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R-5214

DESIGN INFORMATION REPORT FOR THE
THOR YLR79-NA-13 MAIN ENGINE AND
LR101-NA-11 VERNIER ENGINES

ROCKETDYNE
A DIVISION OF NORTH AMERICAN AVIATION, INC.

6633 CANOGA AVENUE
CANOGA PARK, CALIFORNIA

Contract AF04(695)-306

Part I, Item 2b as
Amended by Item VI of
Request For Service
Order 306-64-03

PREPARED BY

Rocketdyne Engineering
Canoga Park, California

APPROVED BY

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Atlas/Thor Program Manager

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JAN 30 1964
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NO. OF PAGES 79 & viii

REVISIONS

DATE 30 July 1963

DATE	REV. BY	PAGES AFFECTED	REMARKS
30 Jan 1964	WNP	7	Updated Drawing 104653

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FOREWORD

This Design Information Report was prepared in compliance with AF04(695)-306, Part I, Item 2b as amended by Item VI of Request for Service Order 306-64-03.

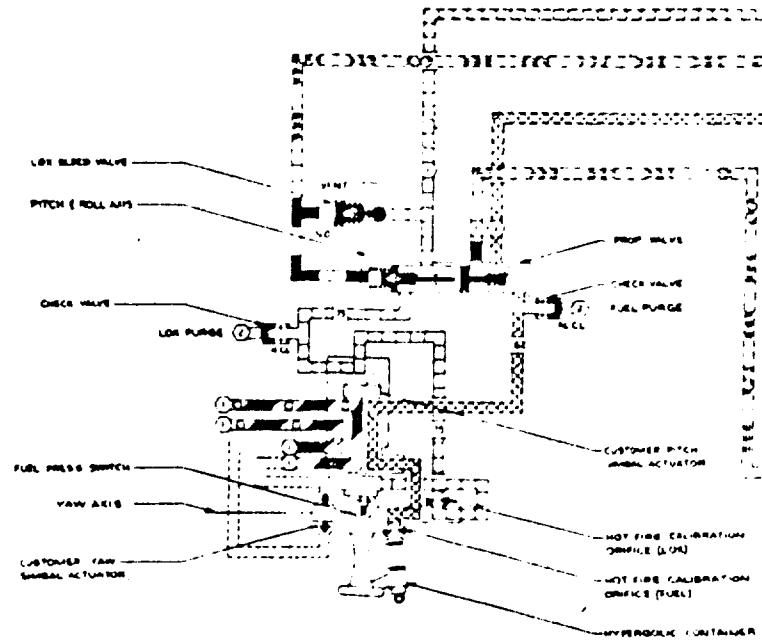
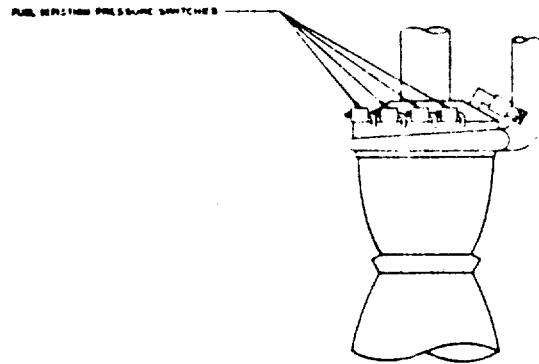
ABSTRACT

This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LRI01-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

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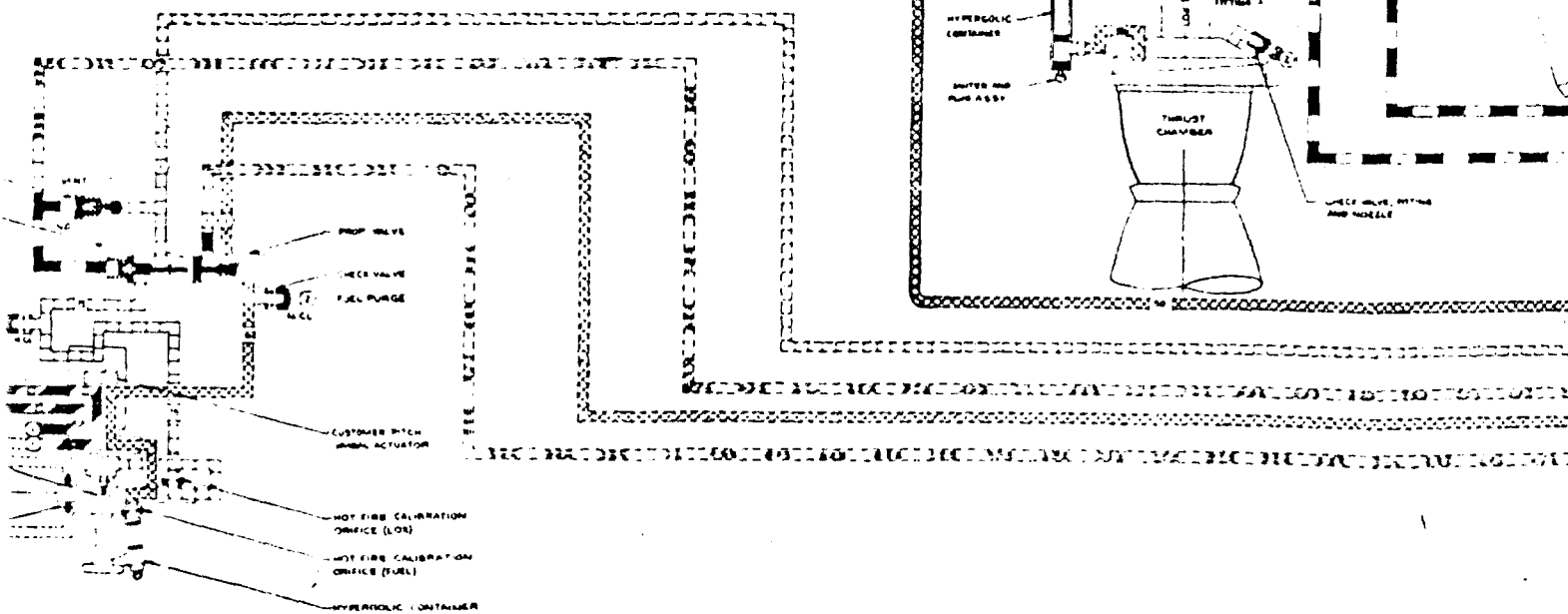
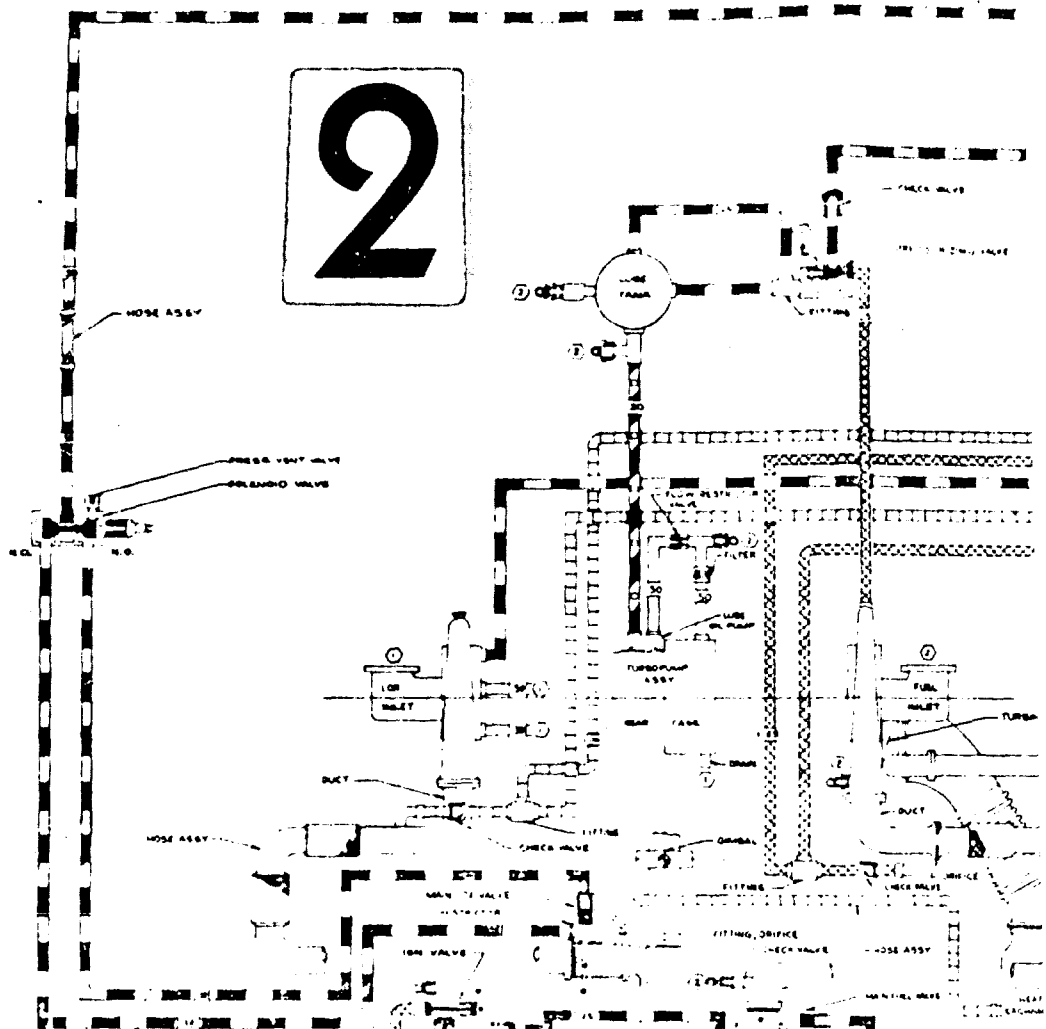
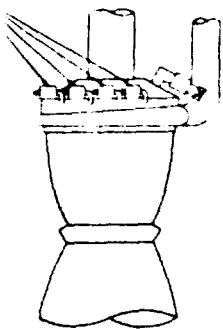
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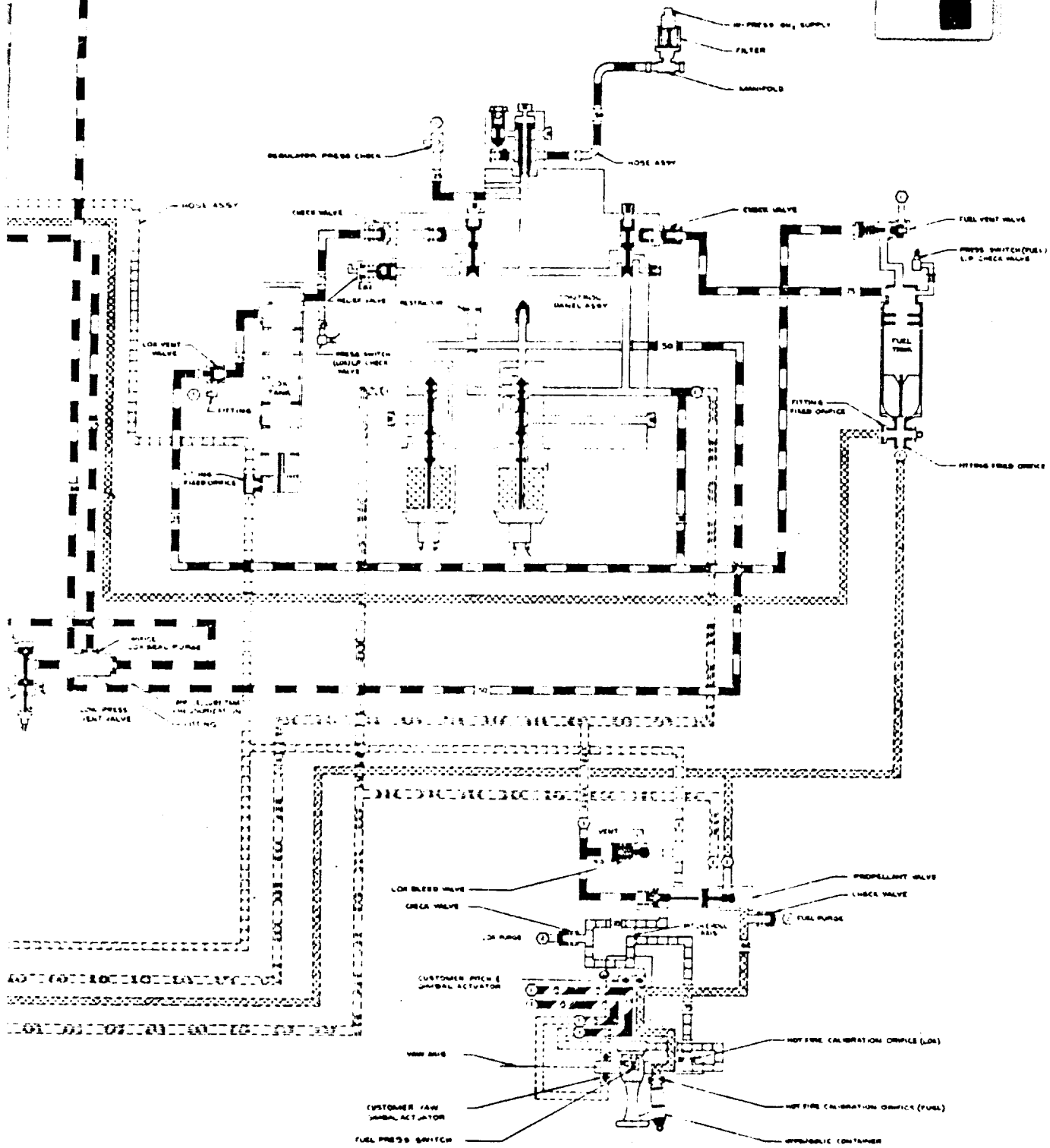


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REVISIONS WITH CHANGES			
1. REVISED FORMAT			
2. ADDED SCHEMATIC CODE			

SCHEMATIC CODE

HOT GAS	□	□	□	□
PNEUMATIC	□	□	□	□
HYDRAULIC	□	□	□	□
LUBE	□	□	□	□
OR-GAS	□	□	□	□
FUEL	□	□	□	□

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① 2 SERVICE CONNECTIONS
② CUSTOMER CONNECTIONS

SEE WIRE CHARTER PAGES

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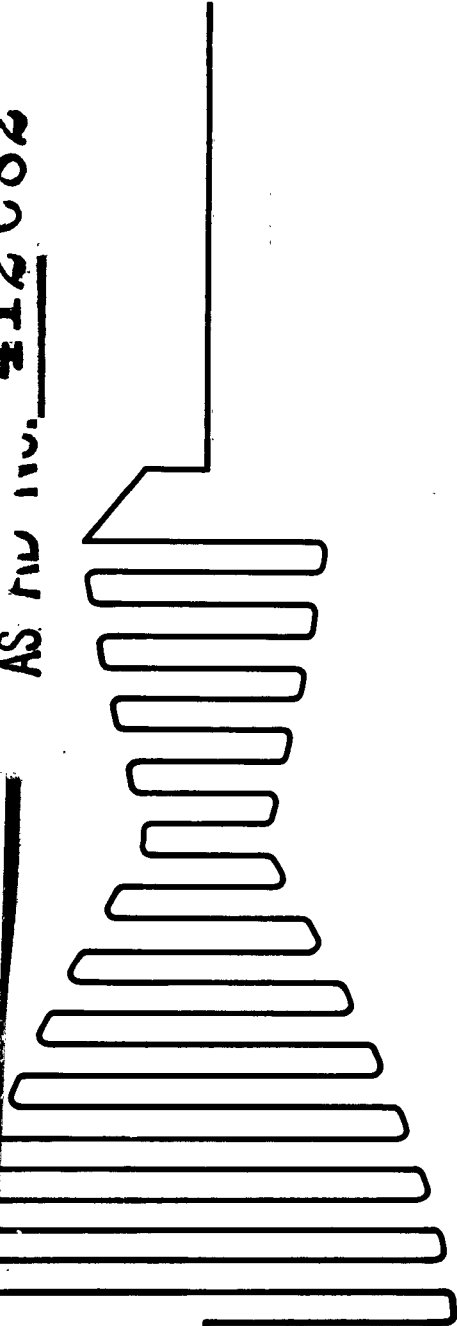
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A DIVISION OF NORTH AMERICAN AVIATION, INC.
CANOGA PARK, CALIFORNIA

FORM R USE REV 6-2

R-5214

DESIGN INFORMATION REPORT FOR THE
LV-2A PROPULSION SYSTEM
(YLR79-NA-13 Main Engine and
LRL01-NA-11 Vernier Engines)

ROCKETDYNE

A DIVISION OF NORTH AMERICAN AVIATION, INC.

6633 CANOGA AVENUE
CANOGA PARK, CALIFORNIA

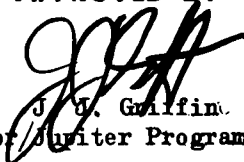
Contract AF04(695)-306

Part I, Item 2b as
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Order 306-63-01

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DATE 30 July 1963

DATE	REV. BY	PAGES AFFECTED	REMARKS

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This report consists of three major sections: (1) a description of the LV-2A propulsion system, consisting of the YLR79-NA-13 main engine and the LR101-NA-11 vernier engines, (2) installation and geometry information, and (3) performance data.

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INTRODUCTION

The function of this report is to compile in handbook form the various items of engine design information in which the customer has expressed prime interest. It is also intended as an aid to design and to ensure compatibility of missile structure and the LV-2A propulsion system.

This report is not intended to supersede or duplicate existing model specification or Rocketdyne Field Service manuals.

Additions and revisions will be issued periodically to maintain this report on a current basis.

SECTION I: PROPULSION SYSTEM DESCRIPTION
AND OPERATING REQUIREMENTS

PROPULSION SYSTEM DESCRIPTION

The LV-2A propulsion system (Fig. 1) is composed of a booster main engine (Air Force designation YLR79-NA-13) and two vernier engines (Air Force designation LR101-NA-11) which provide roll control and finite impulse adjustment at the end of flight. The complete propulsion unit is a liquid bipropellant system and operates on liquid oxygen and RJ-1 hydrocarbon fuel. The main engine has a maximum over-all length of 142.587 inches and a maximum envelope diameter of 76.117 inches. The engine is rated to deliver a thrust of 170,000 pounds under sea-level conditions for a mainstage duration of 175 seconds. An additional 2120 pounds total thrust is developed by the two vernier engines during pump-fed operation and 1660 pounds total thrust during tank-fed operation for approximately 9 seconds after main engine cutoff.

Both the main and vernier engines are of the single-start, fixed-thrust type with no provision for restarting the engines or for intermediate thrust control. System propellant flowrates are controlled exclusively by orificing. All thrust chambers are gimbal-mounted for trajectory control and adjustment. The main engine thrust chamber is provided with a baffled injector. Ignition in all chambers is by means of hypergolic fluid. The entire propulsion system is controlled by an electrical system and a pneumatic system. Nitrogen gas is used in the latter system to operate all pneumatically controlled valves. Electrical power to control the engines is supplied from an external source until the missile is airborne, after which the missile's electrical system supplies the required electrical power.

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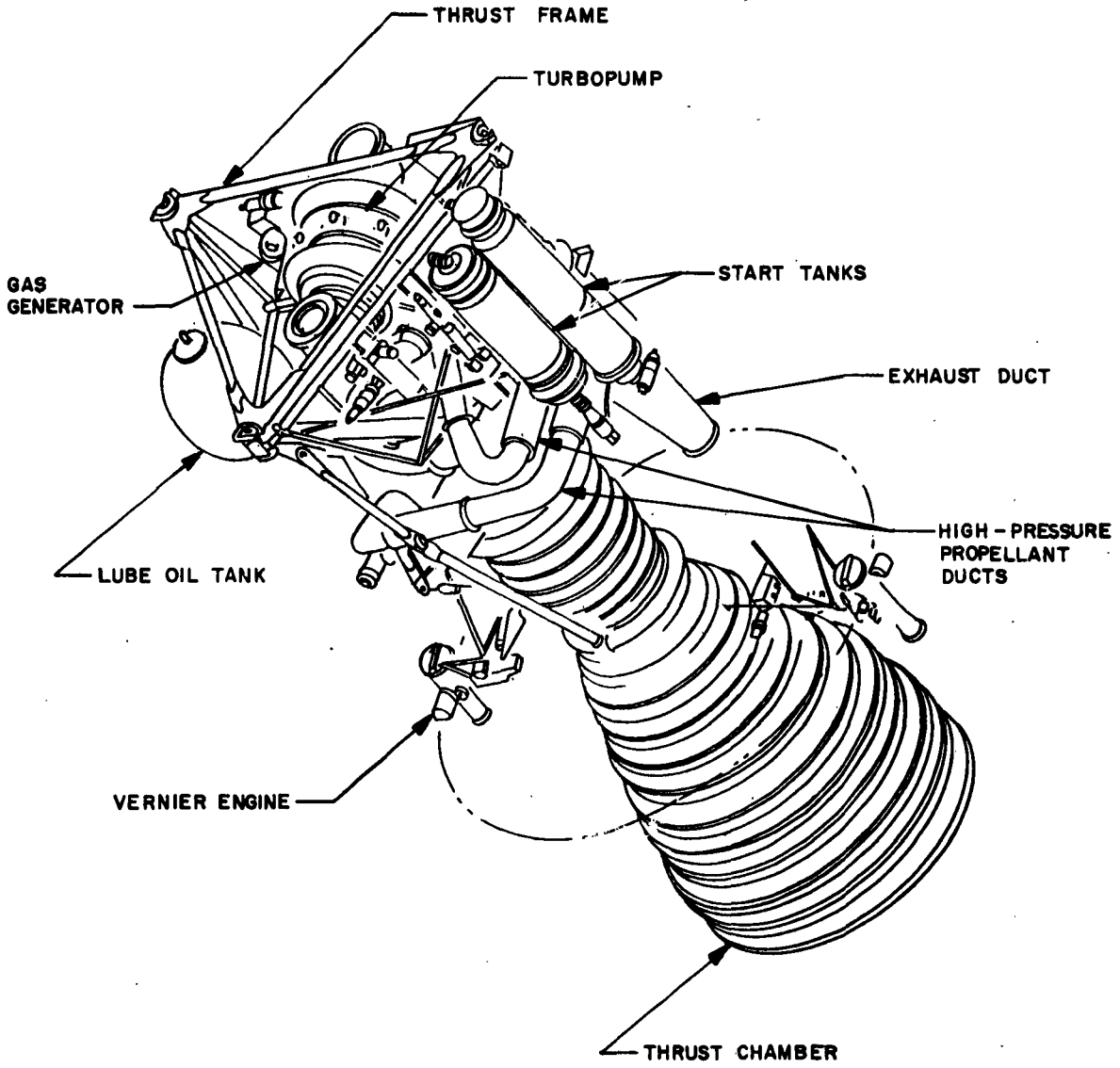


Figure 1. LV-2A Propulsion System

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The turbopump for the main engine provides one accessory drive pad to be used for the attachment of missile accessories. The accessory drive pad is capable of delivering 100 horsepower for the intended flight duration. The accessory drive pad conforms to the Air Force-Navy Aeronautical Design Standard AND20002-X11-K, with the following exceptions:

1. Maximum speed is 4200 rpm; minimum speed is 3650 rpm.
2. Direction of rotation is counterclockwise facing the accessory drive pad.
3. No provision is made for lubrication of accessories.

One single-element heat exchanger for gasifying liquid oxygen to be used as LOX tank pressurant is installed in the turbopump exhaust duct.

A list of propulsion system installation drawings is given in Table 1 .

A schematic of the main engine and details of the control orifice locations are shown in Drawings 104653 and 408113. Control orifice locations for the LR101-NA-11 vernier engines are shown in Drawing 350670.

