.77
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#### OPERATING REQUIREMENTS AND LIMITATIONS

Frequently reviewed specifications and limitations applicable to operation of the LV-2A propulsion system are contained in this section.

FUEL PUMP INLET (RJ-1)

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The minimum required NPSH for starting at 0 to 120 F is 80 feet. The minimum required NPSH for nominal rated thrust operation at 0 to 120 F is 34 feet. The maximum allowable surge pressure at 0 to 120 F is 160 psig.

#### OXIDIZER PUMP INLET

At saturation temperature, (1) the minimum required net positive suction head (NPSH) for starting is 55 feet, (2) the minimum NPSH required for nominal rated thrust operation is 55 feet, and (3) the maximum allowable surge pressure is 160 psig.

GROUND AND FLIGHT LOADING CONDITIONS

#### Handling Load

The main and vernier engines shall withstand a maximum of 4 g handling loads applied in any direction.

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#### Flight Operation

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The engine system shall operate satisfactorily without permanent deformation or failure under the following specified loads:

- 1. Load of 15 g parallel to the direction of flight and 1 g perpendicular to the direction of flight
- 2. Load of 12 g parallel to the direction of flight and 1.25 g perpendicular to the direction of flight
- 3. Load of 10 g parallel to the direction of flight and 1.5 g perpendicular to the direction of flight
- 4. Load of 2.5 g parallel to the direction of flight and 3 g perpendicular to the direction of flight

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#### Critical Customer Connect Point Maximum Loading

The customer connect point maximum loading is as follows:

#### Attach Point* Allowable Loads $F_v = 63,000$ lb 5930-lb side load Mount Attach to Missile (Pt. 1) $F_{y} = 63,000$ lb 5930-lb side load Mount Attach to Missile (Pt. 2) $\vec{F_y} = 63,000 \text{ lb } 5930-1b \text{ side load}$ Mount Attach to Missile (Pt. 3) $\mathbf{F}_{\mathbf{v}} =$ LOX Inlet Duct 3,200 lb Fuel Inlet Duct 7,200 lb Actuator Attach Point ±10,000 lb axial force Aft End of Heat Exchanger 300 lb any direction Forward Attach Lug Heat Exchanger 380 lb any direction $\mathbf{F}_{\mathbf{y}} =$ Aft Attach Lug Heat Exchanger ±380 lb ± 50 lb F_x = F, = ±380 1b Main Oil Discharge 100 lb any direction LOX Seal Drain 50 lb any direction **Oil Seal Drain** 50 1b any direction

*Refer to coordinate system

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#### PNEUMATIC SUPPLY

The pneumatic supply as delivered to the main engine manifold will be MIL-N-6011 nitrogen, liquid and gas. The flows quoted are for the propulsion system requirements only. No allowance has been made for other applications.

- Standby: high-pressure nitrogen, 0.150 lb/min maximum is required at 3000 to 1000 psi for oxidizer pump seal purge and the engine control system bleed and leakage. Nitrogen temperature range is -65 to +160 F.
- Starting: high-pressure nitrogen, 4.0 lb maximum is supplied at 3000 to 1500 psi and at a temperature range of -65 to +160 F for oxidizer pump seal purge, engine start tank pressurization, and pneumatic control.
- 3. Flight operation: high-pressure nitrogen, 2.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for oxidizer pump seal purge, controls, and engine lubrication tank pressurization. Maximum flowrate is 0.0115 lb/sec.
- 4. Vernier engine solo flight: high-pressure nitrogen, 8.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for vernier tank pressurization and pneumatic control. Maximum flowrate is 0.89 lb/sec.

The regulated pneumatic pressure at the customer supply connect-point is 660 psia.

A nitrogen supply temperature of 70 F was assumed for the above computations.

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#### SECTION II: PROPULSION SYSTEM PERFORMANCE

#### STEADY-STATE PERFORMANCE

Steady-state performance values presented in this section were obtained from production engine test results. Run-to-run deviations include random instrumentation errors and run-to-run nonrepeatability. The actual component differences are depicted in the engine-to-engine deviations.