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TABLE 1

LV-2A PROPULSION SYSTEM INSTALLATION DRAWINGS

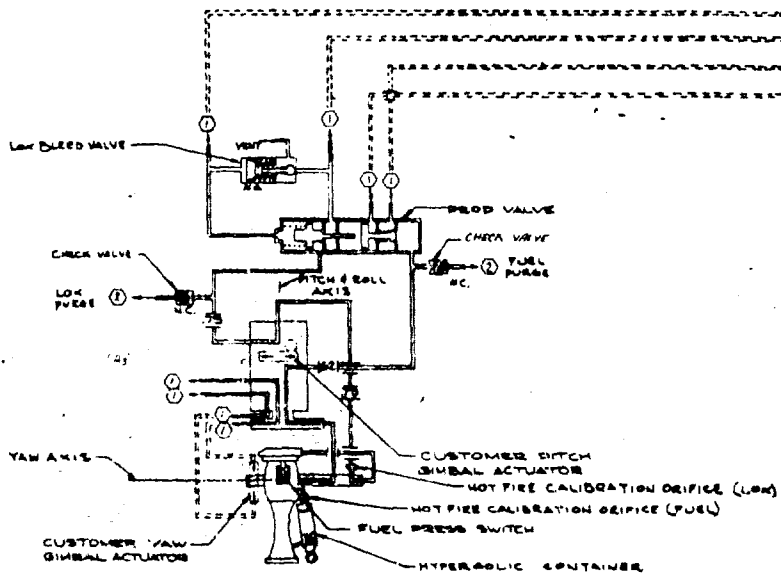
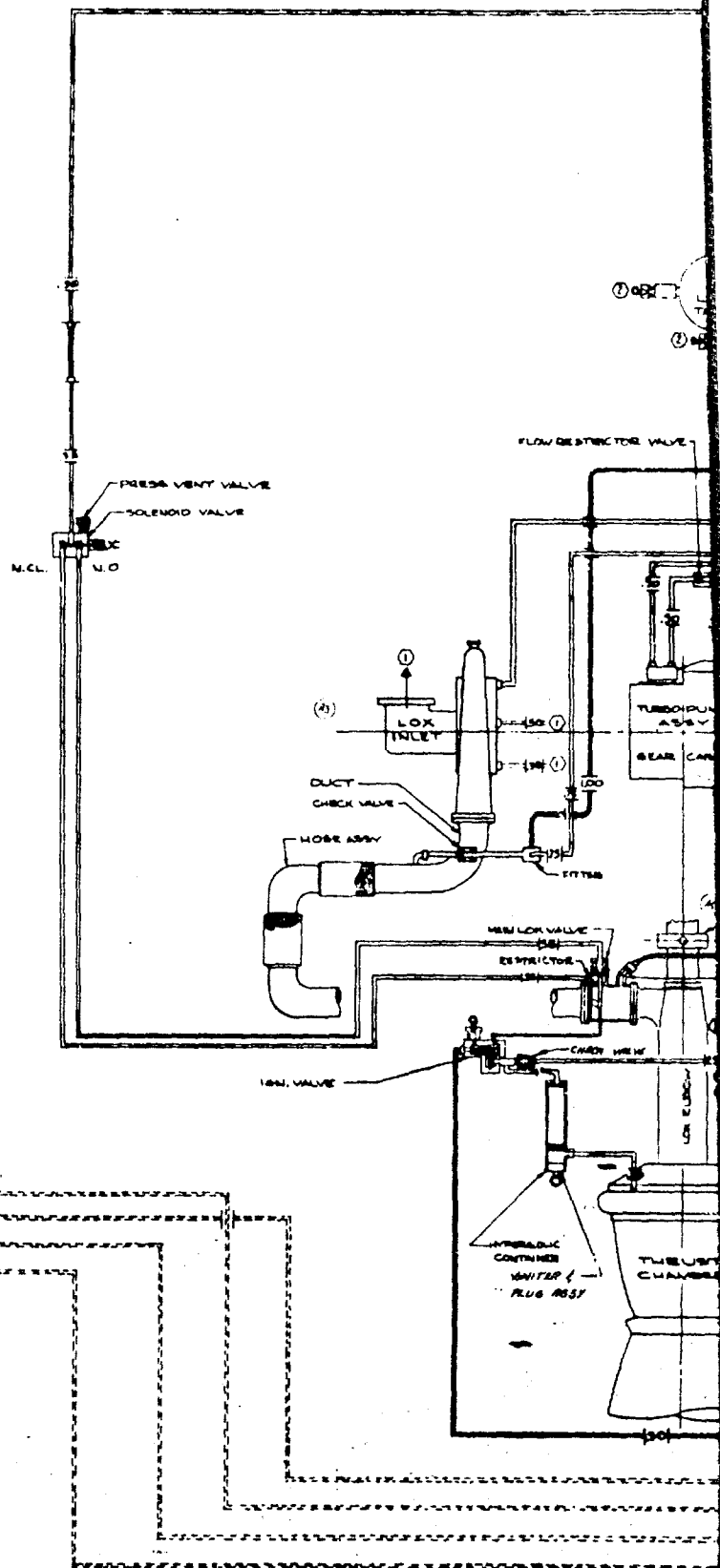
YLR79-NA-13 Main Engine

Engine Assembly Drawing	104651
Major Component Installation	104652
Start System Installation	308451
Gas Generator and Exhaust Installation	308452
Propellant Feed System Installation	407226
Electrical Equipment Installation	502101
Pneumatic System Installation	556351
Lube System Installation	556352
Loose Equipment List	651601

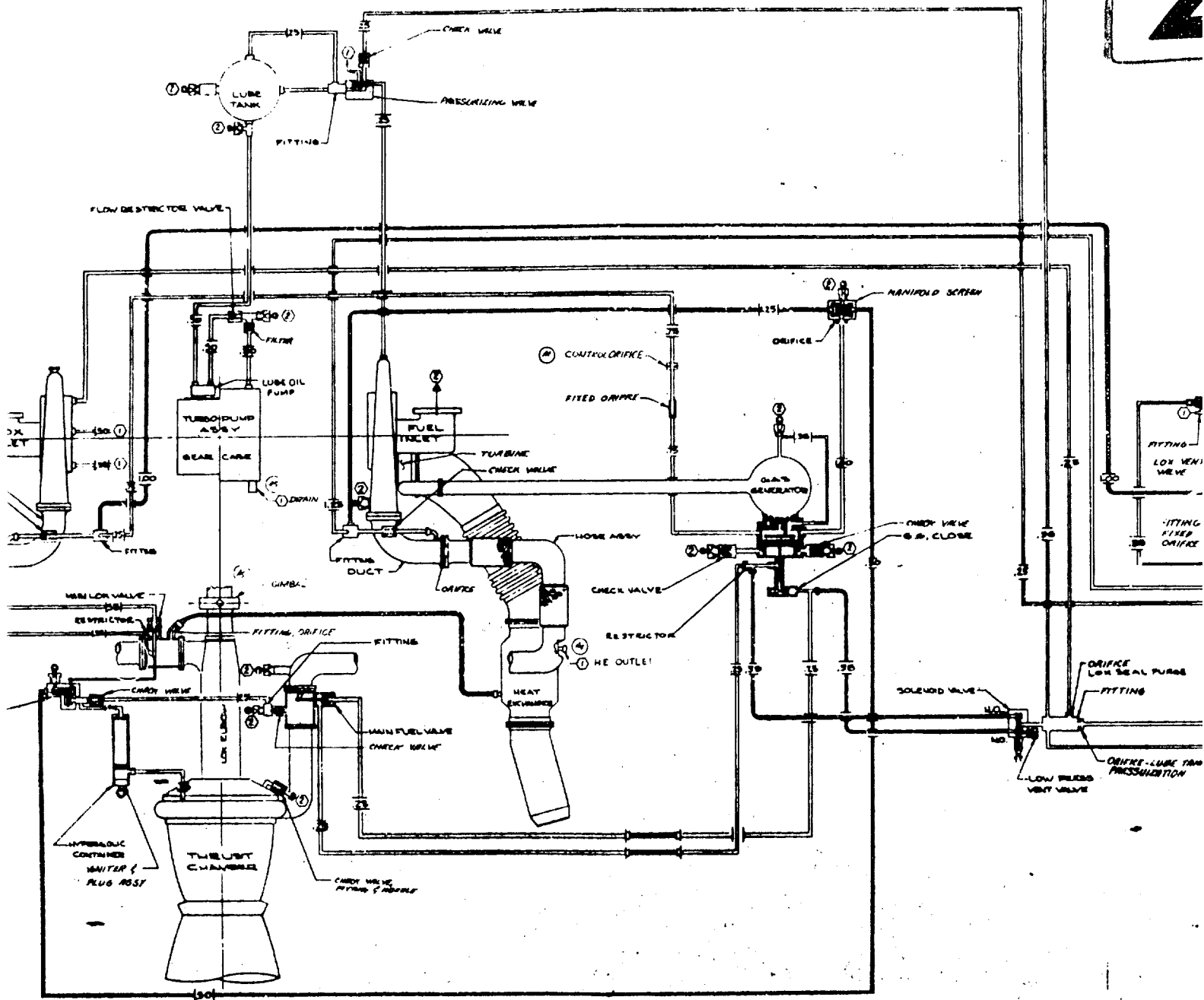
LR101-NA-11 Vernier Engine

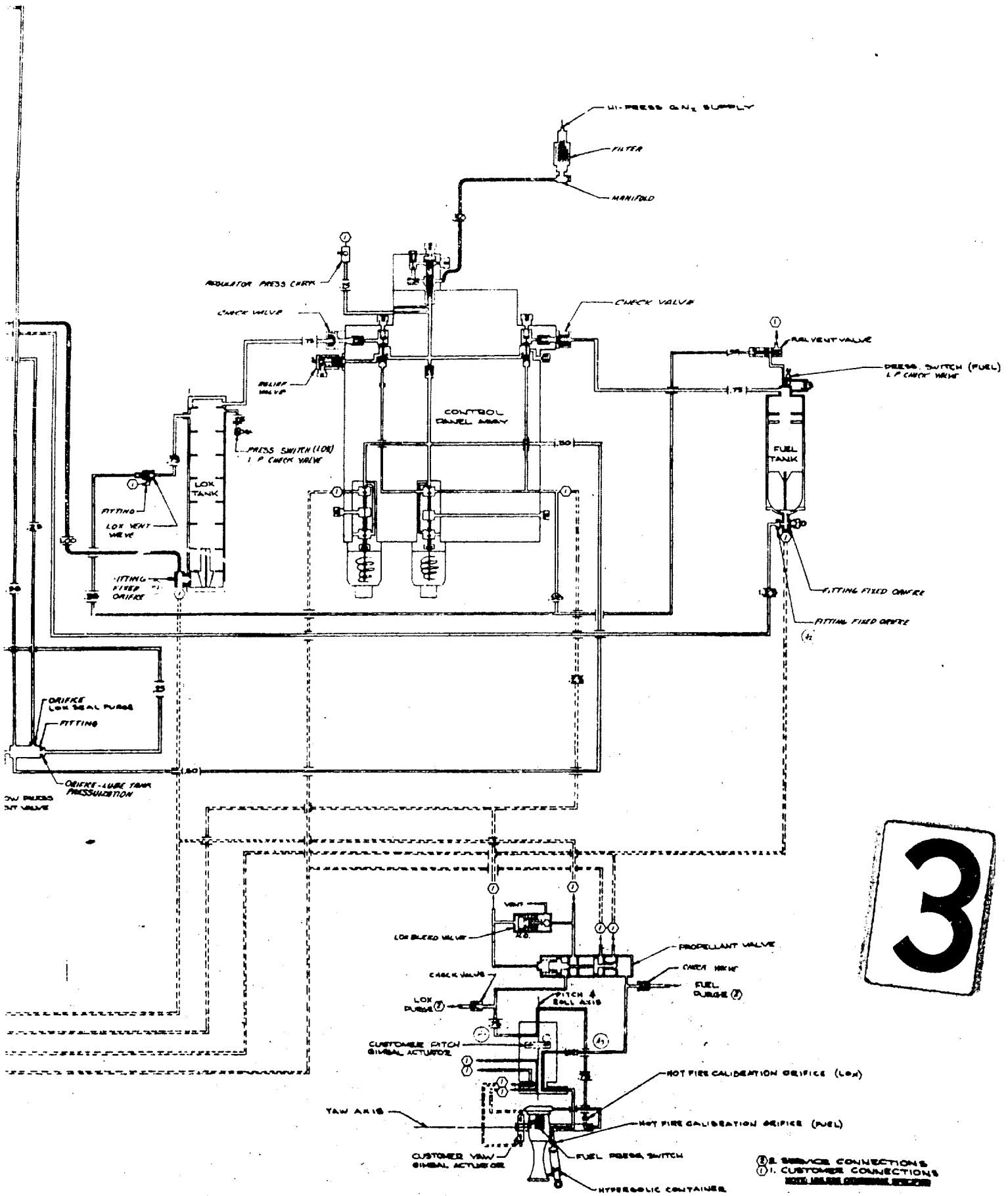
Engine Assembly Drawing	350655
Gimbal Body Installation	350660
Propellant Feed System Installation	350665
Orifice and Accessory Installation	350670
Loose Equipment List	350674
Electrical Installation	350675

1



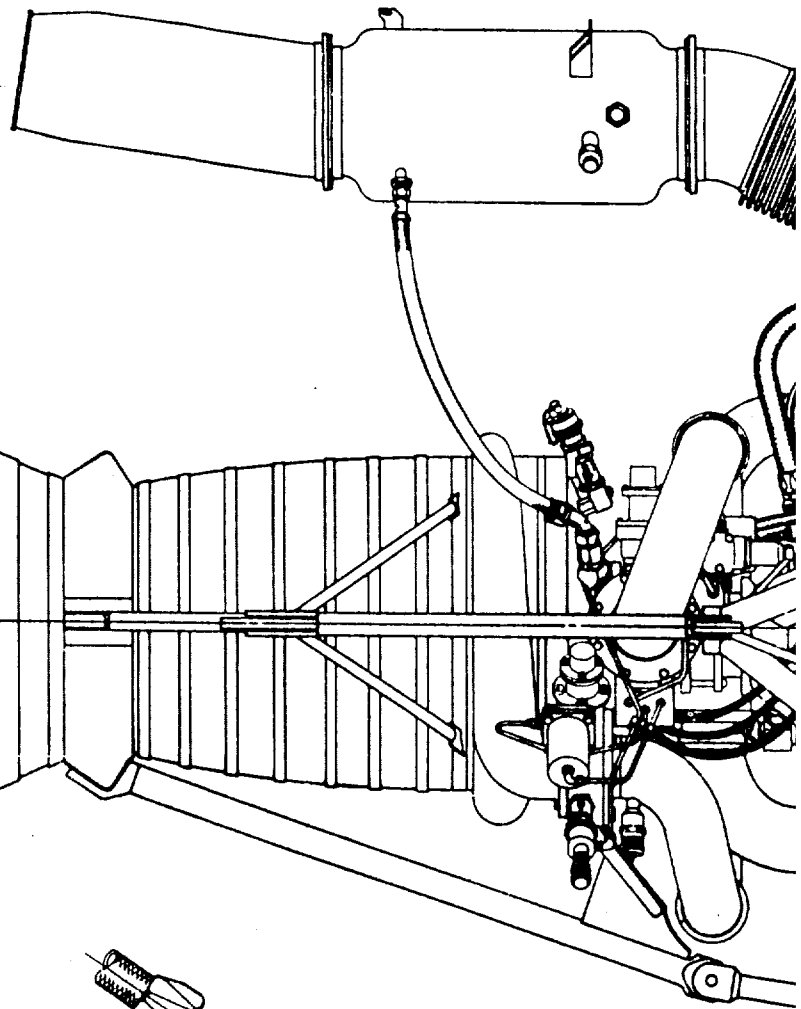
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② B. SERVICE CONNECTIONS
 ① J. CUSTOMER CONNECTIONS
 NOTE: ALL USE STANDARD SIZES



521916-3000 HOSE ASSY (REF)

AN815-160 UNION (REF)

401858 FITTING (REF)
ROTATED 90° FOR CLARITY

MA5-2603279 CHECK VALVE (REF)

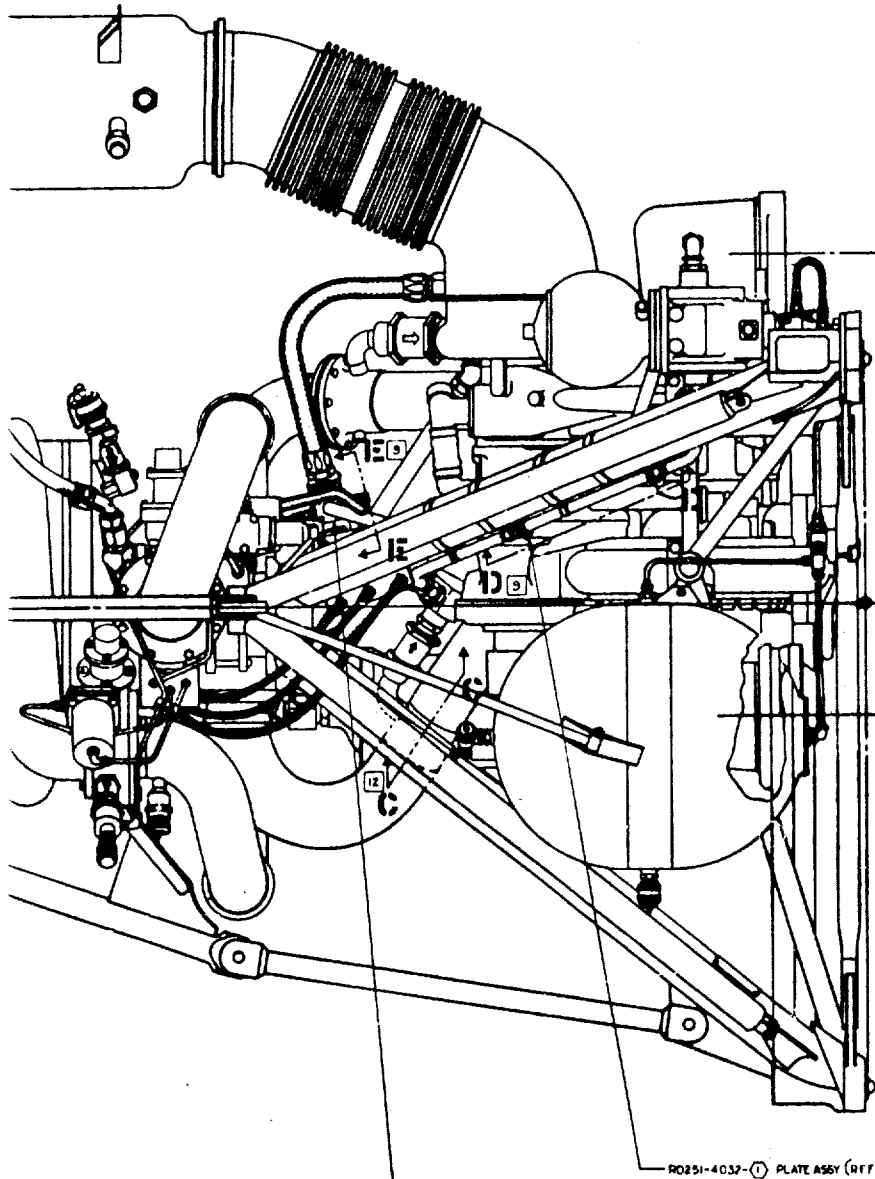
PORT FOR 401300
TUBE ASSY (REF)

401046 DUCT ASSY OF (REF)

VIEW **C-C** II
(HALF SIZE)

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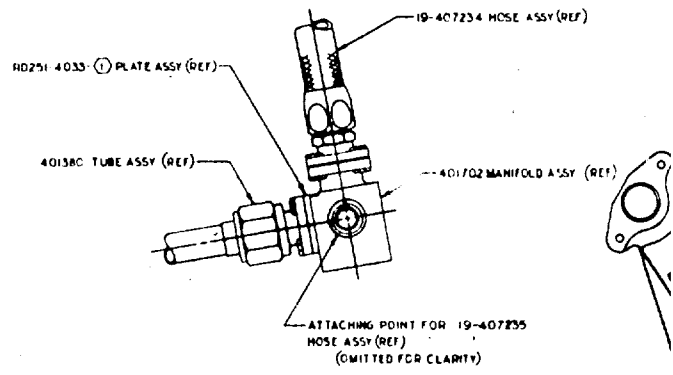
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TUBE ASSY (REF)

401046 DUCT ASSY OF (REF)

R0251-4033-① PLATE ASSY (REF)

R0251-4032-① PLATE ASSY (REF)

2



R0251-4033-① PLATE ASSY (REF)

401390 TUBE ASSY (REF)

401702 MANIFOLD ASSY (REF)

ATTACHING POINT FOR 19-407255
HOSE ASSY (REF)
(OMITTED FOR CLARITY)

VIEW E-E
(HALF SIZE)

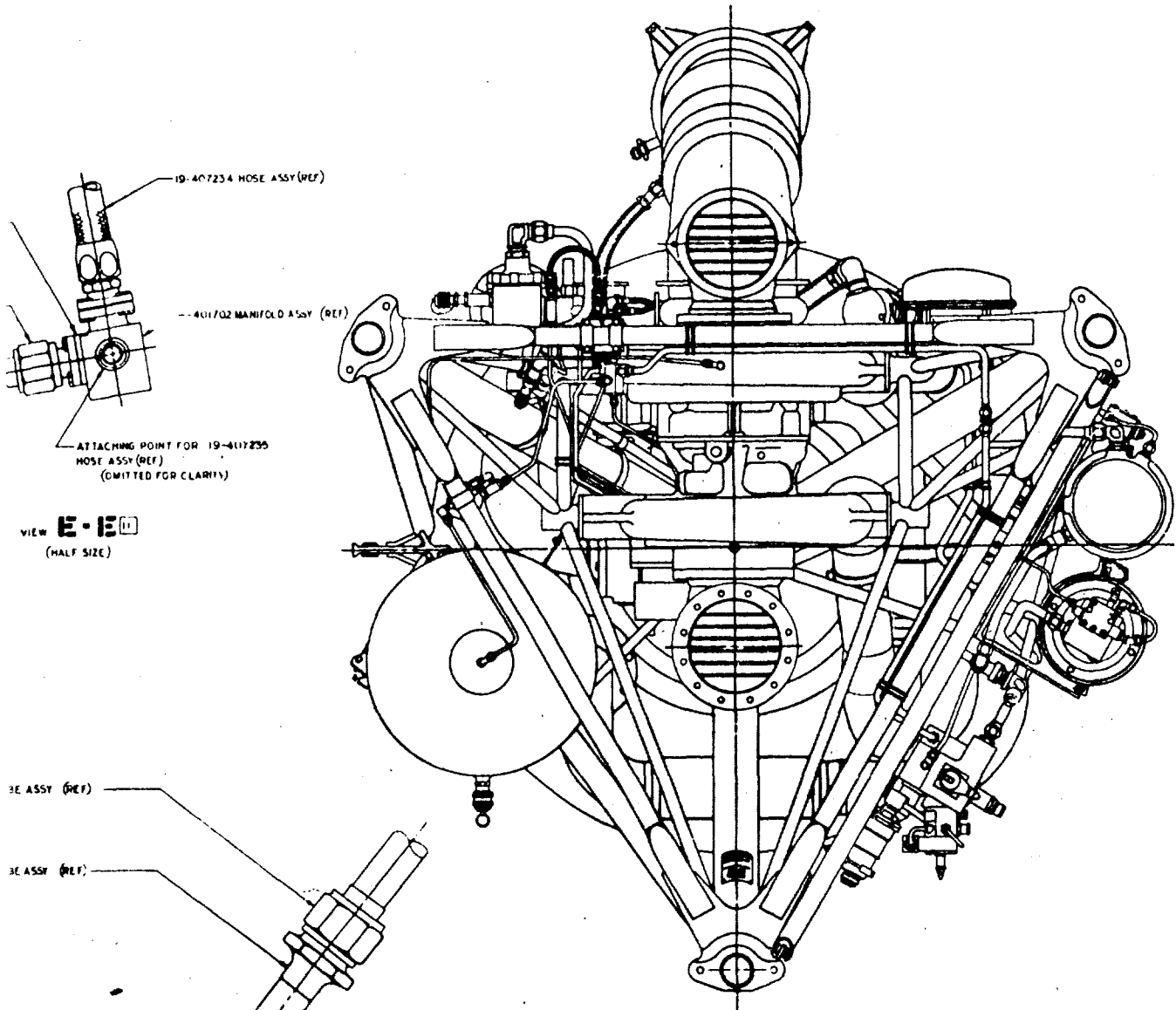
401390 TUBE ASSY (REF)

404988 TUBE ASSY (REF)

401868 TUBE ASSY (REF)

R0251-4032-① PLATE ASSY (REF)

VIEW D-D
(FULL SIZE)



19-407234 HOSE ASSY (REF)

19-401702 MANIFOLD ASSY (REF)

ATTACHING POINT FOR 19-4017235
HOSE ASSY (REF)
(OMITTED FOR CLARITY)

VIEW **E-E** (1)
(HALF SIZE)

3E ASSY (REF)

3E ASSY (REF)

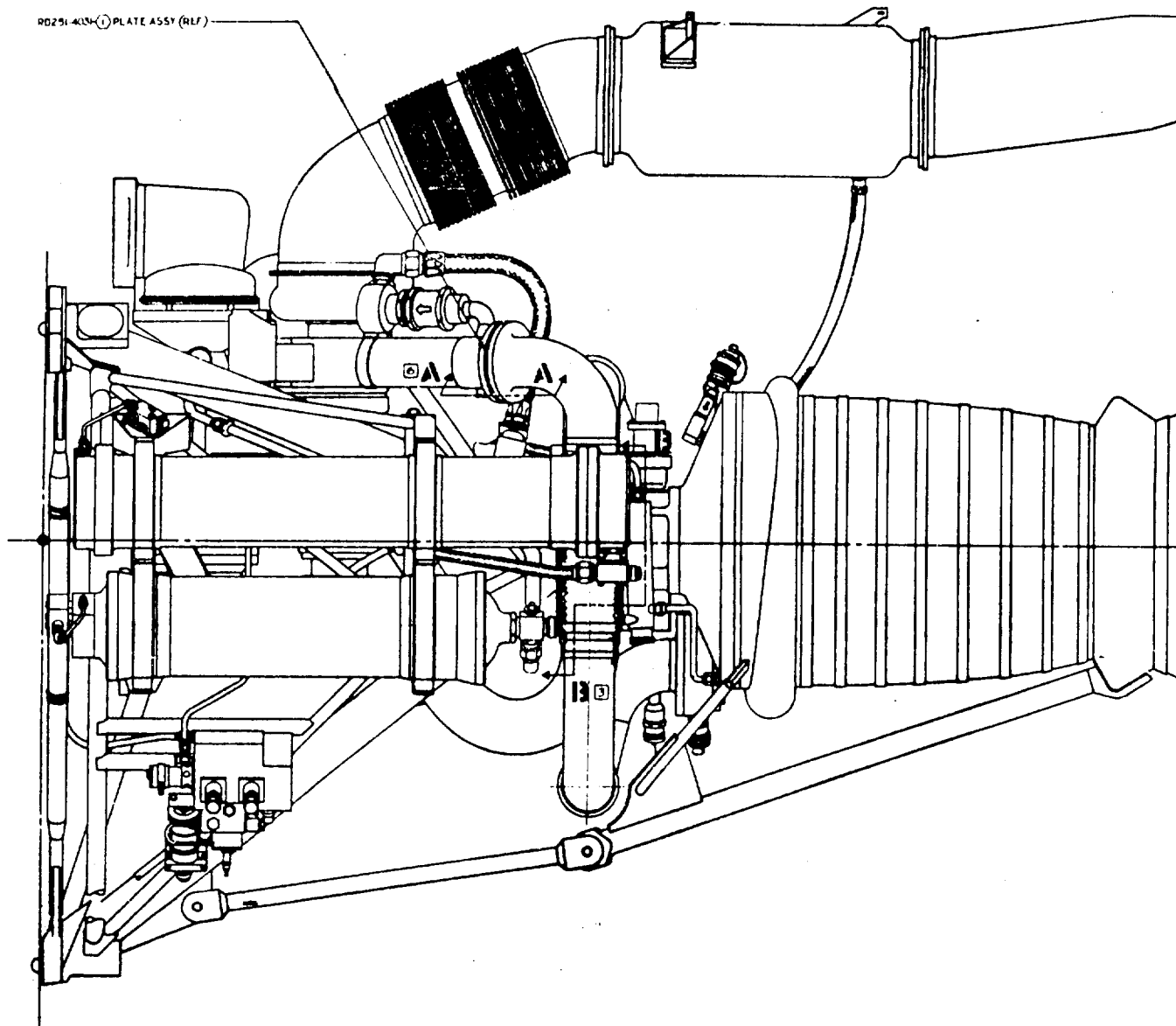
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(FULL SIZE)

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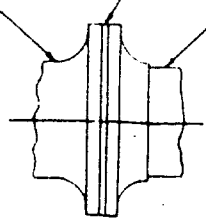
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RD251-403-1 PLATE ASSY (REF)

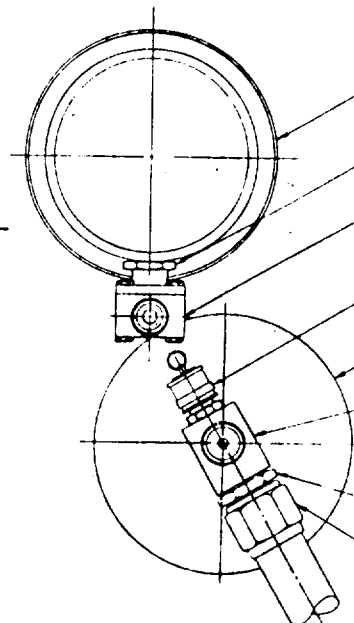
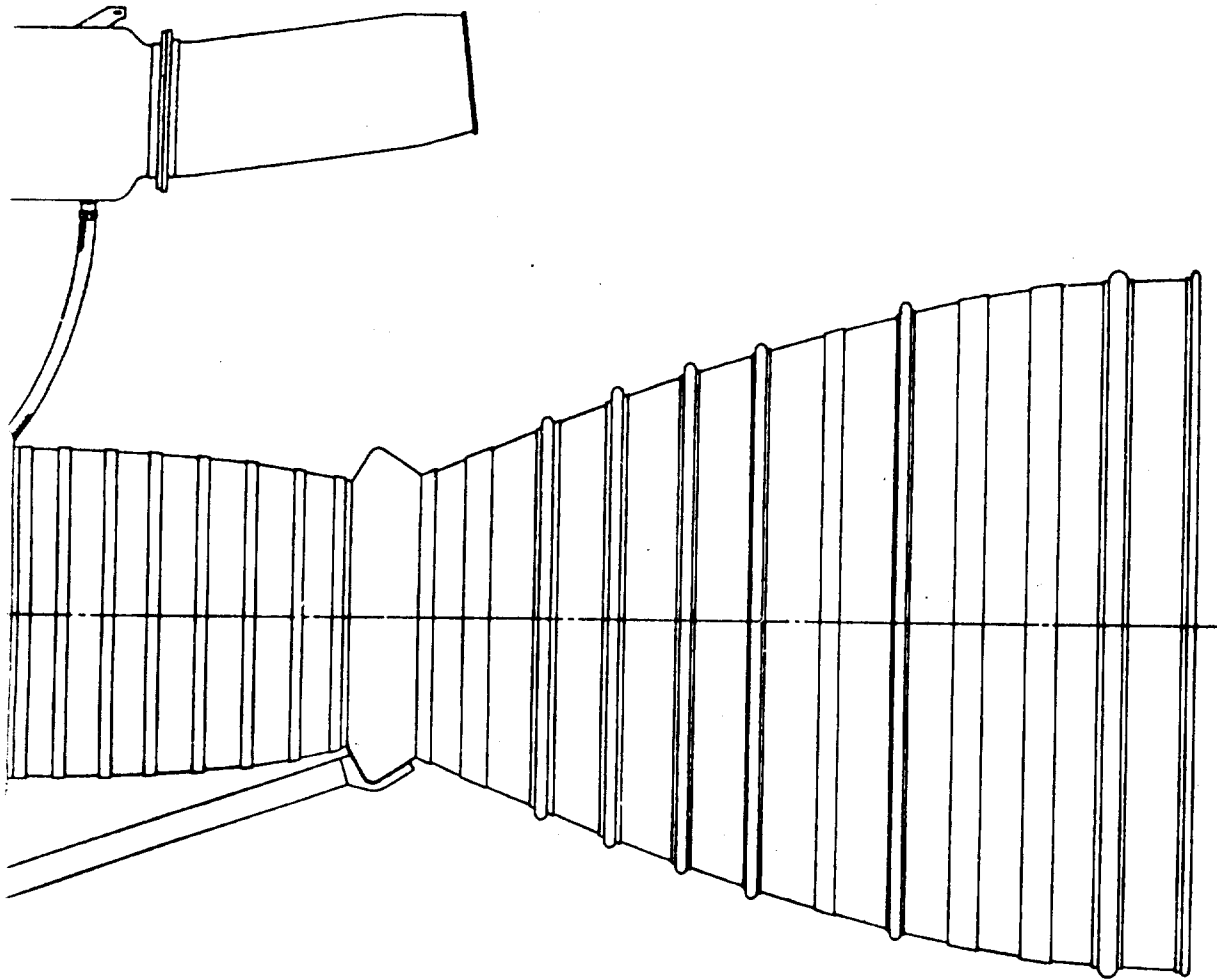
40179 DUCT (REF)

401409 HOSE ASSY (REF)



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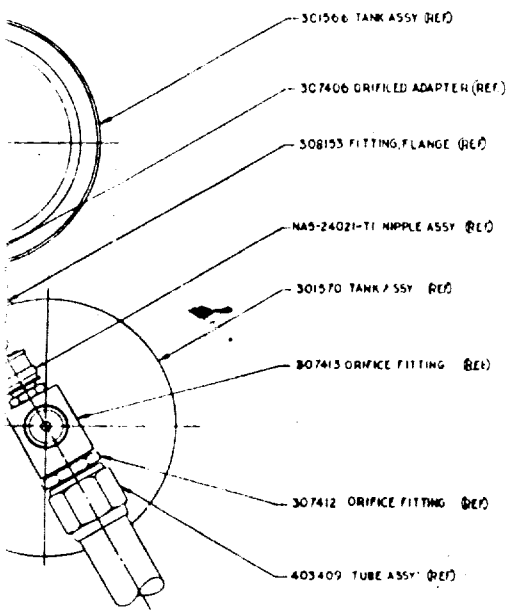
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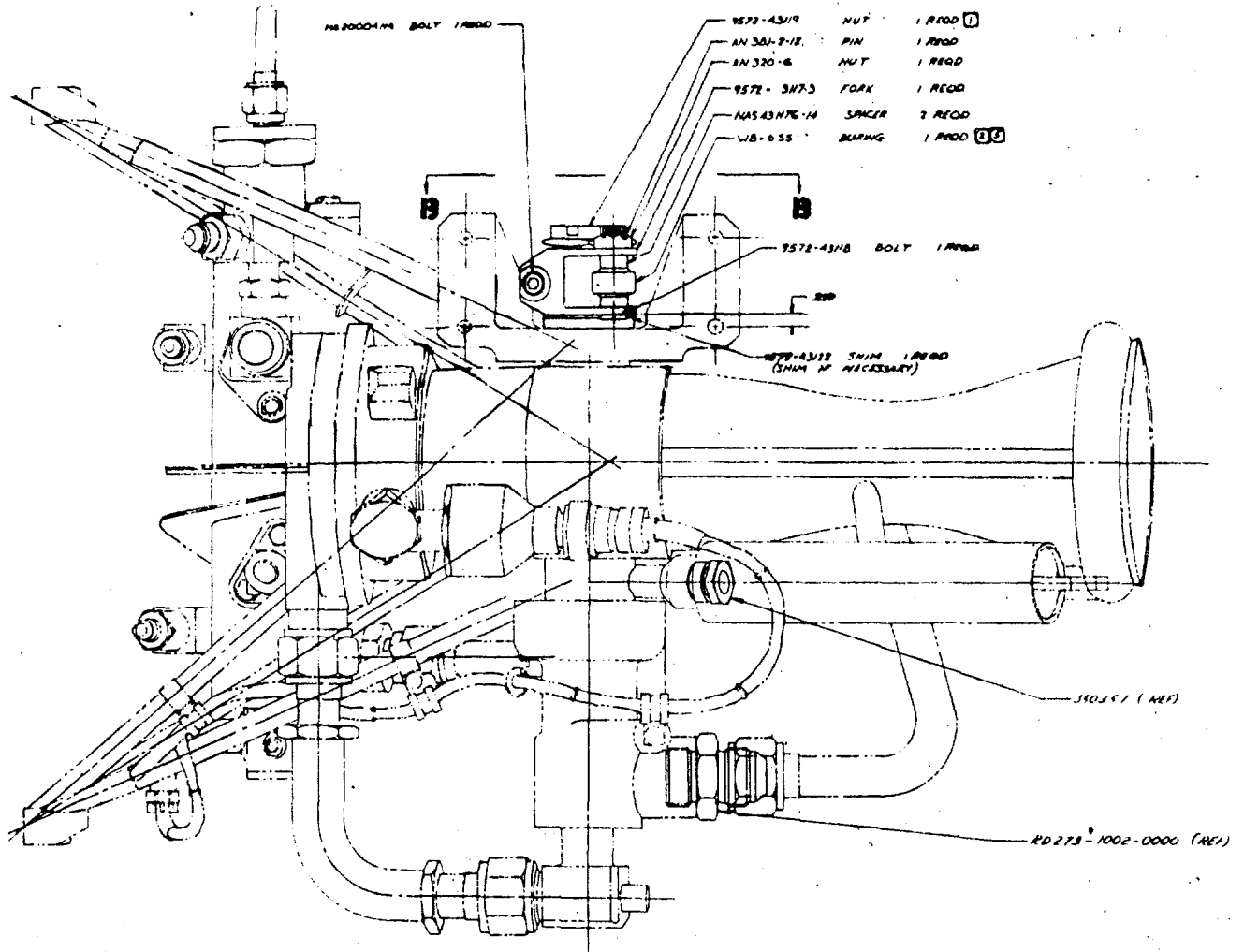
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FOR REFERENCE ONLY

① ORIFICE DIAMETER TO BE DETERMINED BY RA0201-109. IDENTIFY ALTERED PARTS PER RA0104-010 TO REFLECT THE ORIFICE DIAMETER

NOTE: UNLESS OTHERWISE SPECIFIED

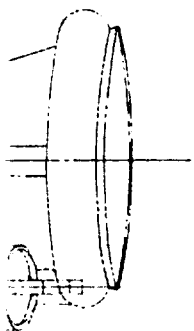
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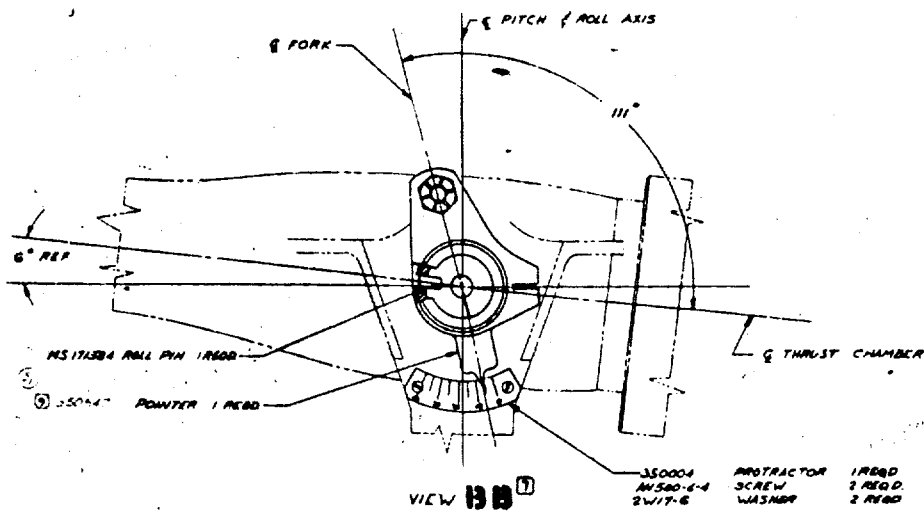
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MAE 26301 SWITCH
 MS17254 PACKING



35035 (REF)

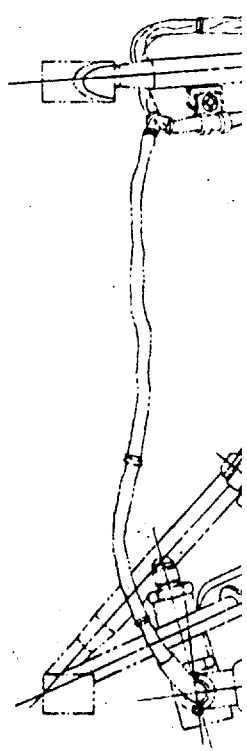
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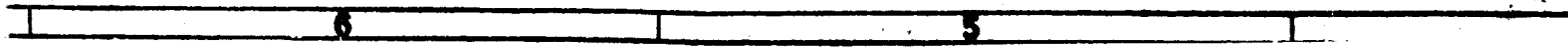
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 35034 POINTNER 1 REQD

350004 PROTRACTOR 1 REQD
 MS580-4-4 SCREW 2 REQD
 2W17-6 WASHER 2 REQD

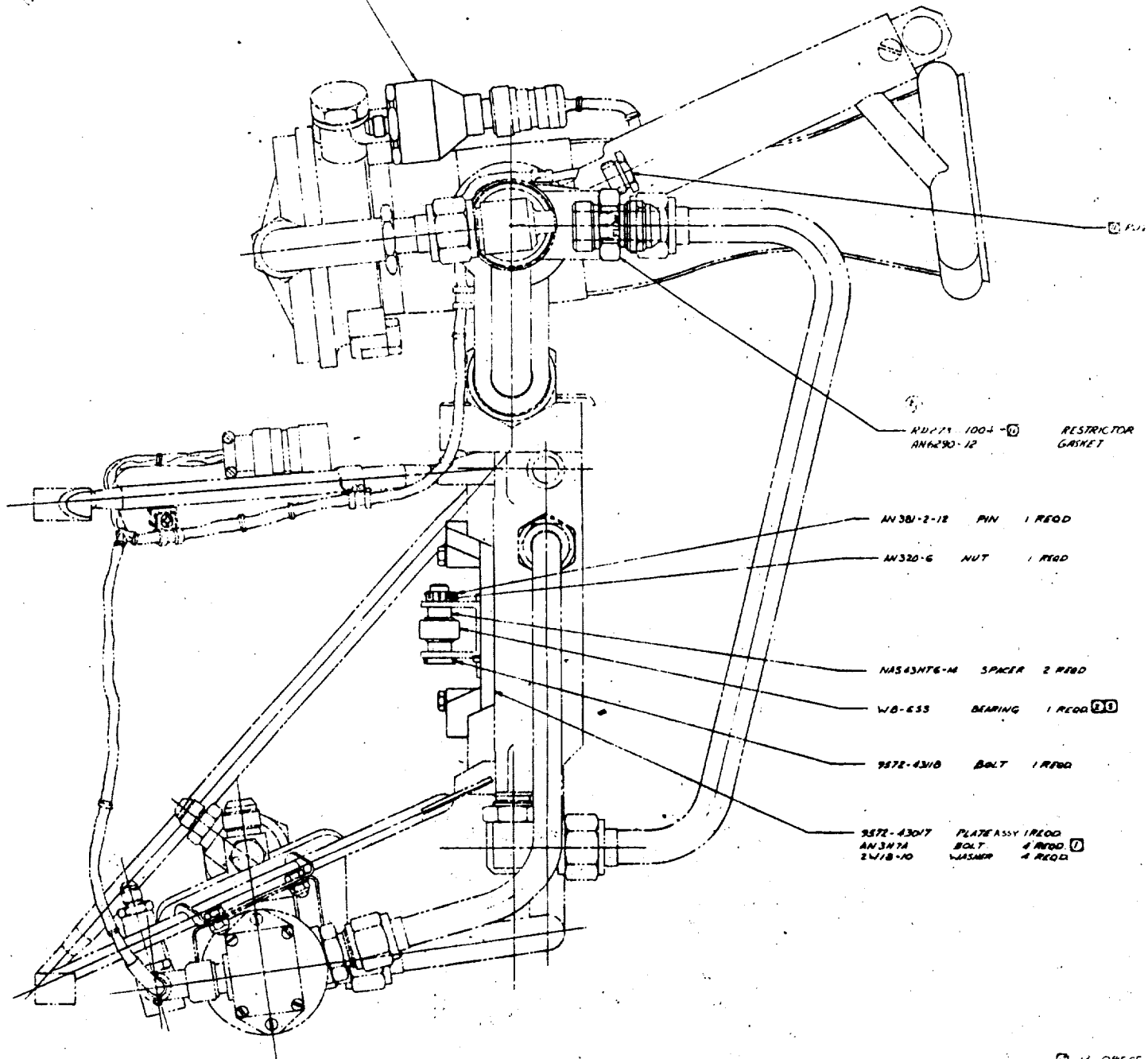
VIEW BB



2



10000
 WAS 26301 SWITCH 1 REQD
 WAS 26302 PACKING 1 REQD



- 10000-100-10 RESTRICTOR GASKET
- AN 301-2-12 PIN 1 REQD
- AN 320-6 NUT 1 REQD
- NAS 43HT6-M SPACER 2 REQD
- WB-653 BEARING 1 REQD 20
- 9572-4308 BOLT 1 REQD
- 9572-4307 PLATE ASSY 1 REQD
- AN 347A BOLT 4 REQD 7
- 24/18-10 WASHER 4 REQD

- 20 12. CHECK & IDENTIFY PERFECT
- 11. PASSIVATE
- 10. VERIFY CLEARANCE
- 9. COMMERCIAL BEFORE OR WARE INSTALL
- 8. WARE INSTALL
- 7. CLEAN PER
- 6. INST LL THING
- 5. ALTERNATE FROM SOUT
- 4. INSTALL PER LOW SERVIX
- 3-125-111-11
- 2. PAY BY PAPER
- 1. INSTALL LOCK

3

CUSTOMER CONNECT INFORMATION

This portion of the report contains information related to LV-2A propulsion system installation, weight distribution, instrumentation, electrical requirements, and general operating requirements and limitations.

ALLOWABLE INSTALLATION MISALIGNMENTS

The coordinate system used by Rocketdyne for designating reference axes and their origins is given in Fig. 2. Data are intended for use in the orientation of the LV-2A propulsion system in the Thor missile boattail.

Table 2 lists the customer connect points, coordinates the expected flight deflections of each point, and the allowable installation misalignments of the LOX and fuel pump inlet bellows for the main engine. The recommended maximum installation misalignment is based upon an inlet bellows approximately 13.5 inches long with an axial spring rate of 600 lb/in. and a maximum lateral spring rate of 500 lb/in. The recommendations assume that:

1. The bellows spring rates will be verified by laboratory test.
2. No liners are present in the bellows unless tests prove that there is a possibility of the liners "bottoming" or "hanging up" when subjected to maximum deflections resulting from the sum of allowable installation misalignment and turbopump and missile deflections.

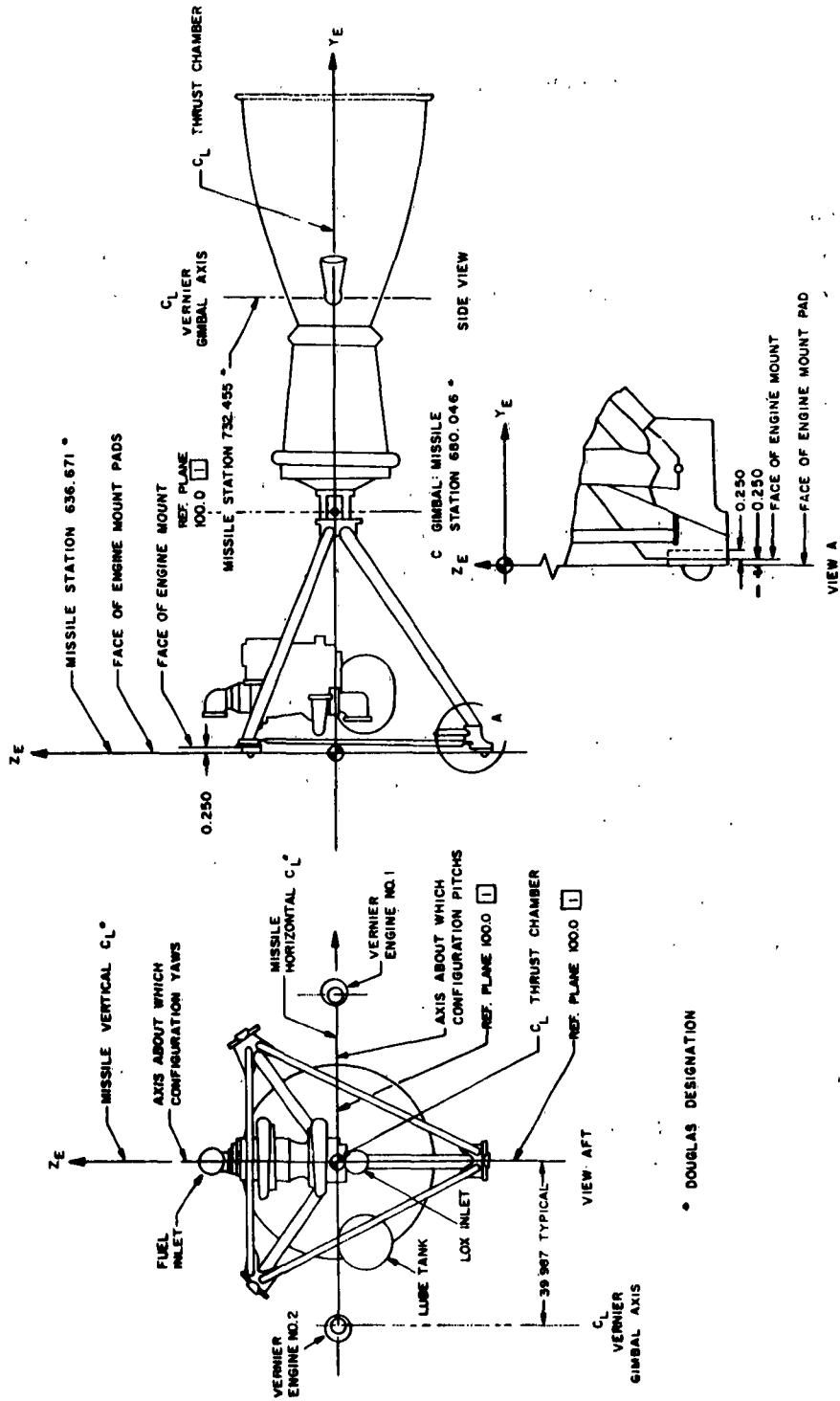


Figure 2. Coordinate System

1

TABLE 2

LV-2A PROPULSION
DEFLECTIONS AND ALLOWABLE INSTABILITY

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflection	
	X	Y	Z	Δ X	Δ Y
Geometrical center of triangle formed by the three thrust missile attach points.	0.000	0.000	0.000		
Mount Attach to Missile	28.919	0.000	16.697	The three thrust mount-to-missile will deflect radially (outboard)	
Mount Attach to Missile	-28.919	0.000	16.697		
Mount Attach to Missile	0.000	0.000	-33.393		
Turbopump, LOX Inlet Elbow	0.000 ±0.187	6.500 ±0.132	-7.776 ±0.187	±0.12	+0.12 to -0.37
Turbopump, Fuel Inlet Elbow	0.000 ±0.187	5.250 ±0.132	23.963 ±0.187	±0.12	+0.31 to -0.12
Forward Pitch Actuator Attach Point (Center of Bearing)	0.000 ±0.12	12.407 ±0.12	-28.703 ±0.12		
Aft Pitch Actuator Attach Point (Center of Bearing)	0.000 ±0.37	43.375 ±0.37	-24.000 ±0.34		
Forward Yaw Actuator Attach Point (Center of Bearing)	-24.000 ±0.34	43.375 ±0.12	0.000 ±0.12	Deflections of actuator attachment points	
Aft Yaw Actuator Attach Point (Center of Bearing)	-28.703 ±0.12	74.341 ±0.12	0.000 ±0.12		
Forward Attach Lug, Heat Exchanger	6.12 ±0.12	51.27 ±0.12	40.69 ±0.12	The three heat exchanger attachment lugs must not be closed by the three thrust attachment points	
Forward Attach Lug, Heat Exchanger	6.12 ±0.12	51.27 ±0.12	40.69 ±0.12		
Aft Attach Lug, Heat Exchanger (Center of Slot)	0.00 ±0.12	66.25 ±0.12	41.32 ±0.12		

*Refer to note 1 on drawing 104654. The total transverse misalignment shall not exceed 0.010 inches.
R-5214

TABLE 2

LV-2A PROPULSION SYSTEM

AND ALLOWABLE INSTALLATION MISALIGNMENTS

In-Flight Deflections, inches		Allowable Installation Misalignment With Respect To Engine, inches					
ΔY	ΔZ	ΔX	ΔY	ΔZ	θX	θY	θZ
<p>Thrust mount-to-missile attach points are within 0.010 inch of true position. The attach points do not deflect more than 0.044 \pm 0.010 (NA-13) inch during flight.</p>							
+0.12 to -0.37	+0.25 to -0.12	$\pm 0.50^*$	0.50 Tension or Compression	± 0.50	$\pm 3^*$	0	± 3
+0.31 to -0.12	+0.25 to -0.12	$\pm 0.50^*$	0.75 \pm 0.50 Tension	± 0.50	$\pm 3^*$	0	± 3
<p>of actuator attach points do not affect the missile structure,</p>							
<p>Heat exchanger attach lugs are mated with the missile. The centroid of the triangular area defined by these lugs must not deflect more than 0.37 inch relative to the centroid of the area enclosed by the three thrust attach points.</p>							



shall not exceed 0.50 inch.