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#### RATED MAIN ENGINE PERFORMANCE

The main engine nominal performance values and attendant variations at sea-level standard temperature and pressure, rated thrust and rated mixture ratio appear in Table 5. The vernier performance values were analytically determined using a typical vernier system downstream of the customer connect points. Since vernier performance depends upon the pressure supplied by the main engine, it will not exactly agree with rated values obtained from vernier production testing. A performance schematic depicting relative positions of flow and pressure data is presented in Fig. 6.

Run-to-run deviations in engine thrust and mixture ratio, and run-to-run and engine-to-engine deviations in specific impulse for the main engine are presented in Table 6.

Information regarding effects of nitrogen dilution on engine performance is included for application for analysis in the event of a suspected occurrence. Performance shifts of sea-level engine specific impulse and thrust due to nitrogen dilution of LOX presented in Fig. 7 and 8 were based on test results conducted on an engine system other than, but considered sufficiently descriptive of, the Thor. Empirically determined effects on c*,  $C_F$ , gas generator temperature and LOX density due to nitrogen dilution were imposed on nominal engine data to generate the figures.

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#### TABLE 5

## NOMINAL MAIN ENGINE PERFORMANCE VALUES AT SEA-LEVEL RATED THRUST AND MIXTURE RATIO

		Standard	Deviation
Parameter	Nominal Value	Engine- to-Engine (S _{EE} )	Run-to-Run (S _{RR} )
Engine			
Oxidizer (LOX) Density, lb/cu ft Fuel (RJ-1) Density, lb/cu ft Thrust, pounds Specific Impulse, seconds Mixture Ratio (o/f), including vernier flow	71.38* 53.17* 170,000* 252.4 2.15*	0.62	0.30
Thrust Chamber	1		
Thrust, pounds Specific Impulse, seconds	169,500 257.5	0.62	0.31
injector end, ft/sec Thrust Coefficient (C ₂ ).	5958	15.4	9.5
injector end Chamber Pressure, injector end,psia	1.391 594.3	0.0038 1.53	0.0021 0.92
Characteristic Velocity, nozzle stagnation, ft/sec Thrust Coefficient nozzle	5517.		
stagnation Chamber Pressure, nozzle	1.502		
stagnation, psia c* Efficiency, % C _F Efficiency, % Benellent Elementor lb/see	550.3 95.5 101.2	0.25 0.25	0.15 0.15
Oxidizer Fuel Mixture Ratio (o/f)	456.3 201.9 2.260	$1.11 \\ 0.48 \\ 0.0016$	0.54 0.26 0.0008
Main Fuel Orifice Pressure Drop,psi at 190 lb/sec and 53.17 lb/cu ft Orifice Diameter, inches	55.6 49.2 2.74	10.3	1.8

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## TABLE 5

## (Continued)

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		Standard	Deviation
		Engine_	
	Nominal	to-Engine	Run-to-Run
Parameter	Value	(S _{EE} )	(S _{RR} )
Propellant Pumps			
LUX Pump			
Inlet Pressure (total), psia	53.0^		
Discharge Pressure (total), psia	862.	14.8	2.9
Developed Head, feet	1641.	11.8	6.7
Weight Flow, 1b/sec	469.9	1.14	0.56
Volume Flow, gpm	2955.	7.2	3.5
Speed, rpm	6252.	26.8	8.4
Shaft Power, bhp	1772.	16.2	8.6
Efficiency, %	79.1		
Fuel Pump			
Inlet Pressure (total), psia	48.0*		
Discharge Pressure (total), psia	902.	14.8	2.9
Developed Head, feet	2307.	39.8	7.8
Weight Flow, 1b/sec	217.2	0.53	0.26
Volume Flow, gpm	1833	4.50	2.18
Speed, rpm	6252.	26.8	8.4
Shaft Power, bhp	1272.	22.0	5.24
Efficiency, %	71.6		
Turbine	-		
Turbine Shaft Power, bhp	3136.	31.	13
Turbine Inlet Temperature, F	1203.	10.6	3.0
Turbine Gas Flow, lb/sec	15.21	0.16	0.05
Turbine Exhaust Pressure (static),			
psia	23.6	1.69	0.25
Turbine Inlet Pressure (total),psia	515 <i>.</i> 6	4.8	2.3
Turbine Pressure Ratio (total psia inlet/static exhaust)	21.8		