TABLE 2
(Continued)

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflections, i		
	X	Y	Z	ΔX	ΔY	ΔZ
Oxygen Outlet, Heat Exchanger	-7.93 ± 0.12	51.37 ± 0.12	30.87 ± 0.12	Deflects with missile		
Aft End Heat Exchanger	0.00 ± 0.12	69.45 $\pm 0.12^*$	34.57 ± 0.12	Deflects with missile		
LOX Supply to Vernier Engine	30.63 ± 0.12	47.07 +0.34 -0.27	-2.48 +0.47 -0.49	± 0.12	+0.31 to -0.12	$\pm 0.$
Fuel Supply to Vernier Engines	28.15 +0.29 -0.31	40.85 +0.27 -0.28	-6.82 +0.33 -0.31	± 0.12	+0.25 to -0.12	$\pm 0.$
Main Oil Discharge	1.33 ± 0.12	29.73 ± 0.12	14.72 ± 0.12	± 0.12	+0.19 to -0.12	$\pm 0.$
Fuel Start Tank Vent Valve Vent	20.19 ± 0.12	12.53 ± 0.12	-0.18 ± 0.12	± 0.12	+0.25 to -0.12	$\pm 0.$
LOX Start Tank Vent Valve Vent	24.70 ± 0.12	6.54 ± 0.12	-14.06 ± 0.12	± 0.12	+0.19 to -0.12	± 0.1
High-Pressure Gaseous Nitrogen Supply	8.65 ± 0.12	11.35 ± 0.12	-26.45 ± 0.12	± 0.12	+0.19 to -0.12	± 0.1
Center Tachometer Mount Pad (No gasket)	-0.40 ± 0.12	20.07 ± 0.12	-3.76 ± 0.12	± 0.25	+0.12 to -0.25	± 0.2
Center Hydraulic Pump Mount Pad (No gasket)	3.96 ± 0.12	24.85 ± 0.12	-1.26 ± 0.12	± 0.25	+0.12 to -0.25	± 0.2
LOX Seal Drain	-2.00 ± 0.12	30.17 ± 0.12	15.98 ± 0.12	± 0.25	+0.19 to -0.12	± 0.3
Oil Seal Drain	-3.50 ± 0.12	29.90 ± 0.12	15.87 ± 0.12	± 0.12	+0.25 to -0.12	± 0.3
Pressure Takeoff from Pneumatic Manifold	15.08 ± 0.12	7.40 ± 0.12	-15.17 ± 0.12	± 0.12	+0.19 to -0.12	± 0.1

*Refer to note 7 on drawing 104654

TABLE 2
(Continued)


Maximum Flight Deflections, inches		Allowable Installation Misalignment With Respect to Engine, inches					
ΔY	ΔZ	ΔX	ΔY	ΔZ	θX	θY	θZ
Missile		<p>The customer connect points are to be connected with no load applied except that necessary to support its weight. The parts shall be designed and installed to provide for both maximum missile and maximum flight deflections.</p> <p>Turbine Exhaust System</p> <p>(a) The aft flange of the turbine exhaust duct assembly shall be parallel with the heat exchanger flange within four degrees.</p> <p>(b) The distance between the two flanges shall be 0.31 ±0.25 inch</p> <p>(c) The misalignment of the centerline of the two flanges shall not exceed 0.38 inch</p> <div style="text-align: center; margin-top: 20px;">  </div>					
Missile							
+0.31 to -0.12	±0.12						
+0.25 to -0.12	±0.12						
+0.19 to -0.12	±0.37						
+0.25 to -0.12	±0.12						
+0.19 to -0.12	±0.12						
+0.19 to -0.12	±0.12						
+0.12 to -0.25	±0.25						
+0.12 to -0.25	±0.25						
+0.19 to -0.12	±0.37						
+0.25 to -0.12	±0.37						
+0.19 to -0.12	±0.12						

TABLE
(Continued)

Customer Connect Points	Coordinates, inches (Drawing No. 104654)			Approximate Flight Deflection	
	X	Y	Z	ΔX	ΔY
Electrical Ground Connection	17.25*	11.40	17.48	± 0.19	+0.25 to -0.12
Missile Interconnection	17.25	14.05	17.55	± 0.19	+0.25 to -0.12
Missile Power Connection	19.55*	13.25	17.55	± 0.19	+0.25 to -0.12
Vernier LOX Vent Valve Control Solenoid Exit	14.53 ± 0.12	21.18 ± 0.12	-3.41 ± 0.12	± 0.12	+0.19 to -0.12
Vernier Engine Propellant Valve Control Solenoid Exit	15.92 ± 0.12	23.31 ± 0.12	-4.33 ± 0.12	± 0.12	+0.19 to -0.12
Lube Tank Vent and Overflow	-19.23 ± 0.12	2.59 ± 0.12	5.27 ± 0.12	± 0.06	± 0.06
Lube Tank Horizontal Drain					

*Refer to note 9 on drawing 104654

1

R-5214

TABLE 2
(Continued)

ate Flight Deflections, inches		Allowable Installation Misalignment With Respect to Engine, inches					
ΔY	ΔZ	ΔX	ΔY	ΔZ	θX	θY	θZ
+0.25 to -0.12	± 0.19	These values are based on inlet bellows which have an axial inlet bellows with an axial spring rate of 600 lb/in. and a maximum transverse spring rate of 500 lb/in.					
+0.25 to -0.12	± 0.19						
+0.25 to -0.12	± 0.19						
+0.19 to -0.12	± 0.12						
+0.19 to -0.12	± 0.12						
± 0.06	± 0.06						



WEIGHT DISTRIBUTION AND FLUID VOLUMES

Weight, balance, inertia, and fluid volume information for the LV-2A propulsion system configurations is presented in Tables 3 and 4.

This data may be used in determining missile deadweight distribution, structural requirements, basic loads, stability, performance, and control requirements.

CUSTOMER CONNECT AND INSTRUMENTATION DRAWINGS

The locations of connections that are necessary for the operation of the LV-2A propulsion system in the missile are shown in Drawings 104654 and 350723 . Locations shown include those for supply connections, drain and vent connections, and flush and purge connections. Structural attachments and accessory pad information are shown, as well as gimbal bearing alignment and lubrication points.

The instrumentation tap locations on the main vernier engines that are available for use appear in Drawings 702827 and 350050 .

TABLE 3

CENTER OF GRAVITY, MOMENT OF INERTIA, AND WEIGHTS
FOR MAIN ENGINE (RJ-1 FUEL)

Propulsion system weights and centers of gravity* (including vernier engines)

Condition	Weight, pounds	Y Arm, inches	X Arm, inches	Z Arm, inches
Dry	2116	100.2	100.4	103.3
Wet	2690	100.0	100.6	102.3
Burnout	2468	101.5	100.5	102.8

*Reference point (gimbal bearing) is (100,100,100).

Moments of inertia of the propulsion system about axes through its center of gravity, wet and dry, with corresponding radii of gyration

Condition	Weight, pounds	Y Roll	X Pitch	Z Yaw
Dry Radii of gyration	2116	167 slug sq ft 19.1 inches	616 slug sq ft 36.7 inches	626 slug sq ft 37.0 inches
Wet Radii of gyration	2690	223 slug sq ft 19.6 inches	782 slug sq ft 36.7 inches	816 slug sq ft 37.5 inches

Moment of inertia of the gimballed mass about the gimbal axes (verniers not included)

Condition	Weight, pounds	Y Roll, slug sq ft	X Pitch, slug sq ft
Dry	828	32	311
Wet	1057	44	416

Longitudinal (Y axis) location of center of gravity of the gimballed mass in inches aft of the gimbal axis.

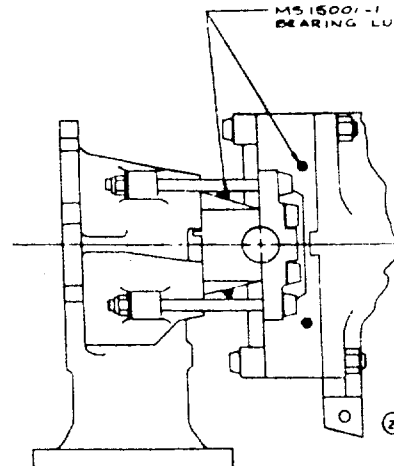
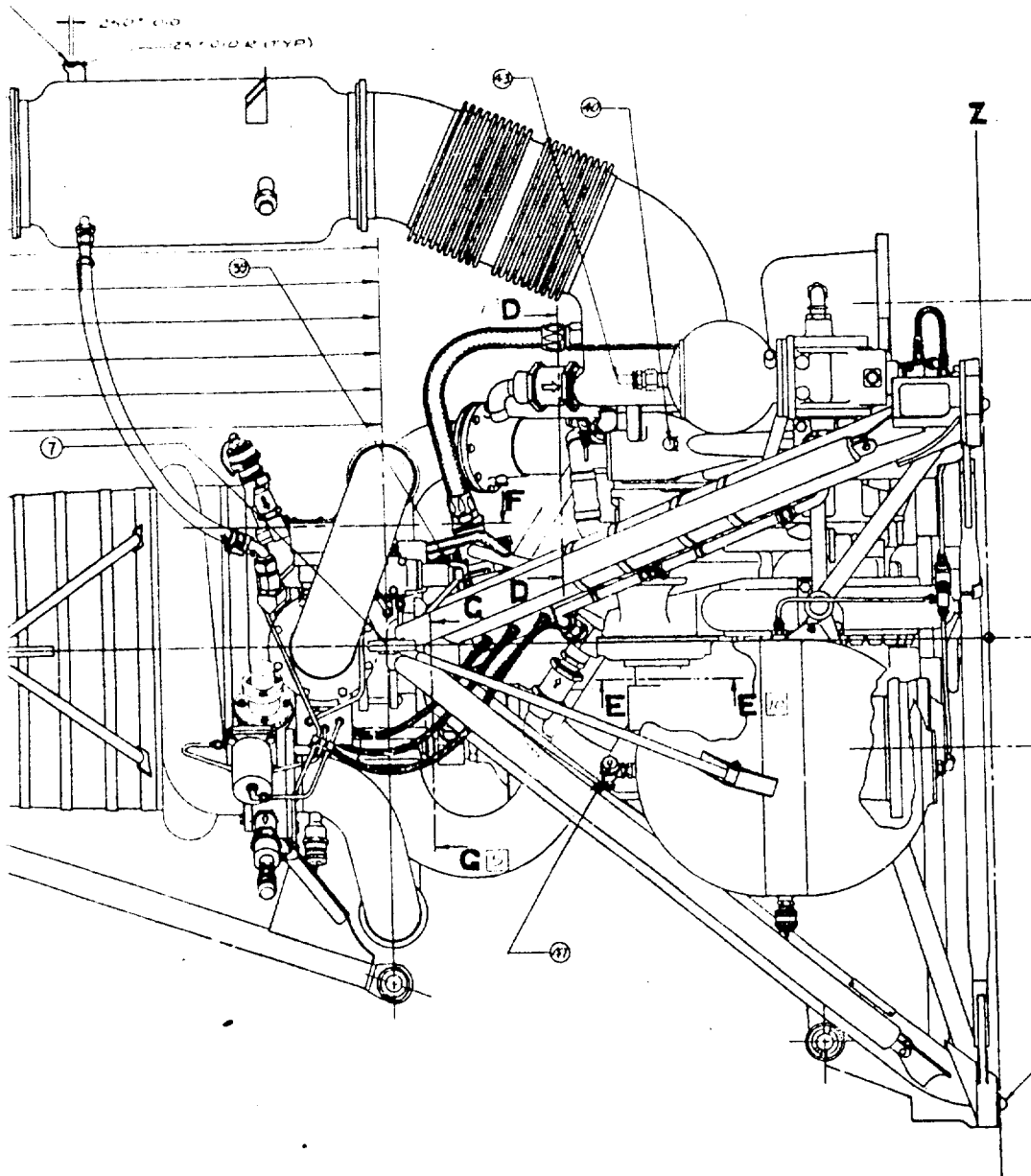
Dry = 29.0 inches
Wet = 29.2 inches

ROCKETDYNE
A DIVISION OF NORTH AMERICAN AVIATION, INC

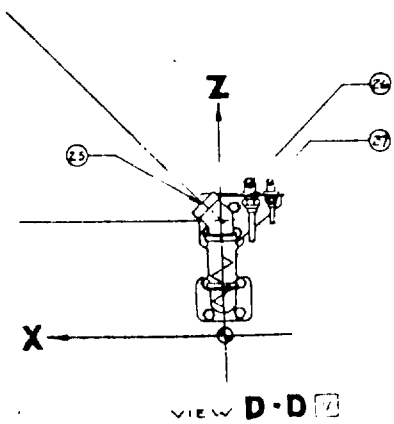
TABLE 4

MAIN ENGINE FLUID VOLUME DATA

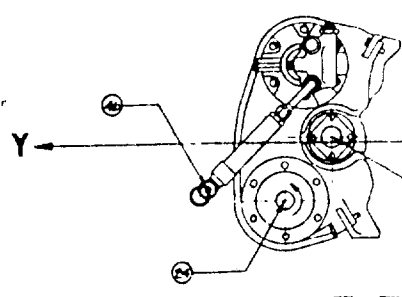
Component	Fuel Volume, cu in.	Liquid Oxygen Volume, cu in.	Oil Volume, cu in.
Thrust Chamber	3987	935	
Main Ducts	1111	1614	
Turbopump	950	945	
Lubrication System			3927
Start System	1319	1454	
Vernier Engines (2)	106	46	
Miscellaneous Units	120	183	



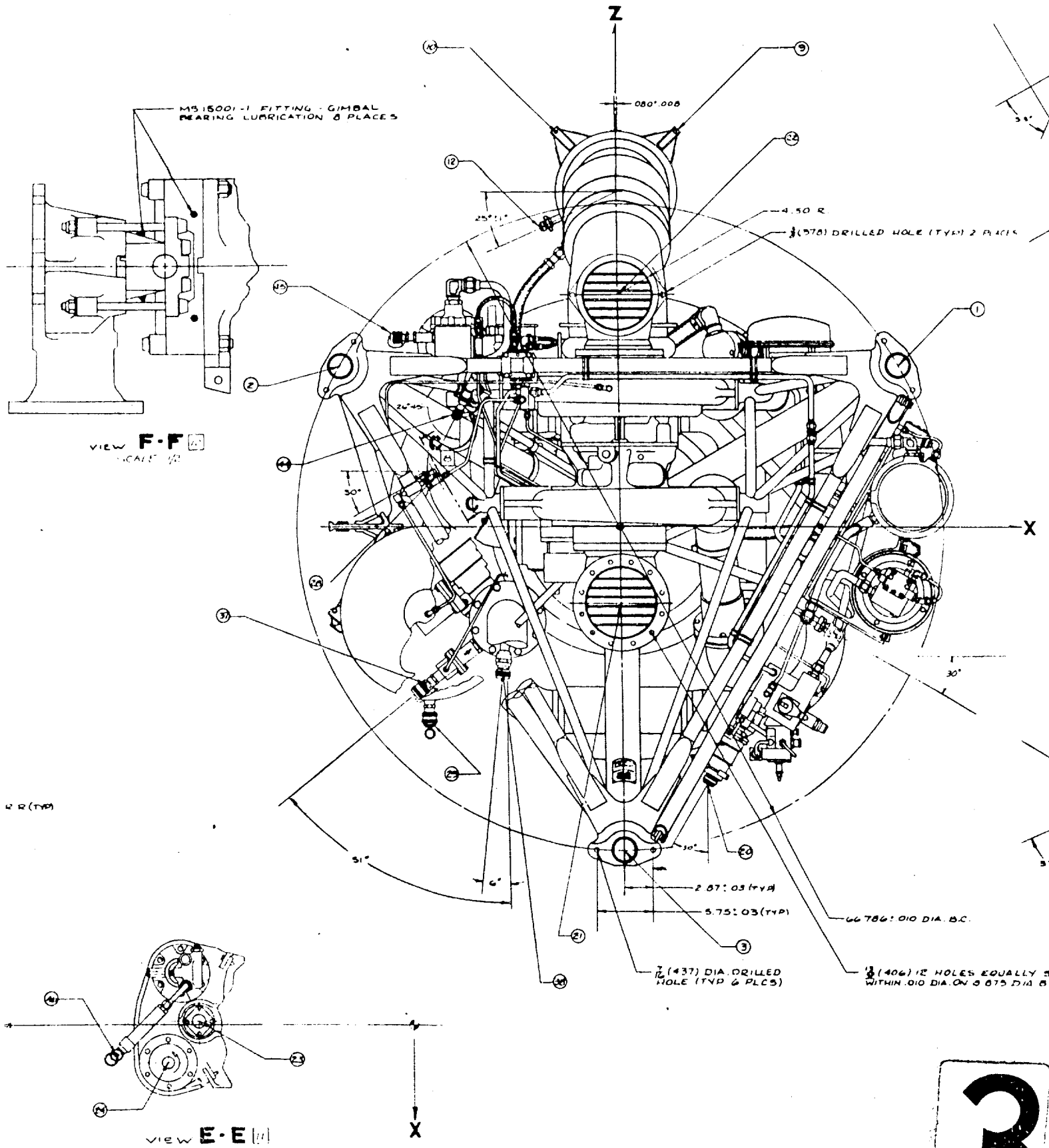
VIEW F-F
SCALE 1/2



2

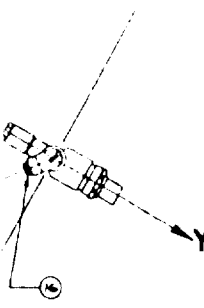
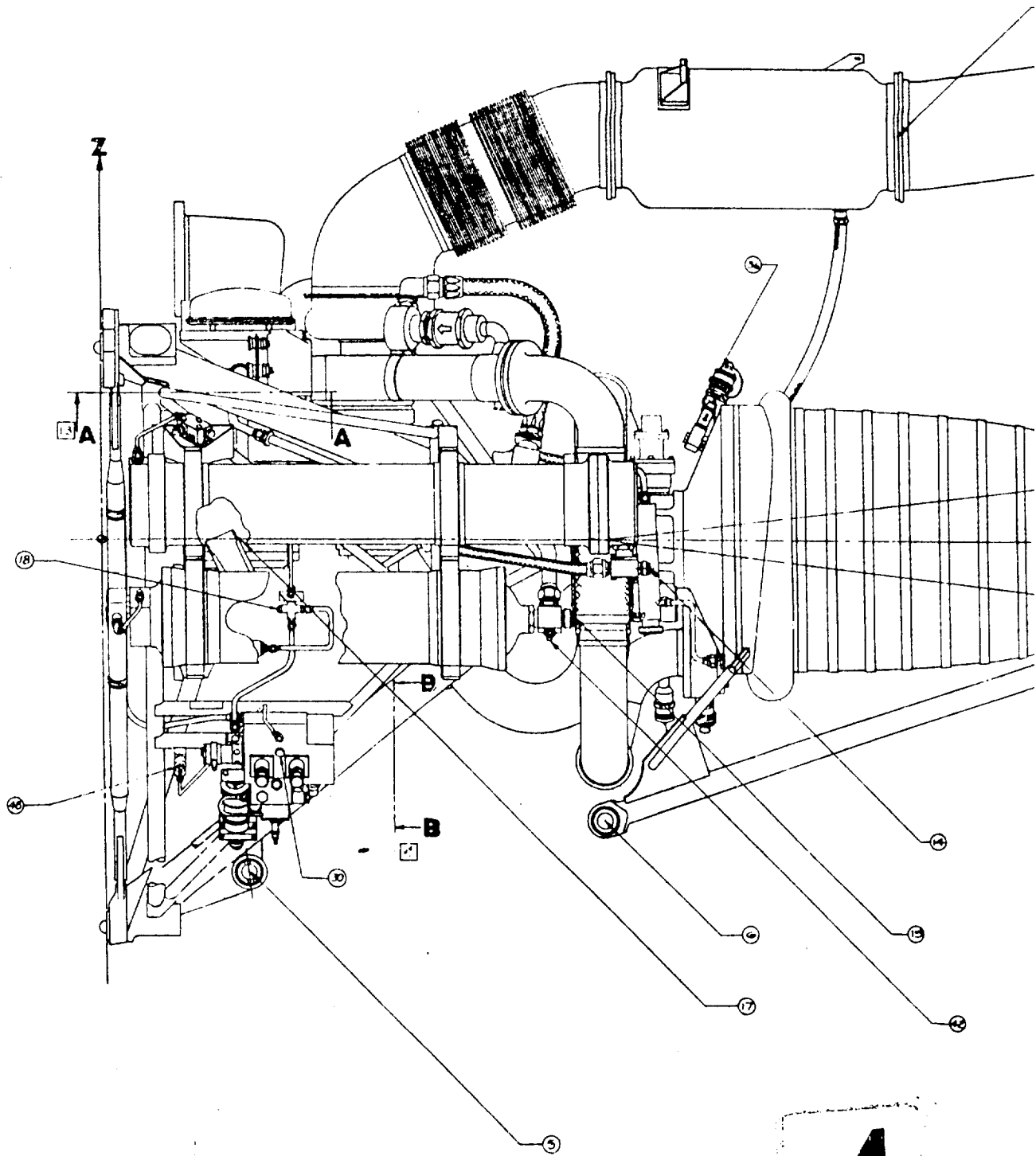


VIEW E-E

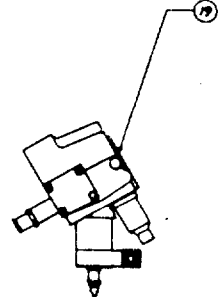
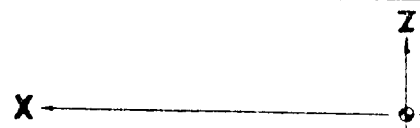
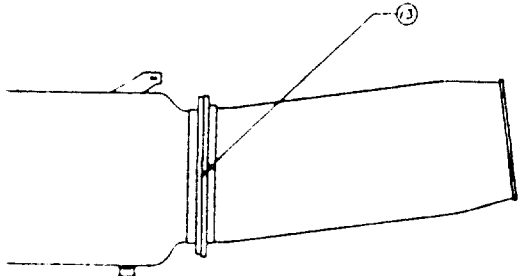


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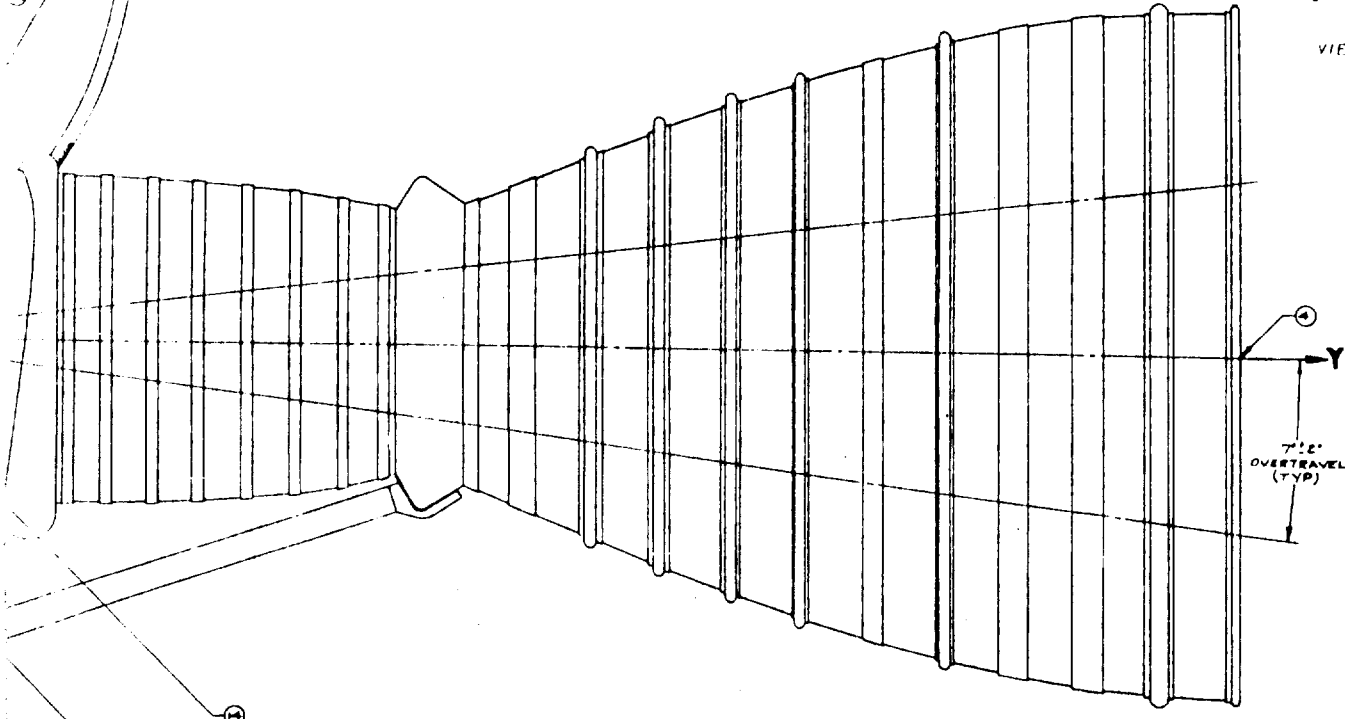
VIEW C-C



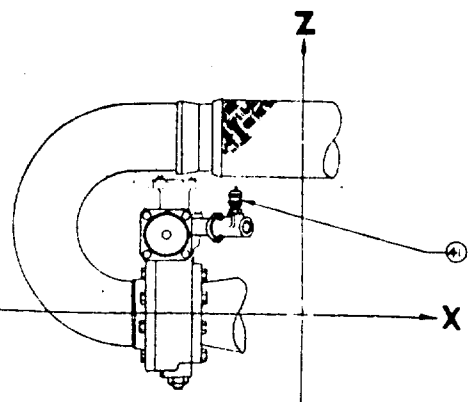
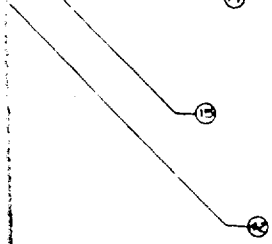
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VIEW **B-B** 17

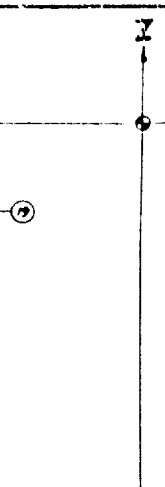


NO	OF	REV	DATE	BY	CHKD	DESCRIPTION
1	(1)	0				- 0.00
2	(1)	10				- 2.00
3	(1)	9				0.00
4	(1)	4				0.00
5	(1)	6				0.00
6	(1)	6				0.00
7	(1)	12				- 2.00
8	(1)	14				- 2.00
9	(1)	13				- 0.12
10	(1)	10				- 0.12
11	(1)	12				0.00
12	(1)	5				- 7.00
13	(1)	6				0.00
14	(1)	5				- 3.75
15	(1)	6				- 2.15
16	(1)	8				- 3.30
17	(1)	6				- 3.19
18	(1)	4				- 2.93
19	(1)	4				1.12
20	(1)	9				- 0.00
21	(1)	9				0.00
22	(1)	9				0.00
23	(1)	10				- 0.00
24	(1)	10				- 3.90
25	(1)	18				- 1.50
26	(1)	11				- 2.00
27	(1)	11				- 3.50
28	(1)	10				- 1.90
29	(1)	9				- 1.81
30	(1)	9				- 1.81
31	(1)	13				- 1.72
32	(1)	13				- 1.72
33	(1)	13				- 1.72
34	(1)	13				- 1.72
35	(1)	13				- 1.72
36	(1)	12				- 1.72
37	(1)	10				- 1.72
38	(1)	9				- 1.72
39	(1)	12				- 1.72
40	(1)	11				- 1.72
41	(1)	4				- 1.72
42	(1)	6				- 1.72
43	(1)	18				- 1.72
44	(1)	10				- 1.72
45	(1)	10				- 1.72
46	(1)	10				- 1.72
47	(1)	11				- 1.72
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50	(1)	7				- 1.72