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TABLE	5
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(Continued)

		Standard	Deviation
Parameter	Nominal Value	Engine- to-Engine (S _{EE} )	Run-to-Run (S _{RR} )
Gas Generator	, -		
Gas Generator Chamber Pressure, injector end, psia LOX Bleed Pressure, psia Fuel Bleed Pressure, psia Total Propellant Flow **, lb/sec LOX Flow**, lb/sec Fuel Flow**, lb/sec Mixture Ratio (o/f) Fuel Orifice Pressure Drop, psi at 10.5 lb/sec and 53.17 lb/cu ft Orifice Diameter, inch LOX Orifice Pressure Drop, psi at 3.5 lb/sec and 71.38 lb/cu ft	541.4 788. 888. 15.21 3,73 11.48 0.325 167.3 139.9 0.530 86.3 75.9	5.5  0.16 0.04 0.14 0.004  14.5	1.6  0.05 0.01 0.04 0.001  1.3
Verniers (Pump-Fed)			- - - -
LOX Flow, lb/sec Fuel Flow, lb/sec Vernier Total Flow, lb/sec Mixture Ratio (o/f) LOX Customer Connect Pressure, psia Fuel Customer Connect Pressure,psia Heat Exchanger LOX Flow, lb/sec	6.56 3.61 10.17 1.82 762. 701. 3.17	0.054 0.035 0.070 0.019 9.0 7.9 0.045	0.019 0.011 0.026 0.006 3.3 2.6 0.046

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### TABLE 5

## (Continued)

		Standard Deviation			
Parameter	Nominal Value	Engine- to-Engine (S _{EE} )	Run-to-Run (S _{RR} )		
Verniers (Solo)					
LOX Flow, lb/sec	5.38	0.028	0.014		
Fuel Flow, 1b/sec	3.01	0.018	0.006		
Vernier Total Flow, lb/sec	8.39	0.046	0.020		
Mixture Ratio (o/f)	1.78	0.007	0.006		
LOX Customer Connect Pressure, psia	575.	4.40	2.1		
Fuel Customer Connect Pressure, ps	ia 530.	4.20	1.20		
Engine Regulator Pressure Setting,	-				
psia	660.				

NOTE: All pressures were measured with a static tap, unless designated as total. Pressure designated as total were calculated from a static measurement.

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* Rated value

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**Calculated from turbine inlet temperature and pressure

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#### TABLE 6

## PERFORMANCE DEVIATIONS, YLR79-NA-13 THOR MAIN ENGINES (Data Based on 47 Runs Involving 23 Engines)

Paramatan	Specified or Moon Value	Derriction d
rarameter	Mean value	Deviation, 70
Engine Thrust		
Specified, pounds	170,000 <b>.±3%</b>	
Run-to-Run Deviation*		0.25
Run-to-Run, 95% Tolerance		0.61
<u>Mixture Ratio</u>		
Specified	2.15 ±1.02%	
Run-to-Run Deviation*		0.23
Run-to-Run, 95% Tolerance		0.56
Specific Impulse**		
Specified Minimum, seconds	249.	
Mean	252.4	
Run-to-Run Deviation*		0.12
Run-to-Run, 95% Tolerance		0.29
Engine-to-Engine Deviation		0.25
Engine-to-Engine, 95% Tolerance		0.61
<b>Over-all Standard Deviation</b> $***$		0.27
<b>Over-all, 95% Tolerance</b>		0.63

* Run-to-run standard deviation

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** Specific impulse values are quoted at rated thrust and mixture ratio ***Run-to-run and engine-to-engine standard deviation. This method of combination allows a conservative estimation.

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Figure 7.