VIEW **G-G** 12

5

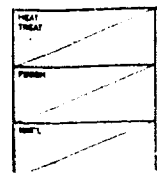


D-B 7

POINT	TYPE OF CONNECTION	Z	DISTANCES FROM ORIGIN			DESCRIPTION	END OF CONNECTION
			X	Y	Z		
1	0	0	20.719	0.000	16.477	MOUNT ATTACH TO MISSILE	
2	0	0	20.719	0.000	16.477	MOUNT ATTACH TO MISSILE	
3	0	0	0.000	0.000	16.477	MOUNT ATTACH TO MISSILE	
4	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	40 02E 0 0
5	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
6	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
7	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
8	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
9	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
10	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
11	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
12	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
13	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
14	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
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18	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
19	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
20	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
21	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
22	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
23	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
24	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
25	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
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56	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
57	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
58	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
59	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
60	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
61	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
62	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
63	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
64	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
65	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
66	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
67	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
68	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
69	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
70	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
71	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
72	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
73	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
74	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
75	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
76	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
77	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
78	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
79	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
80	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
81	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
82	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
83	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
84	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
85	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
86	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
87	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
88	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
89	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
90	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
91	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
92	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
93	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
94	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
95	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
96	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
97	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
98	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
99	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1
100	0	0	0.000	14.350	0.000	END OF THRUST CHAMBER	PER MS 33650-1

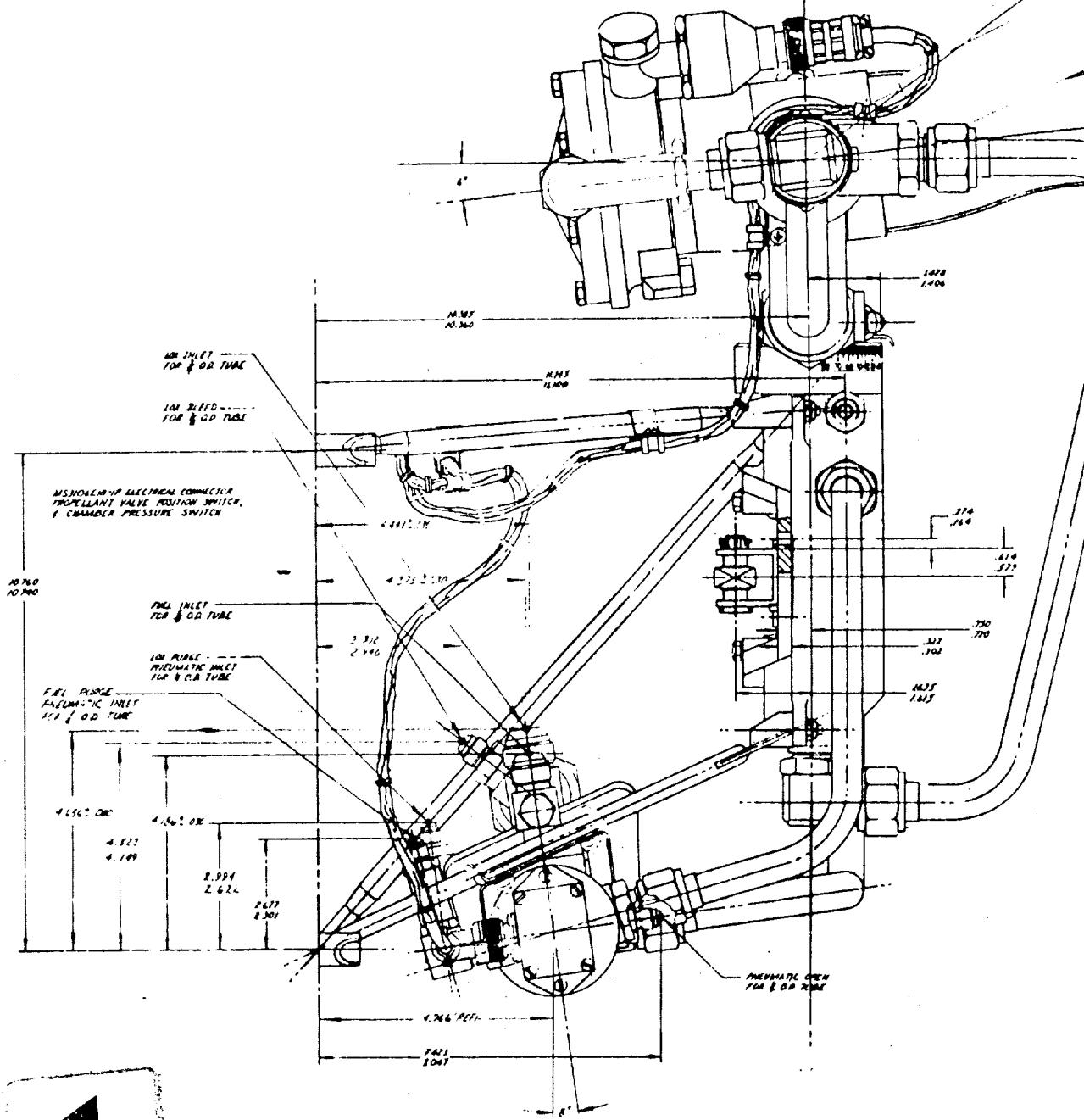
6

- ① THE BRUNING CO, LINCOLN, NEBRASKA
- ② THESE DIMS NOT TO BE HELD TO ± 1% TOLERANCE
- ③ BENDIX AVIATION CORP SCITILLA DIVISION, NEW YORK
- ④ CHANGE OF DIM WITH FULL TANK - 20 (MAX)
- ⑤ SYMBOL Ⓞ DENOTES ORIGIN OF REFERENCE
- ⑥ SYSTEM POSITIVE DIRECTIONS FROM ORIGIN ARE INDICATED BY ARROWHEADS ON AXES
- ⑦ FOR ALIGNMENT TOLERANCES REFER TO 9572 94000-4
- ⑧ TOLERANCES ± 1% FOR DIMENSIONED CUSTOMER CONNECTIONS
- ⑨ EFFECTIVE ON PLR 79-1413 ENGINES
- ⑩ E. B. WIGGINS OIL TOOL CO., LOS ANGELES 23, CALIF
- ⑪ SOUTHWEST PRODUCTS CO., DUARTE, CALIF
- ⑫ SERVICE CONNECTION
- ⑬ CUSTOMER CONNECTION TO MISSILE



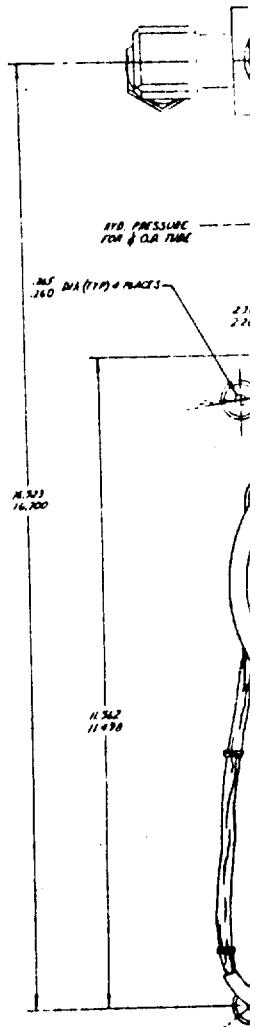
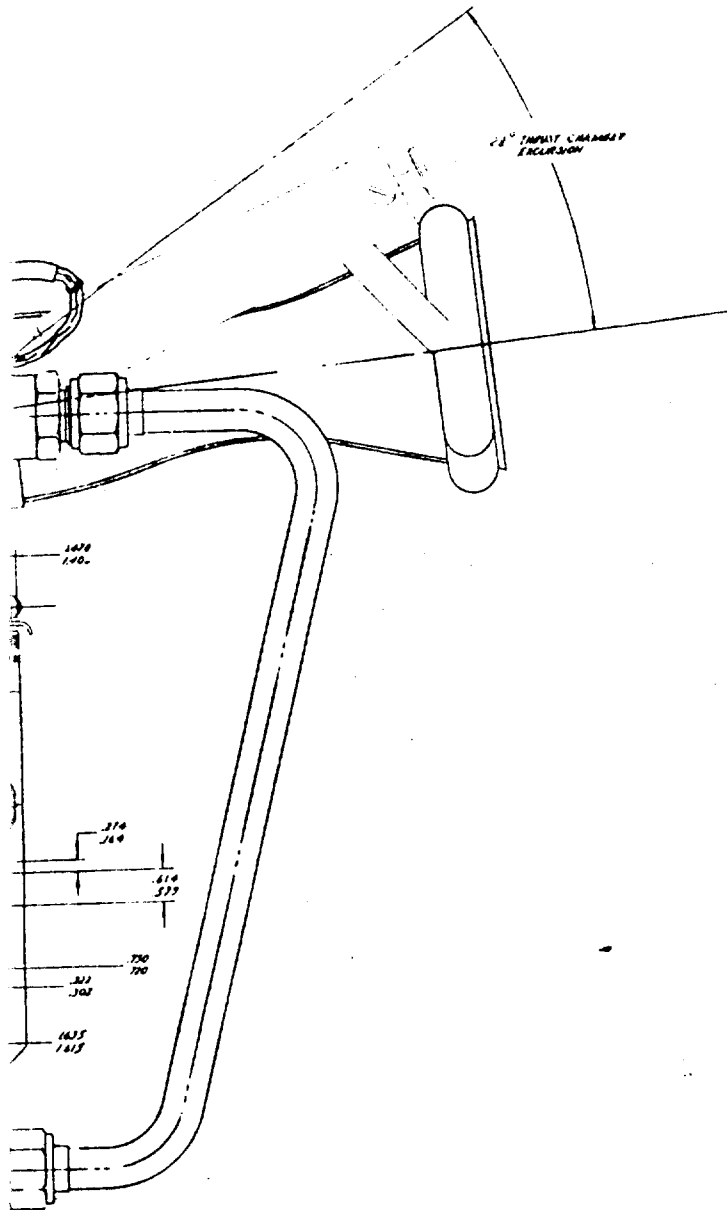
30102

13

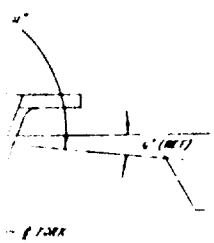


1

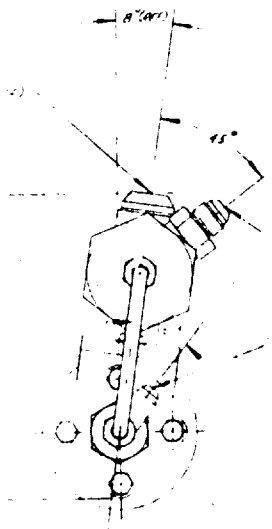
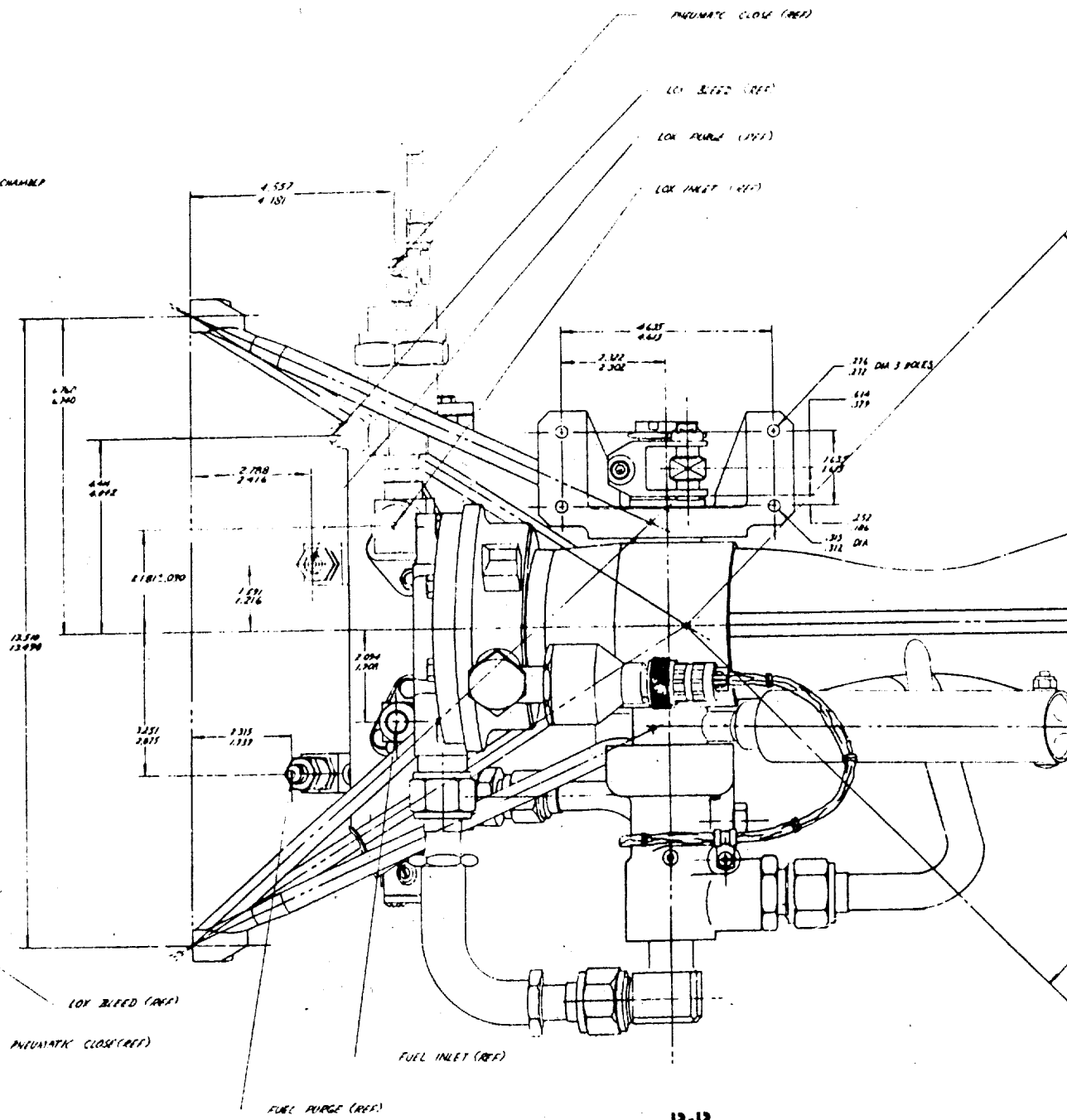
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2



PITCH / ROLL AXIS
7



FUEL INLET (REF)

FUEL PURGE (REF)

NEW 13-13

ADJACENT PARTS OMITTED FOR CLARITY

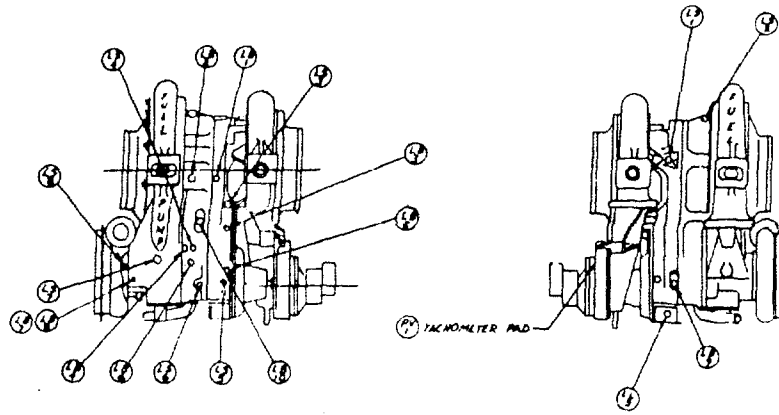
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REV	DATE	BY	DESCRIPTION

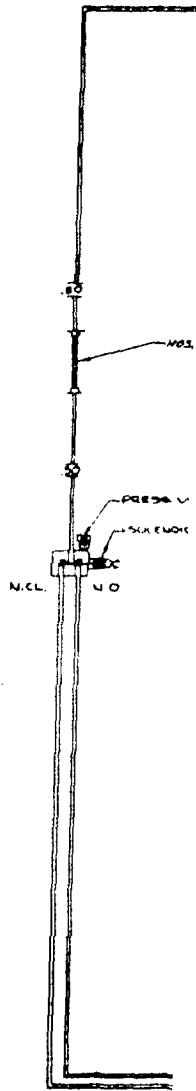
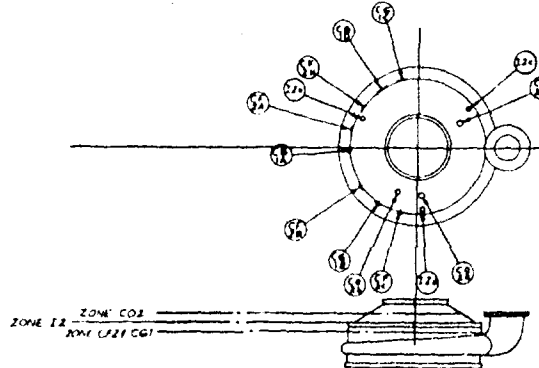
6

1. FOR CUSTOMER CONNECTIONS ON 3LR-101-NA-11.
NOTE: USE OTHER NOTES APPLICABLE

SERIALS HOLD POLARIZATION 0120 TO 1200-0-000 - 000 1120 TO 2000-0-000 - 000 2120 TO 3000-0-000 - 000 3120 TO 4000-0-000 - 000 4120 TO 5000-0-000 - 000 5120 TO 6000-0-000 - 000	CHECKED BY: [] DATE: [] BY: [] TITLE: []	CUSTOMERS CONNECTION - VERNIER ENGINE	ROCKETDYNE A DIVISION OF NORTH AMERICAN AVIATION, INC. 4840 CANON AVE. CANON, CALIFORNIA
6000 TO 7000-0-000 - 000 7000 TO 8000-0-000 - 000 8000 TO 9000-0-000 - 000 9000 TO 10000-0-000 - 000	APPROVED BY: [] DATE: [] BY: [] TITLE: []	PART NO. [] REV. []	350724 J