Effects of Liquid Nitrogen Dilution on Sea Level Engine Specific Impulse

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Figure 8. Effects of Liquid Nitrogen Dilution on Sea-Level Engine Thrust

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#### RATED VERNIER ENGINE PERFORMANCE

Statistical analyses of LR101-NA-11 vernier engine data are presented in Table 7, covering mean performance, run-to-run, and engine-to-engine variations. The data are based on 94 tests on 47 acceptance engines. RP-1 was used for all tests. Data were reduced to sea-level standard temperature and pressure rated thrust, mixture ratio, and propellant inlet pressures prior to statistical analysis. The data reduction program computes orifices required to give rated thrust and mixture ratio at tank-fed conditions. With these orifices, the program then computes what thrust and mixture ratio would be under pump-fed conditions.

The following standard conditions are used by the data reduction program:

Rated Parameter	Tank-Fed	Pump-Fed
Thrust, pounds	830	
Mixture Ratio	1,80	
LOX Inlet Pressure, psia	540	660
Fuel Inlet Pressure, psia	510	636
LOX Specific Gravity, lb/cu ft	66.27	70.73
Fuel Specific Gravity, 1b/cu ft	50,48	50.48

A schematic of vernier operation under pump-fed conditions (with RJ-1 fuel) appears in Fig. 9.

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#### TABLE 7

## NOMINAL LR101-NA-11 VERNIER ENGINE PERFORMANCE AND PERFORMANCE DEVIATIONS

Parameter	Mean Value	S _{EE}	Ċ _{VEE}	S _{RR}	C _{VRR}
Tank-Fed			-		
Specific Impulse, seconds	198.7	1.92	0.97	1.12	0.56
Characteristic Velocity (c*), Injector End, ft/sec	4942	69.9	1.41	29.1	0.59
Thrust Coefficient (C _F ), Injector End	1.294	0.007	0.55	0.005	0.35
Chamber Pressure, Injector End, psia	305.4	2.64	0.86	0.85	0.28
Chamber Pressure, Nozzle, psia	298.		, <b>-</b> -		
LOX_Weight Flow, lb/sec	2.68		. – –		
Fuel Weight Flow, lb/sec	1.49		' <u>-</u> ` -		
LOX Orifice Differential Pressure, psi	39.8	7.96	20:0	2.97	7.44
Fuel Orifice Differential Pressure, psi	27.6	7.68	27.8	3.33	12.05
Pump-Fed					
Thrust, pounds	1017	5.64	0.55	4.19	0.41
Mixture Ratio	1,803	0.010	0.54	0.011	0.61
Specific Impulse, seconds	209.8	2.21	1.05	0.83	0.39
c*, Injector End, ft/sec	5054.	51.5	1.02	21.0	0.42
C _F , Injector End	1.336	0.005	0.39	0.005	0.37

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# TABLE 7

## (Continued)

Parameter	Mean Value	s _{EE}	C _{VEE}	$\mathbf{s}_{\mathbf{RR}}$	C _{VRR}
Chamber Pressure, Injector End, psia	362.5	3.39	0.93	1.70	0.47
Chamber Pressure, Nozzle, psia	353.				
LOX Weight Flow, lb/sec	3.12				
Fuel Weight Flow, 1b/sec	1.73				

 $\mathbf{S}_{\mathbf{E}\mathbf{E}}$  Engine-to-engine standard deviation

C_{VEE} Engine-to-engine coefficient of variation (standard deviation expressed as percentage of the mean)

 $S_{RR}$  Run-to-run standard deviation

C_{VRR} Engine-to- engine coefficient of variation (standard deviation expressed as percentage of the mean)

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#### INFLUENCE COEFFICIENTS

#### LINEARIZED SOLUTIONS

Engine influence coefficients result from a linearized solution of a set of steady-state equations which describe the operation of an engine. Each influence coefficient is expressed in percentage from, and represents the effect that a 1% increase in an engine independent variable will have on an engine dependent variable. A coefficient preceded by a positive (+) sign (or no sign) indicates that an increase in the independent variable results in an increase in the dependent variable; a coefficient preceded by a negative (-) sign indicates that an increase in the independent variable results in a decrease in the dependent variable.

#### **ILLUSTRATION**

Figure 10 is a portion of a typical table of engine influence coefficients. This table is in the form as printed by a high-speed digital computer. The symbols E 01, E 04, etc., placed after the nominal values in the table represent powers of 10. Hence 1.4696E 01 is equivalent to 14.696; 6.0000E 04 is equivalent to 60,000; etc.

#### APPLICATION

These influence coefficients may be applied to two different situations; (1) calculations involving an engine type, or (2) calculations involving a specific engine.

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A ONE-PERCENT INCREASE IN A	NY ONE	OF THE D	NDEPENDEN T	VARIABLES	CAUSES	THE
FOLLOWING PERCENTAGE CHANGE	IN ANY	ONE OF	THE DEPENDE	INT VARIABI	LES.	
- INDEPENDENT VAR	IABLES-	•				
1. ATMOSPHERIC PRES		1.4696E	01			
2. FUEL DENSITY		5.0450E	01			
3. OXID DENSITY		7.1380E	01			
4. FUEL PUMP INLET PRES -		7.7000E	01			
5. OXID PUMP INLET PRES -		5.3000E	01			
6. C* CORRECTION			-	•		
	·1-	2	- 3-	4-	5-	6-
-DEPENDENT VARIA	BLES-					
ENGINE THRUST 6 0000E 0	4					
	0 4556	0 53	26 0.0 <del>7</del> 0	3 0 0576	5 0	0 6202
FNGTNE ISP 2 3000F 0	0.400	0.99			, U	0.0494
		0.14		1 0 0190		1 1600
	0.4420	0.14	0.034	1 0.0102	2 0	1.10//
ENGINE MR $= 2.2700E$ U	0 0070	-0.10	5L 0 70)	6 0 000		0.1371
	0.00 <u>3</u> 9	-0.40	<u>54</u> 0.501		, U, V	0,41,14
ENGLINE FUEL FLOW- 7.9770E 0	0 000€	0.65	00 0 160		, <u>,</u>	0.00(0
	0.0090	0.05	50 -0.108	o 0.024)		-0.2208
ENGINE OXID FLOW- 1.8110E 0	2					
	0.0145	0.26	74 0.125	6 0.0461	. 0 •	0.6462

Figure 10 . Sample Table of Influence Ceofficients as Printed by High-Speed Digital Computer

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#### Calculations Involving an Engine Type

Suppose it were desired to determine the thrust of the engine described by the sample table of influence coefficients when operated under the following conditions:

1. Autospherre pressure = 1.40 p	818
2. Fuel density $= 50.45$	lb/cu ft
3. Oxidizer density = 69.55	lb/cu ft
4. Fuel pump inlet pressure = 69.30	psia
5. Oxidizer pump inlet pressure = 59.55	psia

Because the influence coefficients are linear, the total effect of several influences acting simultaneously on an engine can be determined by adding the individual effects of each influence. The change in engine thrust would be

$$\frac{F_{E} - F_{E_{i}}}{F_{E_{N}}} = \frac{P_{a} - P_{a_{i}}}{P_{a_{N}}} (F_{P_{a}}) + \frac{\rho_{F} - \rho_{F_{i}}}{\rho_{F_{N}}} (F \rho_{F}) + \frac{\rho_{o} - \rho_{o_{i}}}{\rho_{o_{N}}} (F \rho_{o}) + \frac{P_{F} - P_{F_{i}}}{P_{F_{N}}} (F_{P_{F}}) + \frac{P_{o} - P_{o_{i}}}{P_{o_{N}}} (F_{P_{o}}), \qquad (1)$$

Where  $F_E$ ,  $P_a$ ,  $\rho_F$ ,  $\rho_o$ , etc., are the actual values of these parameters for the problems considered.

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 $F_{E_i}$ ,  $P_{a_j}$ ,  $P_{F_i}$ ,  $P_{o_i}$ , etc., are the initial or base values of these parameters.