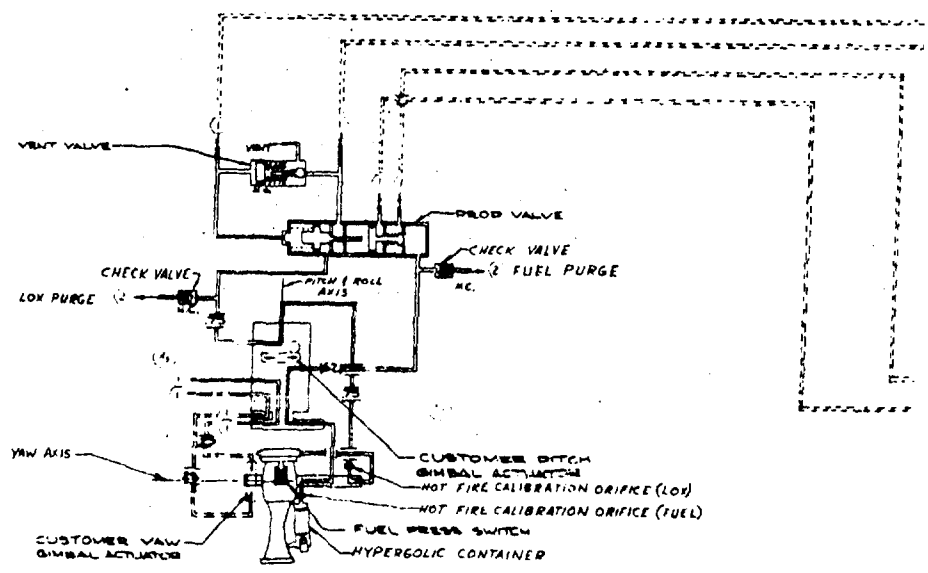


TURBOPUMP TAP POINT LOCATIONS

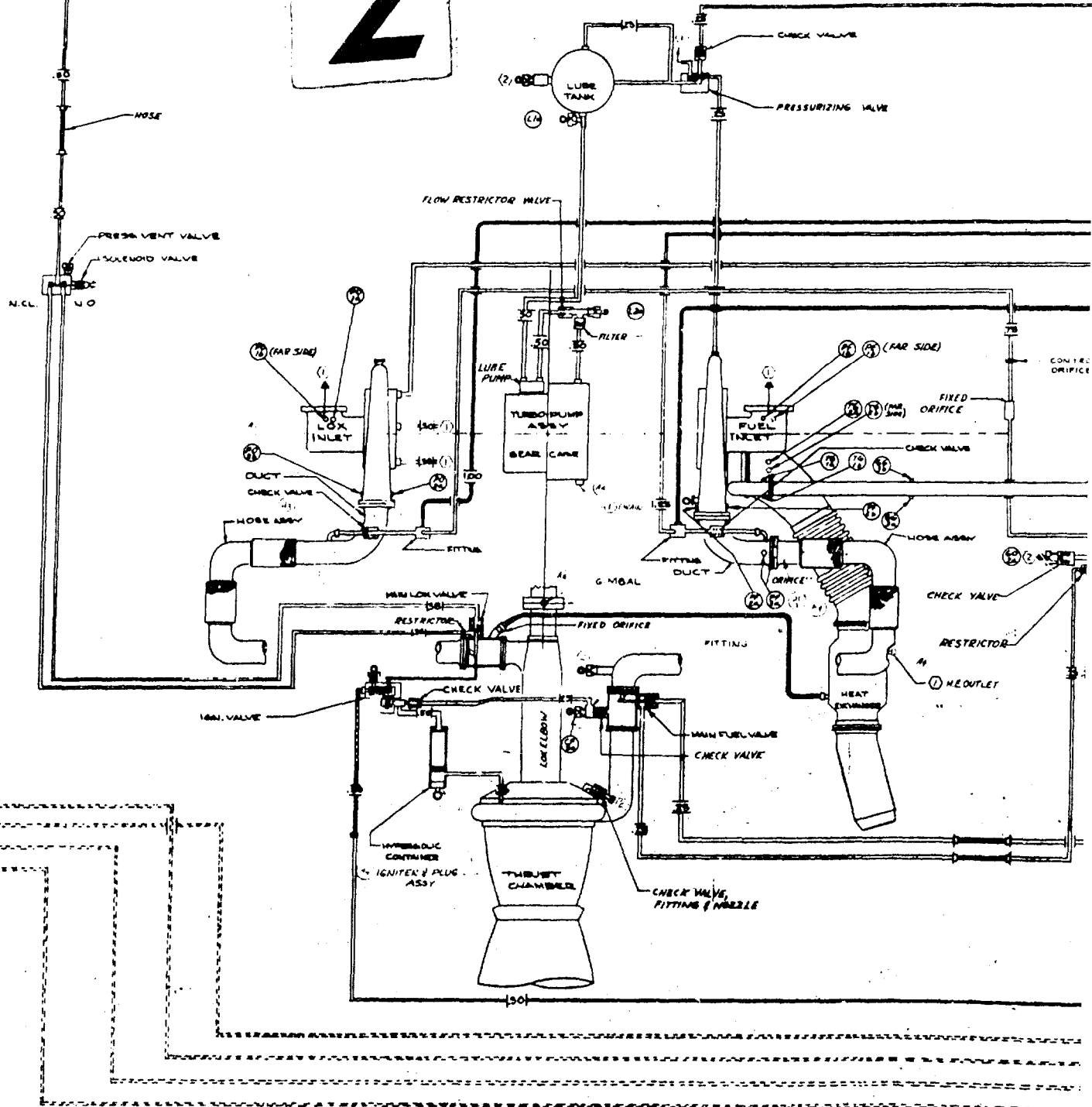


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1



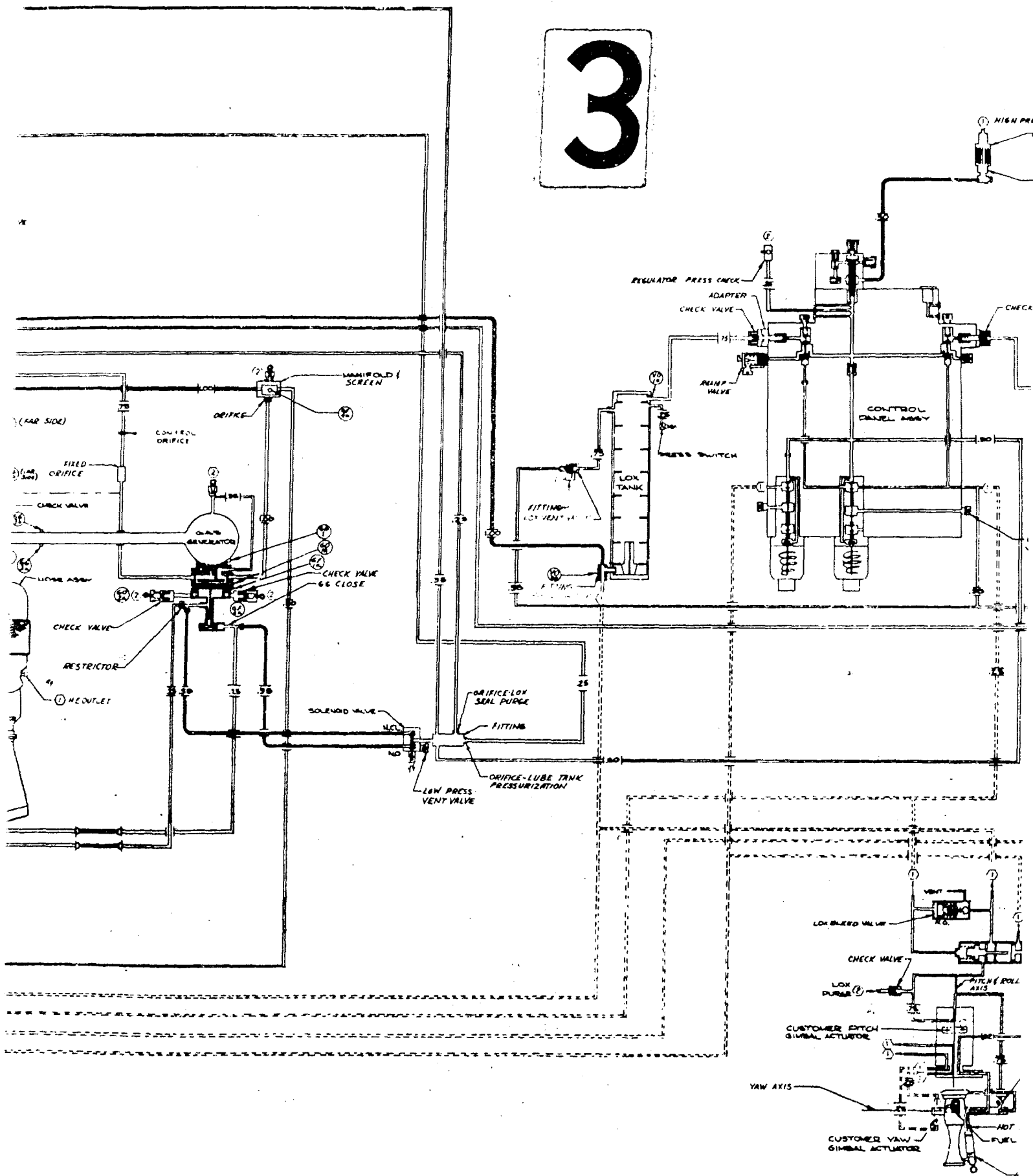
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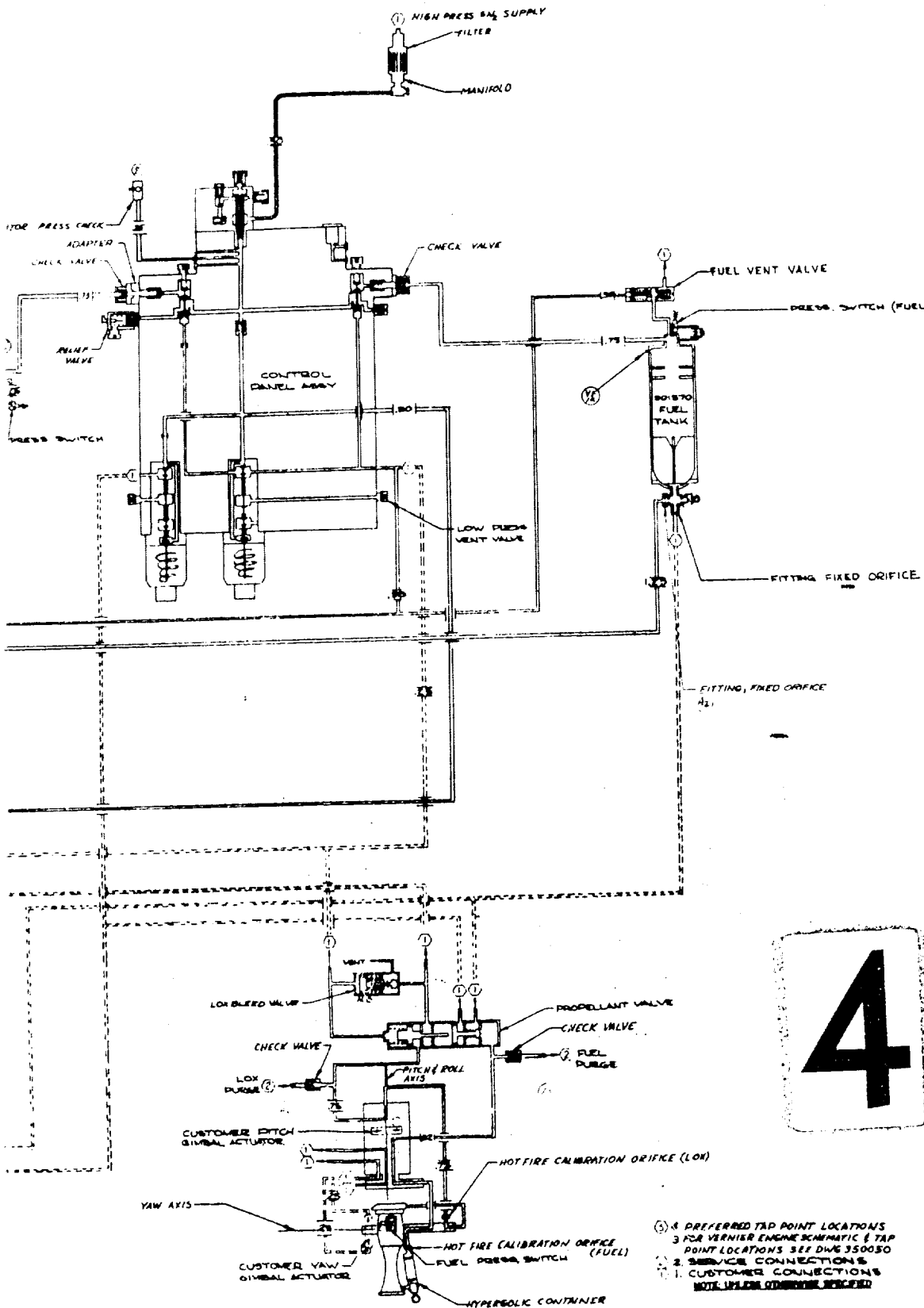


URG

100
50
ON ORIFICE (LOX)
ON ORIFICE (FUEL)

3





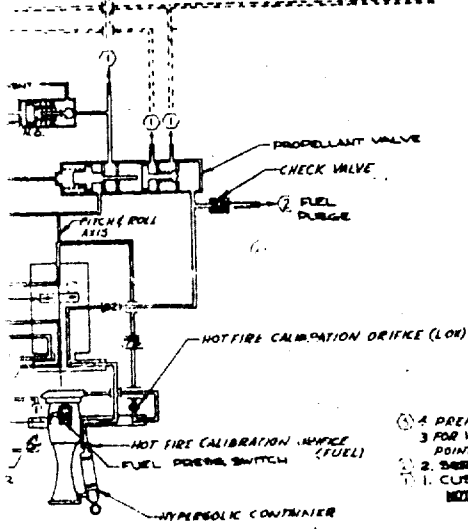
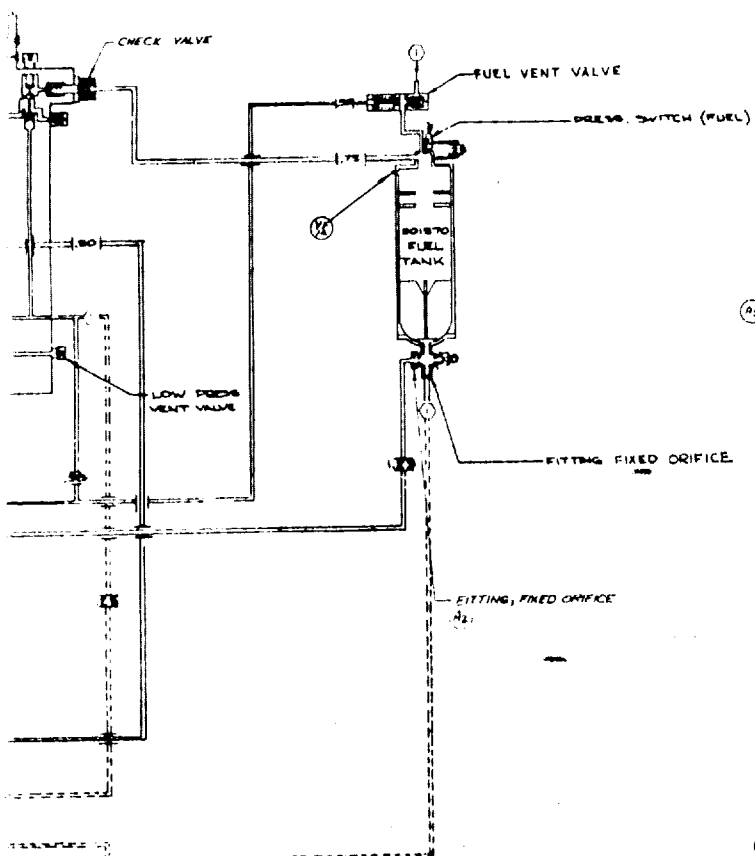
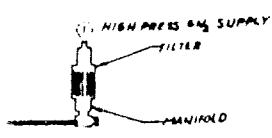
APPROX. TAG	TAP LOCATION
101	TC FUEL INLET MANIFOLD
102	TC FUEL INJECTION
103	TC FUEL INJECTION
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299	TC FUEL INJECTION
300	TC FUEL INJECTION

4

1. CUSTOMER CONNECTIONS
 2. SERVICE CONNECTIONS
 3. PREFERRED TAP POINT LOCATIONS
 4. FOR VERNIER ENGINE SCHEMATIC & TAP POINT LOCATIONS SEE DIVE 350050
 NOTE: UNLESS OTHERWISE SPECIFIED

ITEM	UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES AND APPLY PRIOR TO FINISH UNLESS INDICATED OTHERWISE	AS BY
1	1/2" DIA. HOLES	1/2"
2	3/4" DIA. HOLES	3/4"
3	1" DIA. HOLES	1"
4	1 1/2" DIA. HOLES	1 1/2"
5	2" DIA. HOLES	2"
6	2 1/2" DIA. HOLES	2 1/2"
7	3" DIA. HOLES	3"
8	3 1/2" DIA. HOLES	3 1/2"
9	4" DIA. HOLES	4"
10	4 1/2" DIA. HOLES	4 1/2"
11	5" DIA. HOLES	5"
12	5 1/2" DIA. HOLES	5 1/2"
13	6" DIA. HOLES	6"
14	6 1/2" DIA. HOLES	6 1/2"
15	7" DIA. HOLES	7"
16	7 1/2" DIA. HOLES	7 1/2"
17	8" DIA. HOLES	8"
18	8 1/2" DIA. HOLES	8 1/2"
19	9" DIA. HOLES	9"
20	9 1/2" DIA. HOLES	9 1/2"
21	10" DIA. HOLES	10"
22	10 1/2" DIA. HOLES	10 1/2"
23	11" DIA. HOLES	11"
24	11 1/2" DIA. HOLES	11 1/2"
25	12" DIA. HOLES	12"
26	12 1/2" DIA. HOLES	12 1/2"
27	13" DIA. HOLES	13"
28	13 1/2" DIA. HOLES	13 1/2"
29	14" DIA. HOLES	14"
30	14 1/2" DIA. HOLES	14 1/2"
31	15" DIA. HOLES	15"
32	15 1/2" DIA. HOLES	15 1/2"
33	16" DIA. HOLES	16"
34	16 1/2" DIA. HOLES	16 1/2"
35	17" DIA. HOLES	17"
36	17 1/2" DIA. HOLES	17 1/2"
37	18" DIA. HOLES	18"
38	18 1/2" DIA. HOLES	18 1/2"
39	19" DIA. HOLES	19"
40	19 1/2" DIA. HOLES	19 1/2"
41	20" DIA. HOLES	20"
42	20 1/2" DIA. HOLES	20 1/2"
43	21" DIA. HOLES	21"
44	21 1/2" DIA. HOLES	21 1/2"
45	22" DIA. HOLES	22"
46	22 1/2" DIA. HOLES	22 1/2"
47	23" DIA. HOLES	23"
48	23 1/2" DIA. HOLES	23 1/2"
49	24" DIA. HOLES	24"
50	24 1/2" DIA. HOLES	24 1/2"
51	25" DIA. HOLES	25"
52	25 1/2" DIA. HOLES	25 1/2"
53	26" DIA. HOLES	26"
54	26 1/2" DIA. HOLES	26 1/2"
55	27" DIA. HOLES	27"
56	27 1/2" DIA. HOLES	27 1/2"
57	28" DIA. HOLES	28"
58	28 1/2" DIA. HOLES	28 1/2"
59	29" DIA. HOLES	29"
60	29 1/2" DIA. HOLES	29 1/2"
61	30" DIA. HOLES	30"
62	30 1/2" DIA. HOLES	30 1/2"
63	31" DIA. HOLES	31"
64	31 1/2" DIA. HOLES	31 1/2"
65	32" DIA. HOLES	32"
66	32 1/2" DIA. HOLES	32 1/2"
67	33" DIA. HOLES	33"
68	33 1/2" DIA. HOLES	33 1/2"
69	34" DIA. HOLES	34"
70	34 1/2" DIA. HOLES	34 1/2"
71	35" DIA. HOLES	35"
72	35 1/2" DIA. HOLES	35 1/2"
73	36" DIA. HOLES	36"
74	36 1/2" DIA. HOLES	36 1/2"
75	37" DIA. HOLES	37"
76	37 1/2" DIA. HOLES	37 1/2"
77	38" DIA. HOLES	38"
78	38 1/2" DIA. HOLES	38 1/2"
79	39" DIA. HOLES	39"
80	39 1/2" DIA. HOLES	39 1/2"
81	40" DIA. HOLES	40"
82	40 1/2" DIA. HOLES	40 1/2"
83	41" DIA. HOLES	41"
84	41 1/2" DIA. HOLES	41 1/2"
85	42" DIA. HOLES	42"
86	42 1/2" DIA. HOLES	42 1/2"
87	43" DIA. HOLES	43"
88	43 1/2" DIA. HOLES	43 1/2"
89	44" DIA. HOLES	44"
90	44 1/2" DIA. HOLES	44 1/2"
91	45" DIA. HOLES	45"
92	45 1/2" DIA. HOLES	45 1/2"
93	46" DIA. HOLES	46"
94	46 1/2" DIA. HOLES	46 1/2"
95	47" DIA. HOLES	47"
96	47 1/2" DIA. HOLES	47 1/2"
97	48" DIA. HOLES	48"
98	48 1/2" DIA. HOLES	48 1/2"
99	49" DIA. HOLES	49"
100	49 1/2" DIA. HOLES	49 1/2"
101	50" DIA. HOLES	50"

REVISED		
NO.	DATE	DESCRIPTION
A		1. MAY BE RETROFITTED 2. RECORD LAYOUTS 3. CAPACITY OF RESERVOIR 4. NEW SHOP PRACTICE 5. PARTS MADE OR
1	7-5	1. REEL-WELL CONTROL VALVE FROM ENGINE 5 TO ENGINE 6 2. REMOVED MANUAL ON THE FULL NOMINAL ORIFICE LOW EDUCATIONAL INSTRUMENTAL VALVE 3. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20) (21) (22) (23) (24) (25) (26) (27) (28) (29) (30) (31) (32) (33) (34) (35) (36) (37) (38) (39) (40) (41) (42) (43) (44) (45) (46) (47) (48) (49) (50) (51) (52) (53) (54) (55) (56) (57) (58) (59) (60) (61) (62) (63) (64) (65) (66) (67) (68) (69) (70) (71) (72) (73) (74) (75) (76) (77) (78) (79) (80) (81) (82) (83) (84) (85) (86) (87) (88) (89) (90) (91) (92) (93) (94) (95) (96) (97) (98) (99) (100)
2	7-6	1. ADDED (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20) (21) (22) (23) (24) (25) (26) (27) (28) (29) (30) (31) (32) (33) (34) (35) (36) (37) (38) (39) (40) (41) (42) (43) (44) (45) (46) (47) (48) (49) (50) (51) (52) (53) (54) (55) (56) (57) (58) (59) (60) (61) (62) (63) (64) (65) (66) (67) (68) (69) (70) (71) (72) (73) (74) (75) (76) (77) (78) (79) (80) (81) (82) (83) (84) (85) (86) (87) (88) (89) (90) (91) (92) (93) (94) (95) (96) (97) (98) (99) (100)
3	7-7	1. ADDED (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20) (21) (22) (23) (24) (25) (26) (27) (28) (29) (30) (31) (32) (33) (34) (35) (36) (37) (38) (39) (40) (41) (42) (43) (44) (45) (46) (47) (48) (49) (50) (51) (52) (53) (54) (55) (56) (57) (58) (59) (60) (61) (62) (63) (64) (65) (66) (67) (68) (69) (70) (71) (72) (73) (74) (75) (76) (77) (78) (79) (80) (81) (82) (83) (84) (85) (86) (87) (88) (89) (90) (91) (92) (93) (94) (95) (96) (97) (98) (99) (100)
4	7-8	1. ADDED (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20) (21) (22) (23) (24) (25) (26) (27) (28) (29) (30) (31) (32) (33) (34) (35) (36) (37) (38) (39) (40) (41) (42) (43) (44) (45) (46) (47) (48) (49) (50) (51) (52) (53) (54) (55) (56) (57) (58) (59) (60) (61) (62) (63) (64) (65) (66) (67) (68) (69) (70) (71) (72) (73) (74) (75) (76) (77) (78) (79) (80) (81) (82) (83) (84) (85) (86) (87) (88) (89) (90) (91) (92) (93) (94) (95) (96) (97) (98) (99) (100)

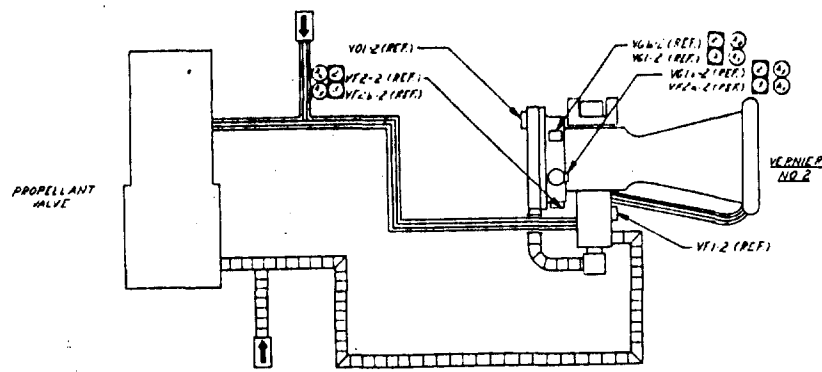
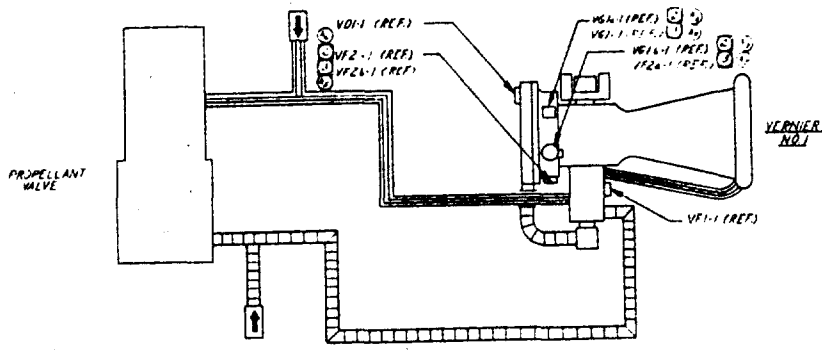


- 1. CUSTOMER CONNECTIONS
 - 2. SERVICE CONNECTIONS
 - 3. FOR VERNIER ENGINE SCHEMATIC & TAP POINT LOCATIONS SEE DWG 350050
 - 4. PREFERRED TAP POINT LOCATIONS
- NOTE: UNLESS OTHERWISE SPECIFIED

ITEM NO.	TAP LOCATION
1	TO FUEL INLET MANIFOLD
2	TO FUEL INJECTION
3	TO FUEL INJECTION
4	TO FUEL INJECTION
5	TO FUEL INJECTION
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100	TO FUEL INJECTION

5

HEAT TREAT	UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES AND DECIMAL FRACTIONS	NO. OF	REV.	SECRETIVE
FURNISH	1/16" INCH TYP. DIMENSIONS TOLERANCES ON DIMENSIONS UNLESS OTHERWISE SPECIFIED	ONE BY	DATE	A DIVISION OF NORTH AMERICAN INSTRUMENTATION, INC. CANADA PARK, CALIFORNIA
DETAIL	HOLE SIZES UNLESS OTHERWISE SPECIFIED	ONE BY	DATE	SCHEMATIC INSTRUMENTATION TAP POINT LOCATION
	DO NOT SCALE PRINT	ONE BY	DATE	CODE DRAW NO. 02602 J 702827



LINE CODE	
OXIDIZER	XXXXXXXXXXXX
FUEL	XXXXXXXXXXXX

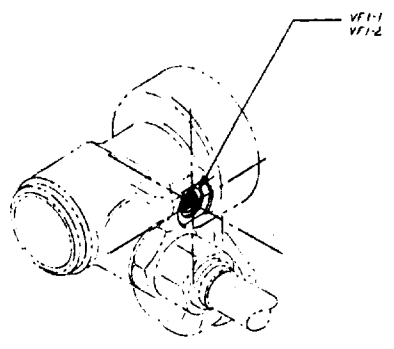
Best Available Co.

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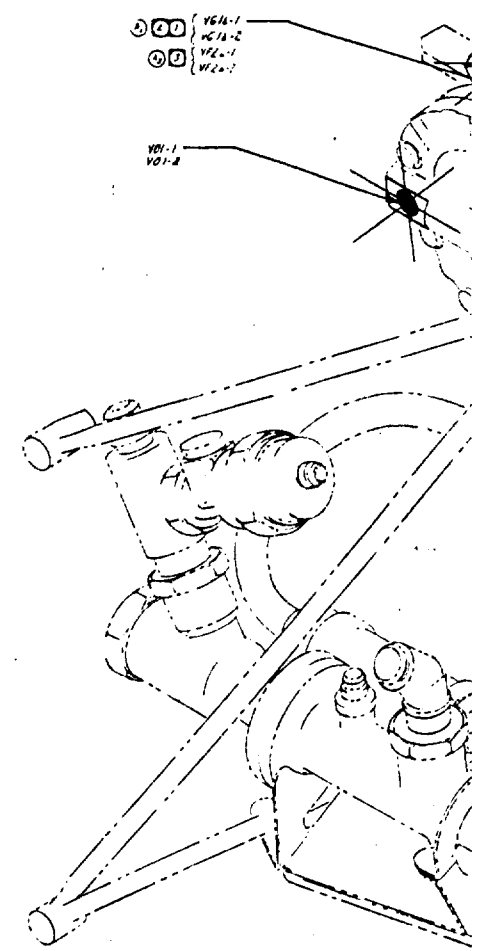
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② ② VGM-1
② ② VGM-2
② ② VGM-1
② ② VGM-2

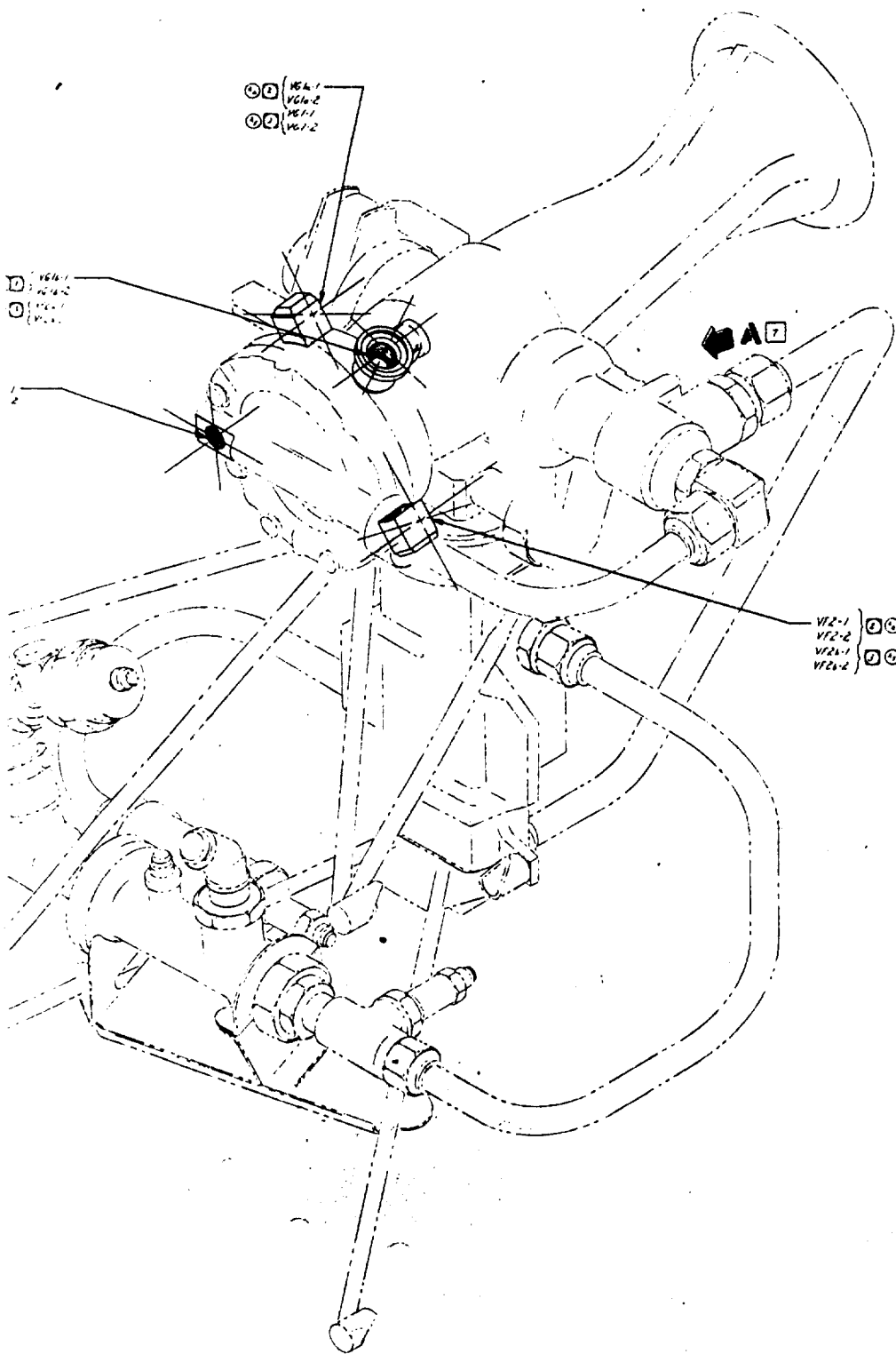
VGM-1
VGM-2



VIEW **A** 4

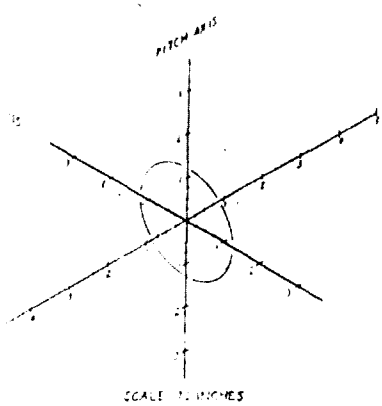


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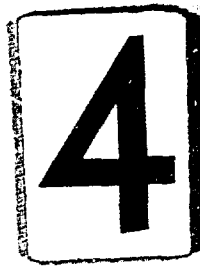
REVISED BY	DATE OF REV	REASON FOR REV
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2	2	ADDED
3	3	ADDED
4	4	ADDED
5	5	ADDED
6	6	ADDED
B		
2	7	IN EFFECT 31-10-57
C		
2	1	ADDED RELIABLE
1	2	ADDED FOR R.