 $F_{E_N}$ ,  $P_{a_N}$ ,  $P_{F_N}$ ,  $P_{o_N}$ , etc., are the nominal values of these parameters, listed in the table of influence coefficients.

 ${}^{F}P_{a}$ ,  ${}^{F}\rho_{F}$ ,  ${}^{F}\rho_{o}$ , etc., are the influence coefficients for engine thrust found in the appropriate columns of the table of influence coefficients.

For calculations involving an engine type, the initial values would be the same as the nominal values, and  $F_{E_1} = F_{E_N}$ ,  $P_a = P_a$ ,  $\rho_{F_1} = \rho_{F_N}$ ,  $\rho_o = \rho_{o_N}$ , etc.

The calculation for the example stated above would be as follows:

$$\frac{F_{E} - 60,000}{60,000} = \left(\frac{1.40 - 14.696}{14.696}\right) \left(-0.4556\right) + \left(\frac{50.45 - 50.45}{50.45}\right) \left(+0.5326\right) \\ + \left(\frac{69.55 - 71.38}{71.38}\right) \left(+0.0703\right) + \left(\frac{69.30 - 77.00}{77.00}\right) \left(+0.0576\right) \\ + \left(\frac{59.55 - 53.00}{53.00}\right) \left(0\right)$$

$$\frac{F_E - 60,000}{60,000} = -0.9047 (-0.4556) + 0(+0.5326) \\ -0.0256 (+0.0703) - 0.1000 (+0.0576) \\ +0.1236 (0) = +0.4046 \text{ or } +40.46\%$$

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Therefore:

 $F_E = +0.4046 (60,000) + 60,000$  $F_E = +24,276 + 60,000 = 84,276$  pounds

The incremental thrust change has been found to be +24,276 pounds for the conditions stated, yielding a final engine thrust of 84,276 pounds.

#### Calculations Involving a Specific Engine.

When the values of actual engine parameters differ from those used as nominal values in the table of influence coefficients, the "delta method" of application of influence coefficients is used. This procedure consists of computing an incremental change of variables rather than a percentage change of these variables. The incremental change is then applied to the actual engine value. This effect can be accomplished by using Eq. (1) if the quantities  $F_{E_i}$ ,  $P_{a_i}$ ,  $\rho_{F_i}$ ,  $\rho_{o_i}$ , etc., are defined as the actual engine values of these parameters. All other quantities are as defined previously.

#### NONLINEAR CORRECTIONS

A special computational procedure has been devised to extend the usefulness of engine influence coefficients. This technique is used to allow nonlinear corrections to be made for certain parameters where the linear approximation is not sufficiently accurate. An example of this method is the c* correction  $(C_{c*})$ . In this case, a plot of  $C_{c*}$  vs the change in engine mixture ratio is included with the table of influence coefficients. Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

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A typical plot of these parameters is shown below:

$$\left(\frac{\mu_{\text{E}} - \mu_{\text{E}_{N}}}{\mu_{\text{E}_{N}}}\right)_{160} = \left(\begin{array}{c} \frac{\text{Change in Engine Mixture Ratio}}{\text{Nominal Engine Mixture Ratio}}\right)_{100\%}$$



The change in engine mixture ratio is computed for the changes in atmospheric pressure, propellant densities, etc., and with the assumption that the c* correction is zero. With this change in engine mixture ratio, the c* correction is read from the curve. This value of c* correction is used with the other independent variables to compute the changes in the remaining dependent variables.

For example, if the change in engine mixture ratio accompanying the  $\pm 40.46\%$  thrust change in the preceding example were -0.62%, then the c* correction from the curve is -0.10%. The true change in engine thrust is therefore:

(% change in  $F_E = +40.46 - 0.10 (+0.6494) = +40.40\%$ )

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Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

#### LV-2A INFLUENCE COEFFICIENTS

Current influence coefficients for the LV-2A propulsion system are presented in Tables 8 and 9. Table 8 includes the additional effect of fuel temperature on system performance while considering fuel density a constant. Any density change, therefore, is considered independently.

The effects of engine mixture ratio on  $c^*$  in terms of a correction appear in Fig. 11.

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#### TABLE 8

## INFLUENCE COEFFICIENTS FOR THE YLR79-N/ AND IRICI-NA-11 VERNIER ENGINI

# A 1% increase in any one of the inde following percentage change in any o

## Independent Var

1.	Atmospheric Pressure, psia	14.696
2.	Fuel Density, 1b/cu ft	53.170
3.	Oxidizer Density, 1b/cu ft	71.380
4.	Fuel Pump Inlet Pressure, psia	48.000

Dependent Variables	Nominal Values	1
Engine Thrust Without Verniers, pounds	170,000.	-0.1472
Engine Specific Impulse Without Verniers, seconds	252.26	-0.1404
Engine Mixture Ratio With Verniers	2.1500	-0.0001
Engine Fuel Flow With Værniers, 1b/sec	217.13	-0.0067
Engine Oxidizer Flow With Verniers, 1b/sec	466.83	-0,0068
Vernier Oxidizer Flow, 1b/sec	6.4860	-0.0056
Vernier Fuel Flow, lb/sec	3.5637	-0.0058
Vernier Thrust, pounds	2112.0	-0.1702
Thrust Chamber Nozzle Stagnation Pressure, psia	551.53	-0.0069
Fuel Pump Outlet Pressure, psia	901.35	-0.0091
Oxidizer Pump Outlet Pressure, psia	861.27	-0.0089
Pump Speed, rpm	6260.8	-0.0051



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TABLE 8

## FOR THE YLR79-NA-13 THOR MAIN ENGINE

11 VERNIER ENGINES (PUMP-FED)

# y one of the independent variables causes the e change in any one of the dependent variables

Independent Variables

. . . . . . . . . . . .

	14.696 53.170 71.380 48.000	5. Oxidiz 6. c* Cor 7. Fuel T	er Pump Inle rection emperature	et Pressure, (at constant	psia density), F	53.000 1.0000 60.000	
ıal		0	7	I.	=	6	~
		<u>_</u> _0 6862	<u>_</u> 1_8030	-0 0178	0.0685	1 0844	-0 0039
,00 <b>.</b> 16	-0.1472	-0.0736	0.9998		0.0085	1 1346	-0.0001
10	-0.0001	-1.6245	1.6197	-0.0533	0.0614	-0.0374	-0.0256
3	-0.0067	0,5003	0.4707	0.0204	0.0179	-0.0178	0.0138
3	-0,0068	-1.1242	2.0903	-0.0329	0.0794	-0.0552	-0.0119
0	-0,0056	-0.7031	1.6793	-0.0193	0.0563	0.4534	-0.0060
7	-0.0058	0.3569	0.6199	0.0085	0.0256	0.3638	0.0076
0	-0.1702	-0.6315	1.7772	-0.0176	0.0604	0.5157	-0.0046
3	-0.0069	-0.5675	1.5463	-0.0145	0.0588	0.9510	-0.0029
5	-0.0091	-0.3755	1.3415	0.0044	0.0509	0.5976	0.0077
7	-0.0089	-1.0884	2.0517	-0.0304	0.0897	0.6184	-0.0093
8	-0.0051	-0.6687	0.6730	-0.0189	0.0256	0.2659	-0.0061

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SNOLTIO			psia 510.00 re, 540.00	Ŋ	897 0.7599	635 0.4086	400 1.2114	503 -0.4275	97 0.7839
TABLE 9 OR THE IR101-NA-11 VERNIER ENGINE OFERATING AT SOLO CON any one of the independent variables causes the tage change in any one of the dependent variables. Independent Variables		essure, y Pressu	4	. 0°0	-0.2(	$-1.2^{l}$	1.15	-0.08	
		ıt Supply Pr ellant Suppl	М	0.3285	0.1767	0.5237	-0.1848	0.3389	
	iables	el Propellar idizer Prope ia	<b>CI</b>	0.0358	-0.1051	-0.4947	0.4589	-0.0358	
	spendent Var	5 4. Fu		-0.2082	-0.2082	0°	°0	°0	
	Inde	ia 14.696 50.480 ft 66.270	Nominal Values	830.00	198.27	1.8000	1.4951	2.6912	
INFLUENCE COEFFICIENTS F	A 1% increase in following percen		Atmospheric Pressure, ps. Fuel Density, lb/cu ft Oxidizer Density, lb/cu	ependent Variables	er Thrust, pounds	rr Specific Impulse, Is	ır Mixture Ratio	r Fuel Flow, lb/sec	r Oxidizer Flow, l <b>b/se</b> c