TAP NO	DESCRIPTION	TAP SIZE	TYPE	ZONE
VE12-1	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE12-2	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE12-3	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE12-4	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE12-5	THRUST CHAMBER COMBUSTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE12-6	THRUST CHAMBER COMBUSTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-1	TRUNNION HOUSING FUEL PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-2	TRUNNION HOUSING FUEL PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-3	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-4	THRUST CHAMBER FUEL INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-5	THRUST CHAMBER COMBUSTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VE1-6	THRUST CHAMBER COMBUSTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VO1-1	THRUST CHAMBER OXIDIZER INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F
VO1-2	THRUST CHAMBER OXIDIZER INJECTION PRESSURE	1/8" TUBE	AND 1/8" O.D.	F

TAP CODE SYSTEM	
FIRST COLUMN CAPITAL LETTER DESIGNATES	LETTER COMPONENT OR SYS
MAJOR COMPONENT OR BASIC SUPPORT	V VERNIER
SECOND COLUMN CAPITAL LETTER DESIGNATES	LETTER IDENTIFICATION
NUMBER BEING SERVED BY THE OPERATING	F FUEL
LECTURE CONNECTED WITH THE TAP	S HOT GAS
	O OXIDIZER
THIRD COLUMN NUMBER IDENTIFIES TAP BY THE COMPONENT OF	THE SYSTEM
FOURTH COLUMN LETTER LOWER CASE IDENTIFIES HIGH OR	LOW TAP OR LINE POSITION LOCATED IN COMMON PLANE
NUMBER IN FIFTH COLUMN INDICATES NECESSITY OF	OTHER IDENTIFICATION
SIXTH COLUMN INDICATES THRUST CHAMBER NUMBER IN	A MULTIPLE CHAMBER CONFIGURATION

5	10034001	F	SUBS	LRP/NA-11
6	10034001	F	SUBS	LRP/NA-11
7	10034001	F	SUBS	LRP/NA-11
8	10034001	F	SUBS	LRP/NA-11
			ENGINE	THRU
				MODEL
				EFFECTIVE ON



FOR REFERENCE ONLY

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100.

| BOLTED HOLE | INSTRUMENT |
|---------------------------------|------------|
| 1.00 TO 1.250 - 1/8" - 20 | TAP |
| 1.250 TO 1.500 - 1/4" - 20 | VERNIER |
| 1.500 TO 2.000 - 3/8" - 16 | 1/30MM |
| 2.000 TO 2.500 - 1/2" - 13 | |
| 2.500 TO 3.000 - 5/8" - 11 | |
| 3.000 TO 3.500 - 3/4" - 10 | |
| 3.500 TO 4.000 - 7/8" - 9 | |
| 4.000 TO 4.500 - 1" - 8 | |
| 4.500 TO 5.000 - 1 1/8" - 7 | |
| 5.000 TO 5.500 - 1 1/4" - 7 | |
| 5.500 TO 6.000 - 1 3/8" - 6 | |
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| 6.500 TO 7.000 - 1 5/8" - 5 | |
| 7.000 TO 7.500 - 1 3/4" - 5 | |
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| 98.500 TO 99.000 - 24 5/8" - 4 | |
| 99.000 TO 99.500 - 24 3/4" - 4 | |
| 99.500 TO 100.000 - 24 7/8" - 4 | |

ELECTRICAL SYSTEM

Twenty-five to 30 volts dc (to the main engine electrical relay box) will be maintained until 0.5 second after all starting sequences have been completed, and 20 to 30 volts dc thereafter. The power required is 800 watts maximum for starting, and 300 watts is required for flight operation. The command cutoff signal shall have a minimum current capacity of 0.30 ampere and shall be sustained for a minimum of 0.10 second. Electrical supply for the heaters during preflight is 115 volts ac at 60 to 400 cps. The maximum ground power supply shall be 3000 watts.

Nominal power requirement profile charts are presented in Fig. 3, 4, and 5. Drawing 900100 is the electrical system schematic for the LV-2A propulsion system.

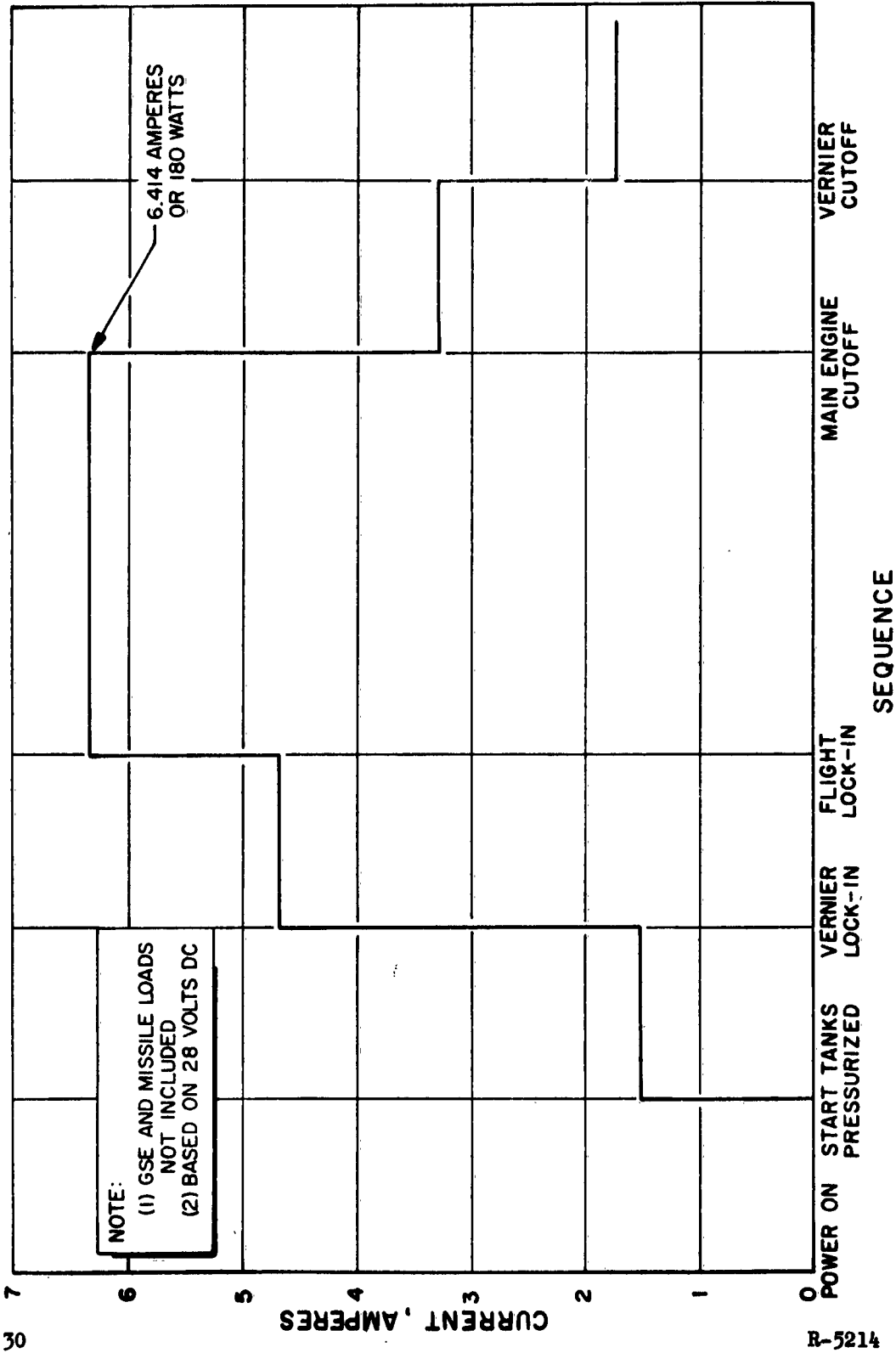


Figure 3 . Direct Current Requirements

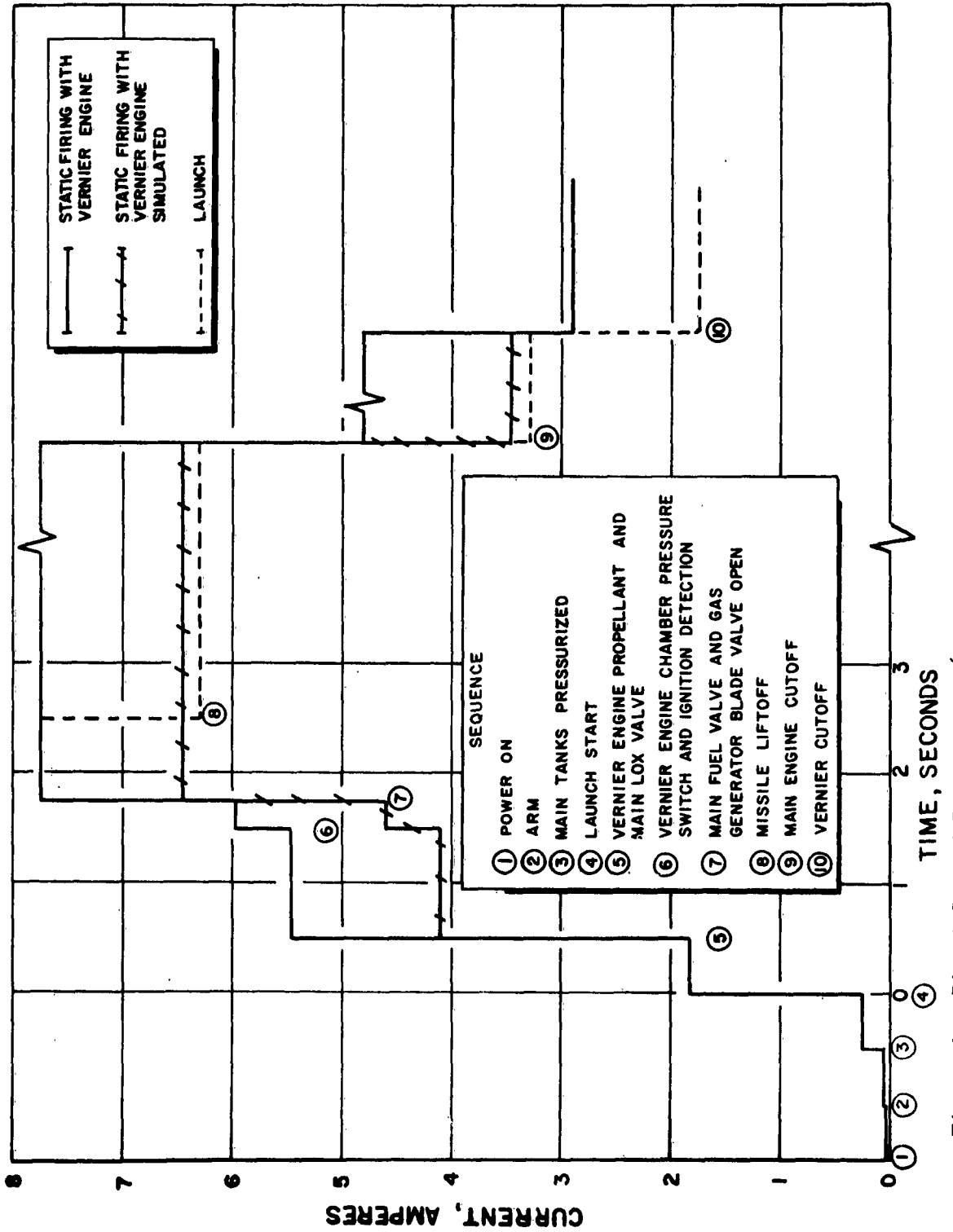


Figure 4. Direct Current Requirements (When Operated With R&D Ground Support Equipment)

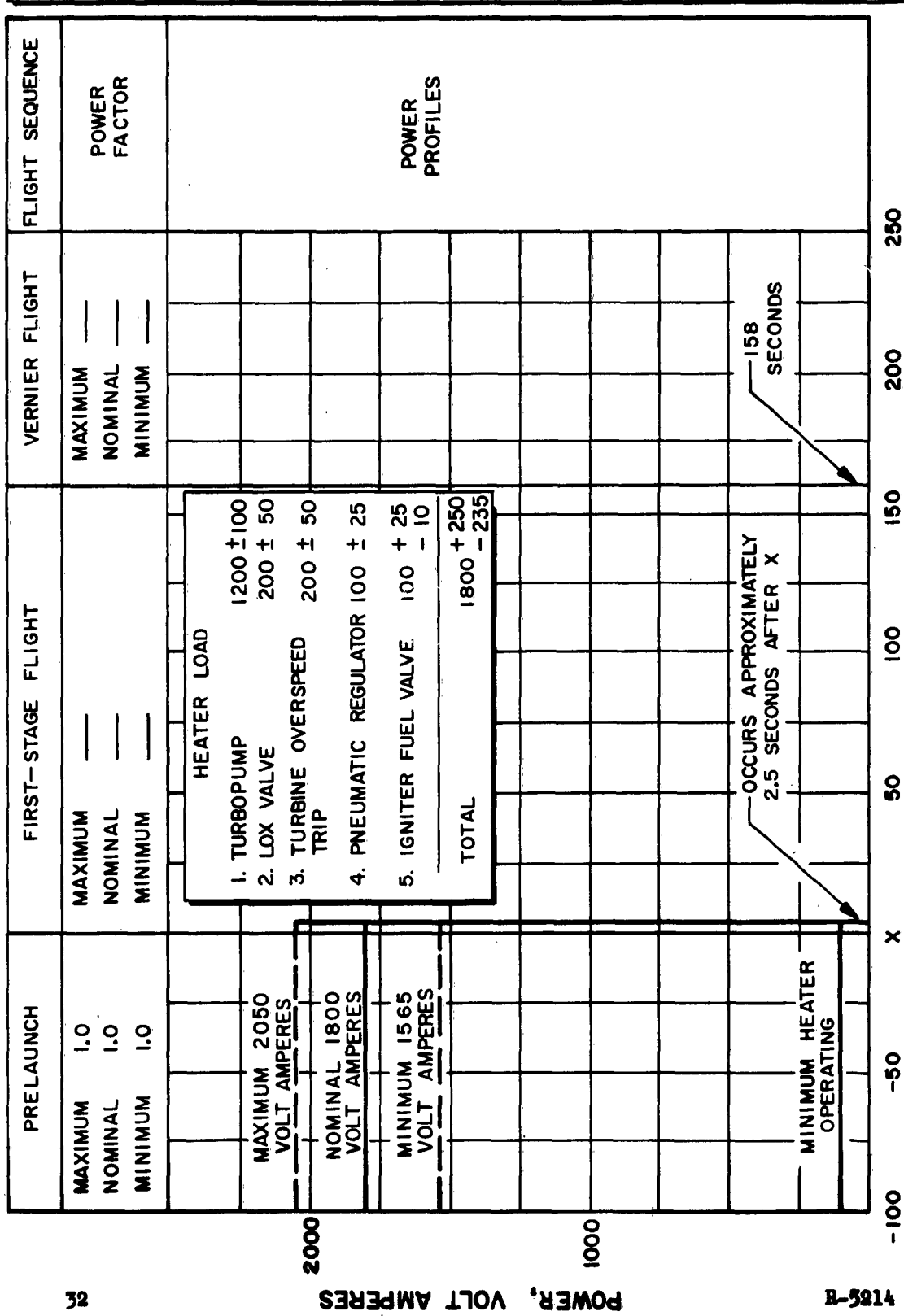
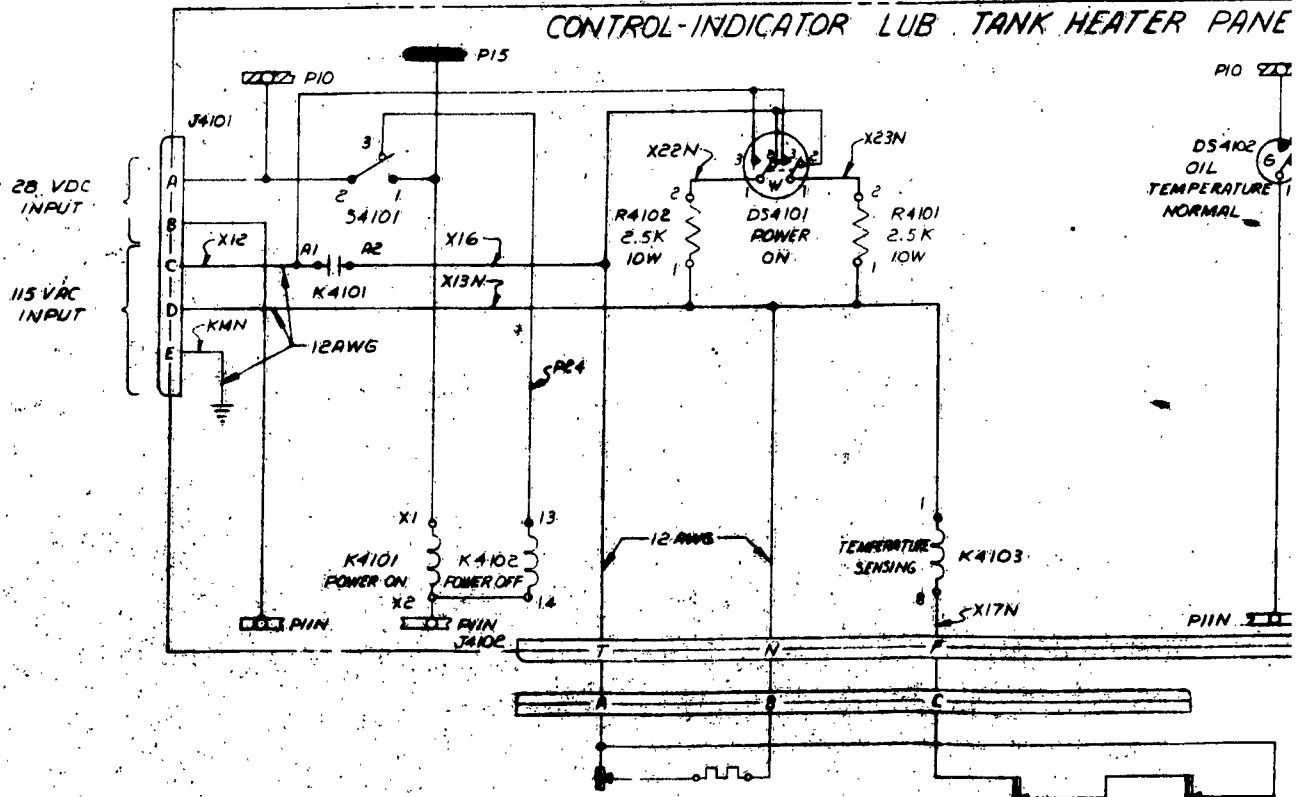