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#### TRANSIENT CHARACTERISTICS

The following portion of this report is devoted to a detailed description of YLR79-NA-13 main engine and LR101-NA-11 vernier engines transient operating characteristics during starting, stabilization, and cutoff. Considered are electromechanical sequencing, engine systems major flows and pressures, and start tanks refill operation. It should be noted that all relationships are typical of static firing operation but are considered good approximations of missile launching conditions as well. Data from simulated missile starts were used where available.

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START AND CUTOFF SEQUENCE

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The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are electrically sequenced for appropriate start and cutoff operation. All valves are pneumatically operated with a 660 psia regulated gaseous nitrogen supply. Pneumatic restrictors (orifices) are used in conjunction with the valves to provide desired actuation delay and movement times.

Figures 12 and 13 schematically represent electromechanical start and cutoff sequence requirements. Figure 14 displays the average time function of the sequence of events during start and cutoff.

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#### START AND CUTOFF TRANSIENT CHARACTERISTICS

The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are ignited by pyrophoric cartridges with an integrated start-vernier solo tank system. Main chamber ignition flame is established by LOX supplied to the injector under tank head, along with start-tank-supplied igniter fuel to spray disks located in each of the six baffled compartments. No chamber fuel jacket prefill is used. Gas generator ignitors are pyrotechnic.

Figures 15 through 17 portray typical start characteristics (primarily propellant flows) of the pump main chamber, and auxilliary systems. Figures 18 and 19 are typical oscillographic recordings (primarily pressures) of an engine start and cutoff, respectively. Vernier engines were simulated during this test. Estimated prelaunch propellant consumption (ignition start to 90% chamber pressure) and start tank refill operation are presented in Tables 10 and 11.

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Figure 19. Main Engine Typical Cutoff Oscillographic Recording

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### TABLE 10

## PRELAUNCH PROPELLANT CONSUMPTION*

	Propellant		
System.	LOX, pounds	Fuel, pounds	
Vernier	6.17	4.52	
Gas Generator	1.94	5.38	
Ignition		3.12	
Total Start Tank	8.11	13.02	
Heat Exchanger	6.53		
Main Chamber	305	130	

*Based on static test performance with 15 to 30 minute LOX chilldown

### TABLE 11

### START TANK REFILL CHARACTERISTICS

	Normal Test Stand Start		Missile Simulated Start		Overboard
Start Tank	Refill Time*, seconds	Refill Rate, lb/sec	Refill Time*, seconds	Refill Rate, lb/sec	Flowrate, lb/sec
0xidizer	22	0.37	50	0.19	0.20
Fuel	60	0.20	60	0.20	0.02

*Time from 90% chamber pressure to refill indication

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#### STABILIZATION CHARACTERISTICS

Gradual stabilizing of pressure-flow parameters under self-sustained operating conditions (bootstrapped power package) is a characteristic of liquid propellant engines with orificed control of gas generator propellant supply flows. The main engine generally attains stabilized operation 30 seconds from 90%. Varying test conditions and random engine hardware influences can, however, result in stabilization times ranging from 15 to 35 seconds from 90%.

The average thrust buildup from 90% to stabilized operation is shown in Fig. 20. Figures 21 through 23 present typical pump, chamber, and auxilliary systems stabilization characteristics (including vernier engines). The test from which the latter relationships were obtained stabilized in 20 seconds, which is not an abnormal condition.

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