Figure 5 . Alternating Current Requirements

901008

CONTROL-INDICATOR LUB TANK HEATER PANE



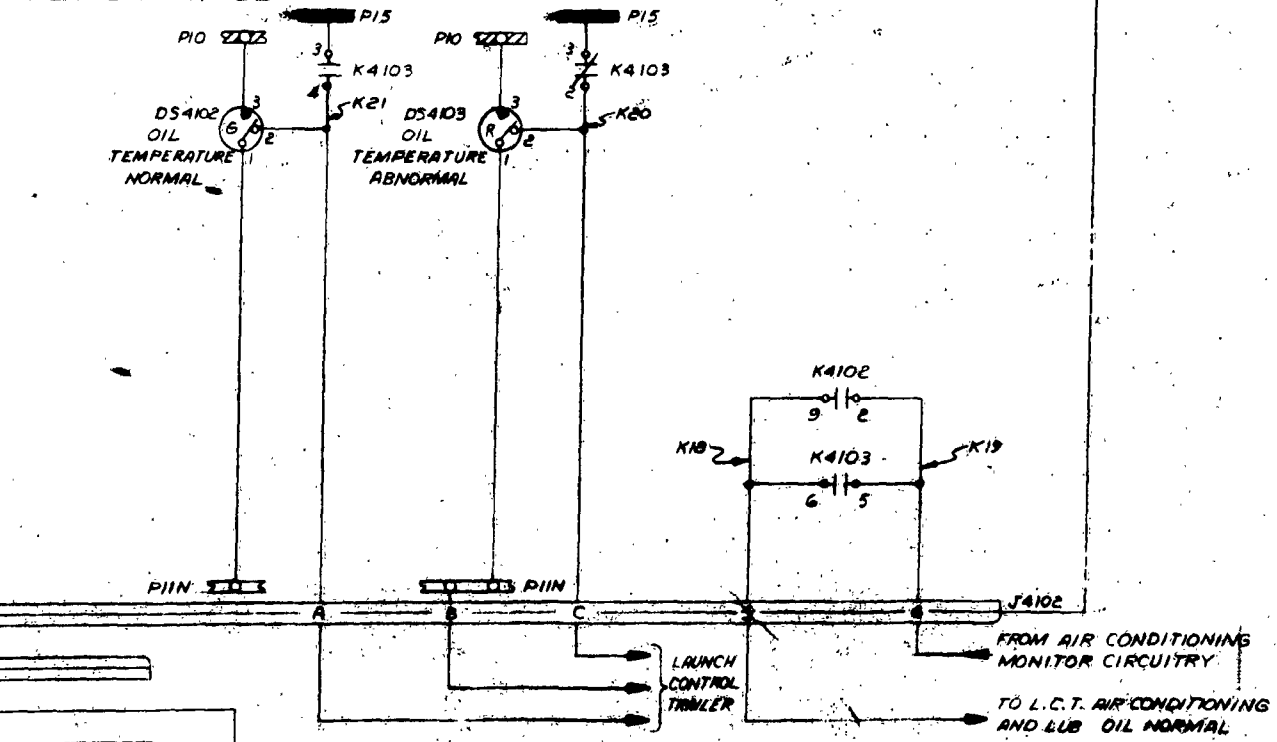
1

LUB TANK HEATER
CLOSES AT 78°F ± 5°
OPENS AT 93°F ± 5°

TANK SENSING THERMOSTAT LOW
CLOSES AT 70°F ± 5°
OPENS AT 55°F ± 5°

TANK SENSING THERMOSTAT NORMAL
CLOSES AT 70°F ± 5°
OPENS AT 55°F ± 5°

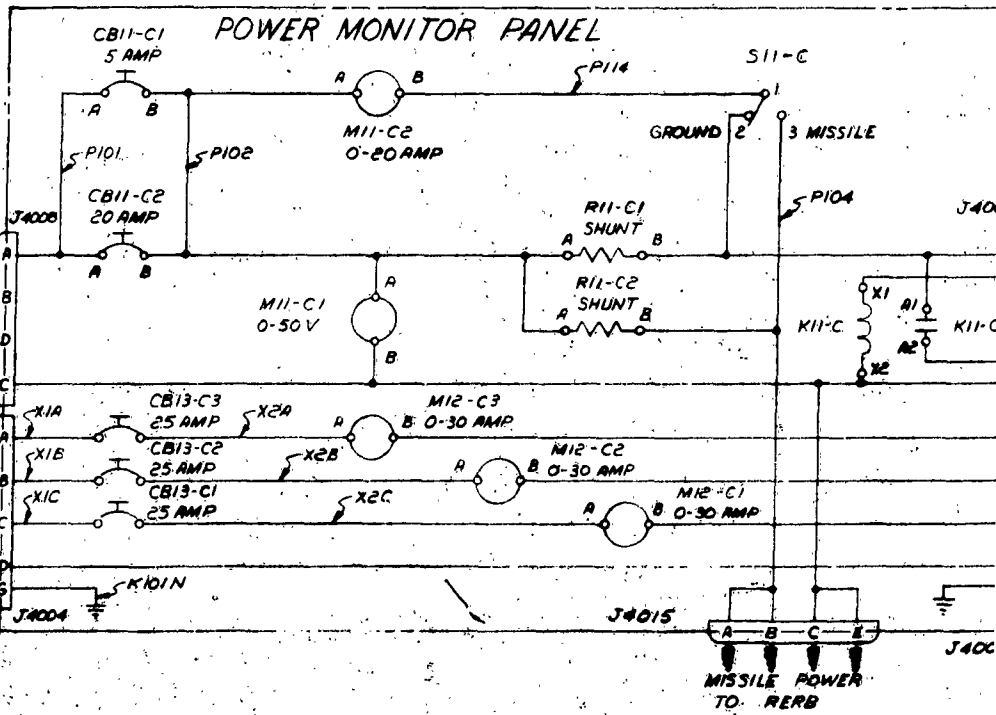
HEATER PANEL



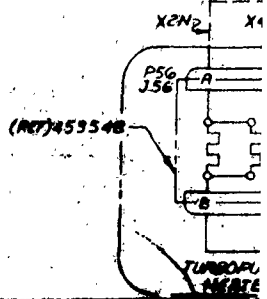
151NG
 AT LOW
 30°F ± 5°
 15°F ± 5°

TANK SENSING
 THERMOSTAT HIGH
 CLOSES 70 ± 5°
 OPENS 45 ± 5°

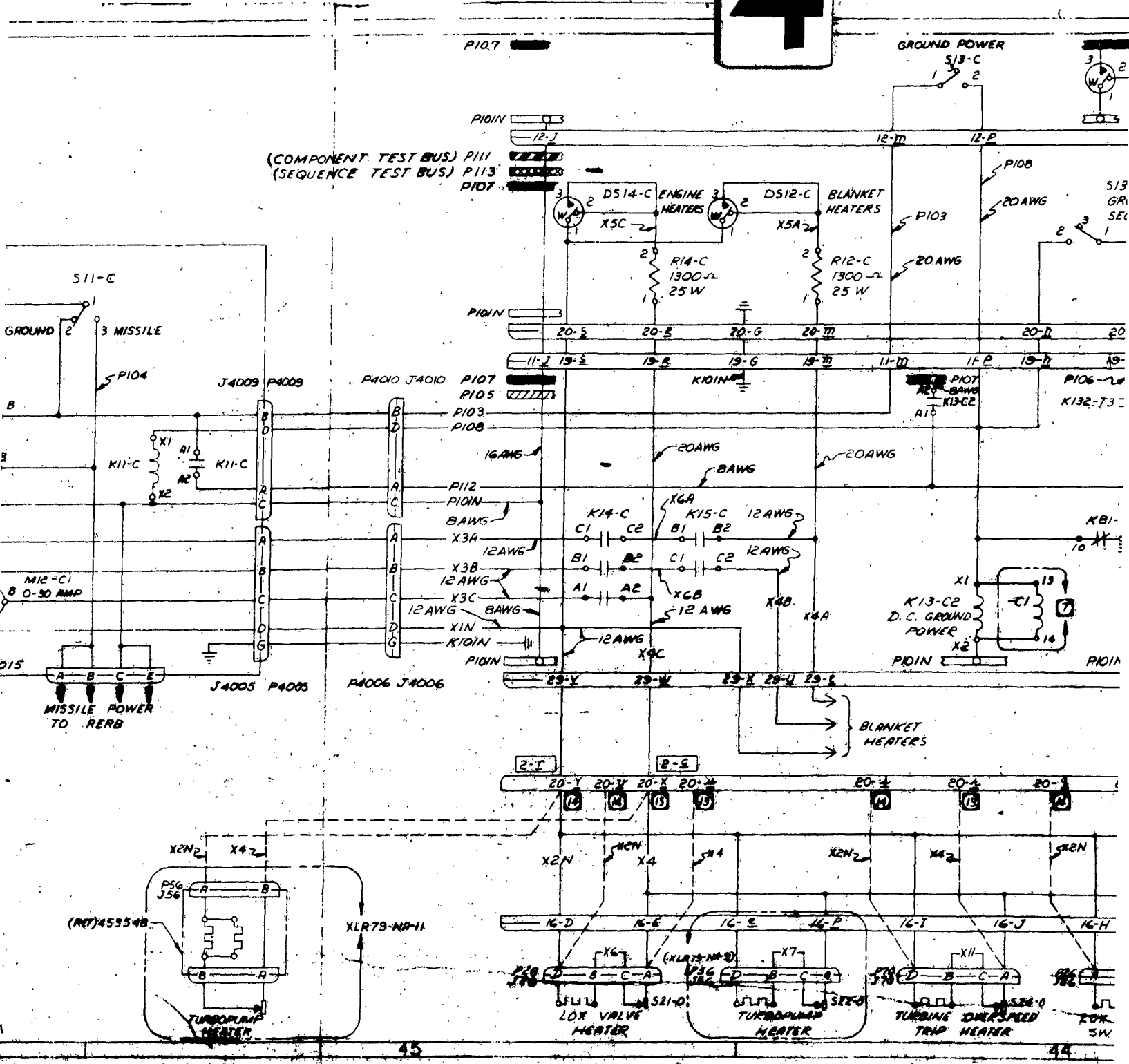


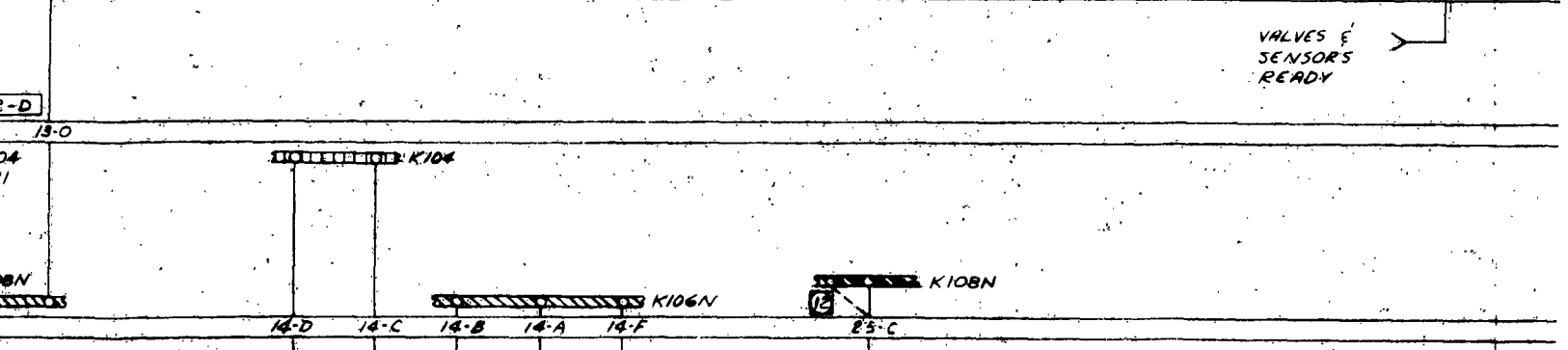
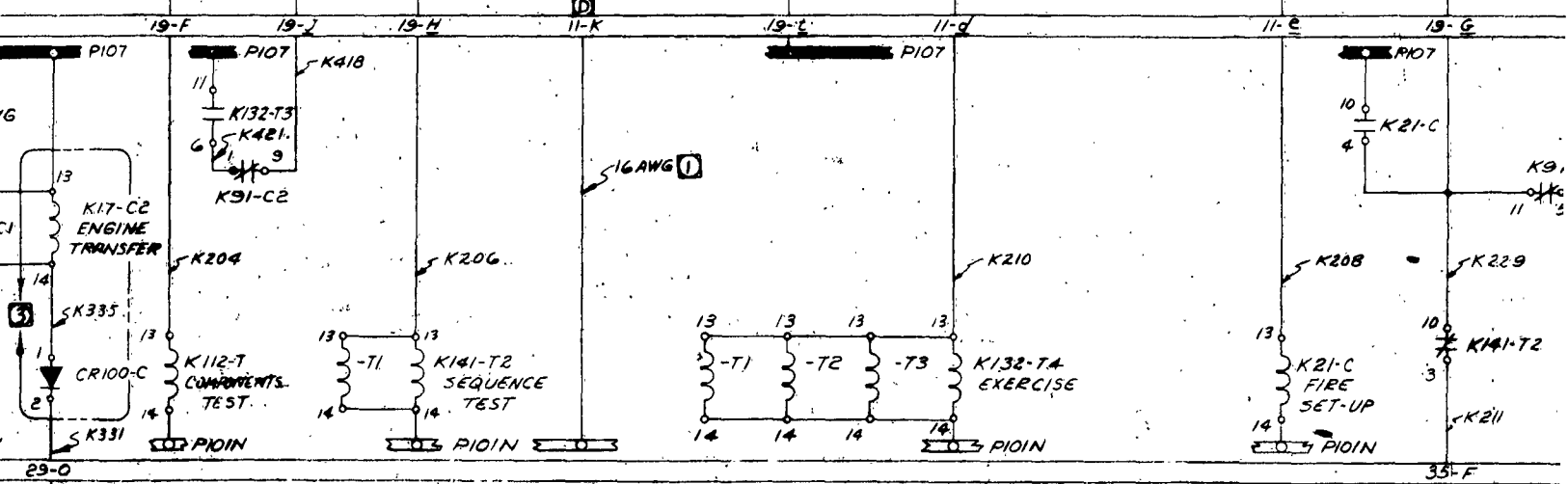
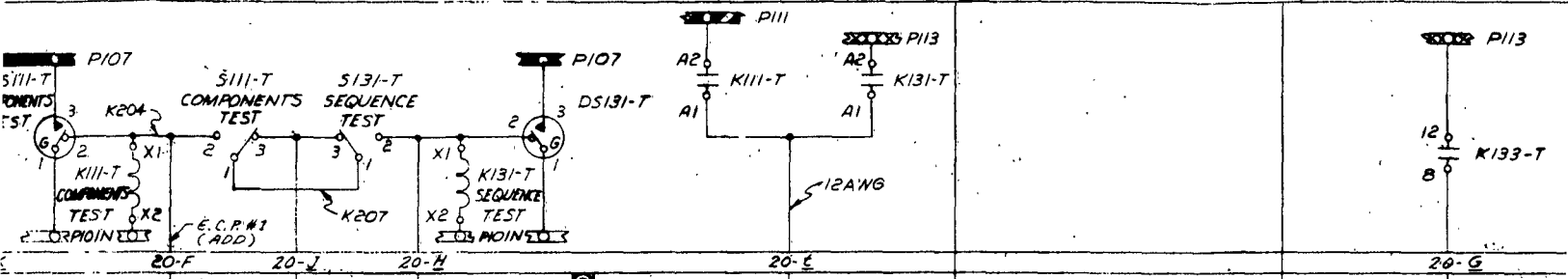
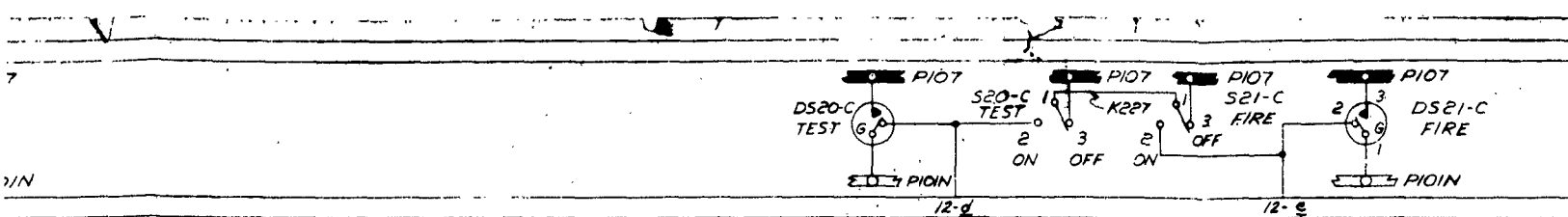


3



4



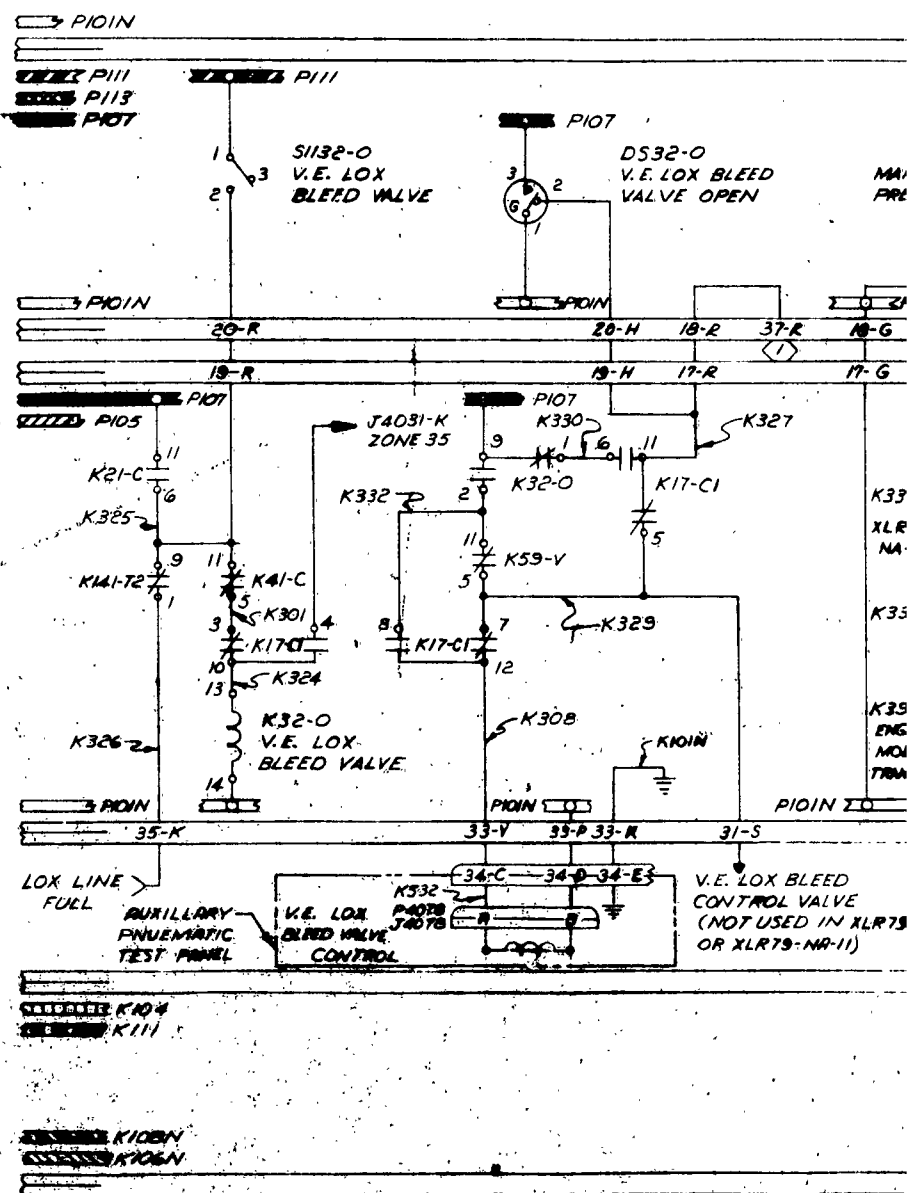
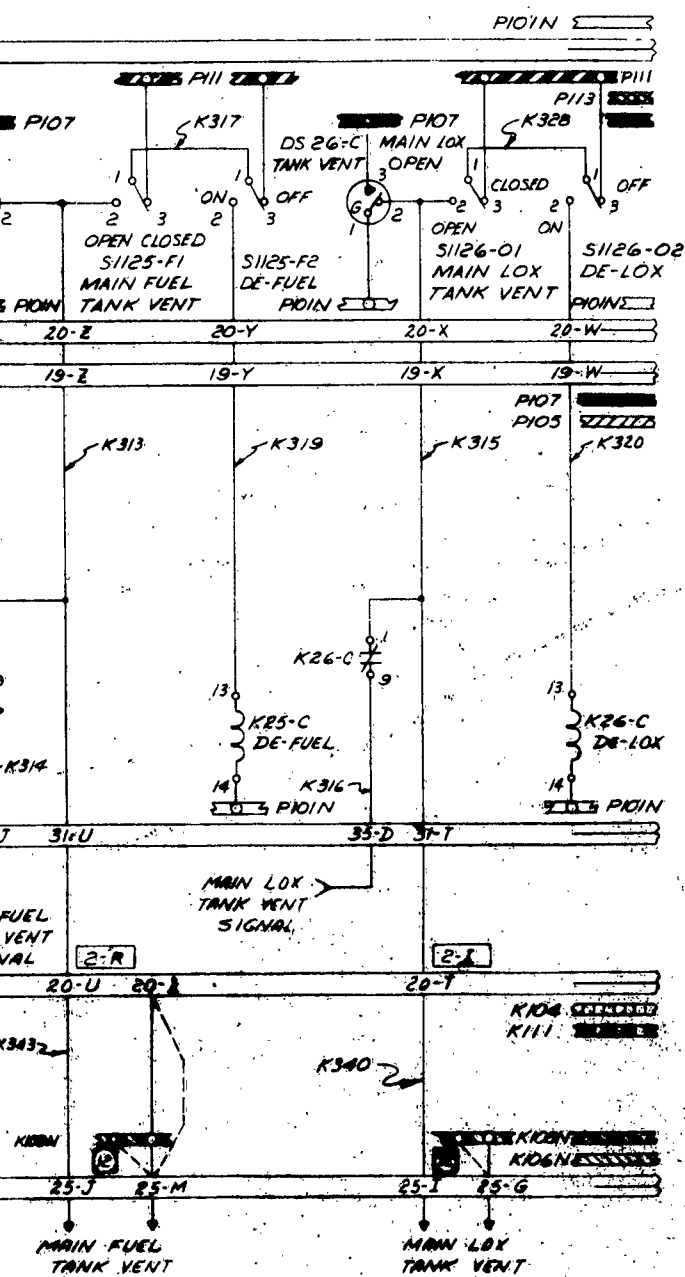


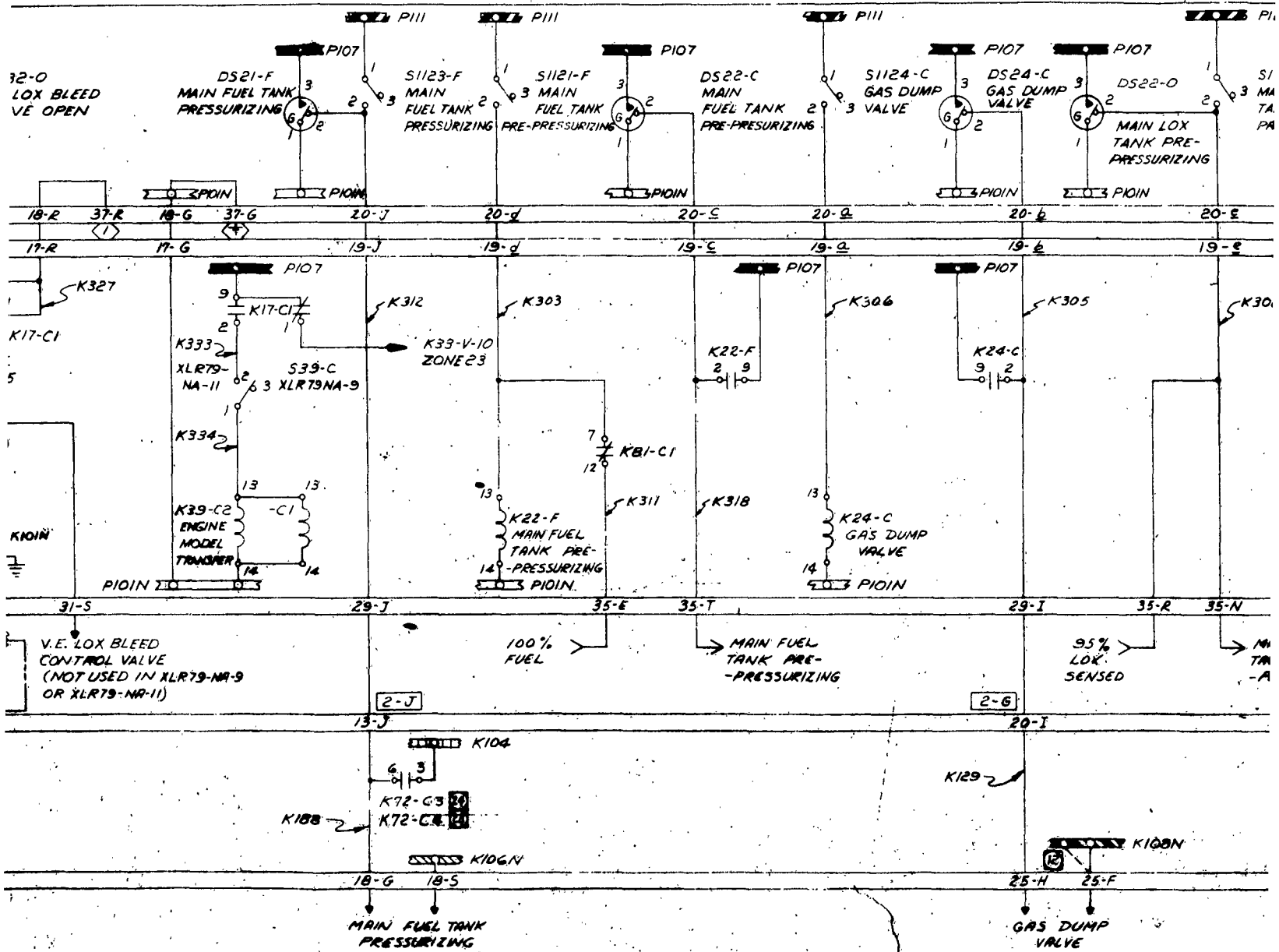
NOTE: THIS JUMPER TO BE ADDED IN THE SIMULATOR PANEL TO ACCOMPLISH THE SAME RESULTS

6

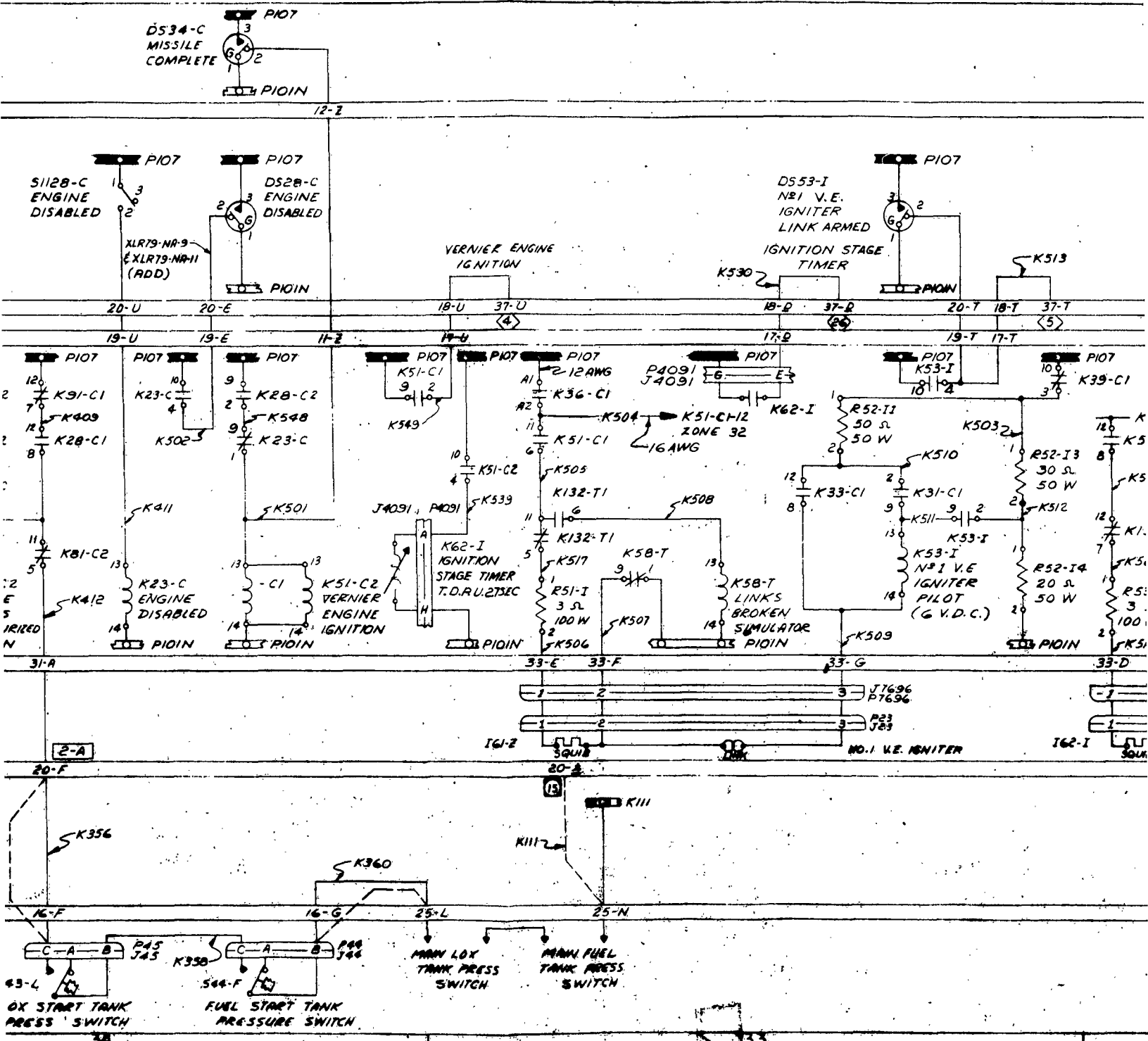
PI07

PI07





9

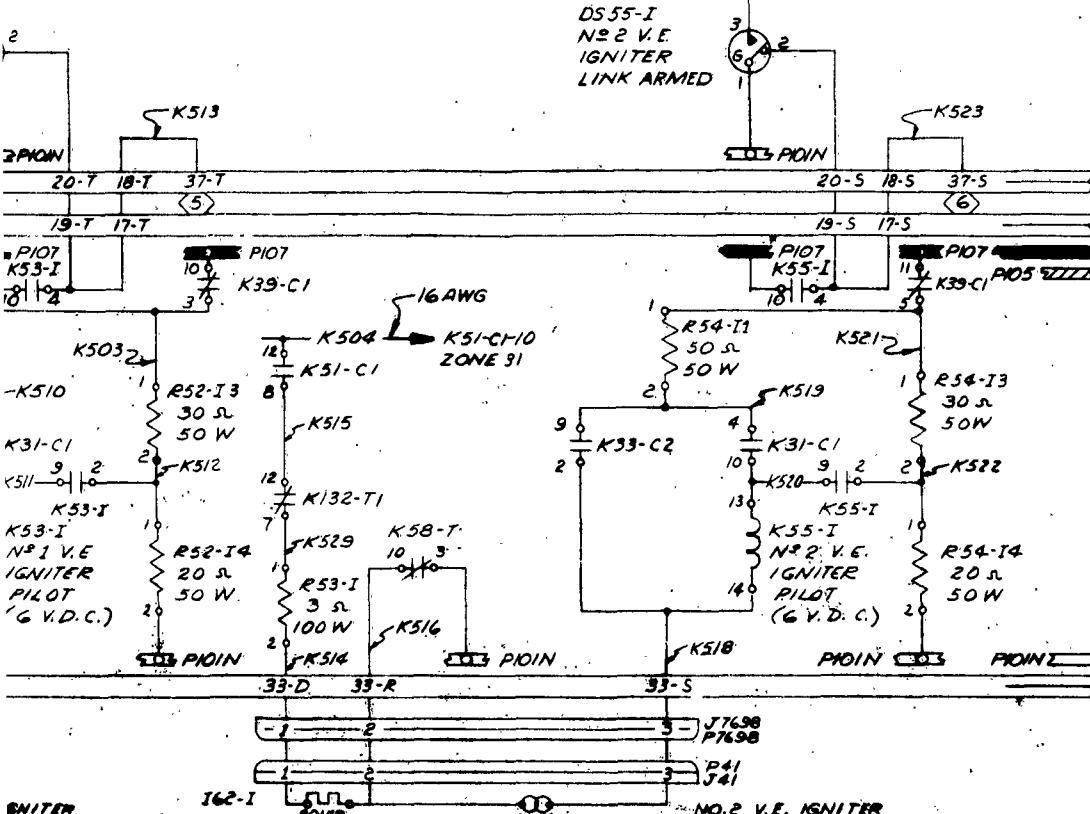


12

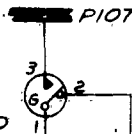
PI07

PI07

PI07



DS55-I
NO. 2 V.E.
IGNITER
LINK ARMED



PI0IN

PI11

PI13

PI07

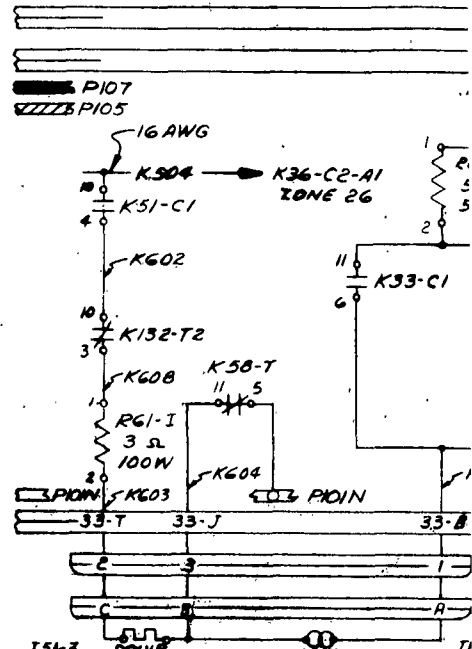
PI0IN

PI11

PI13

PI07

DS64-I
THRUST CHAMBE
IGNITER LINK
ARMED



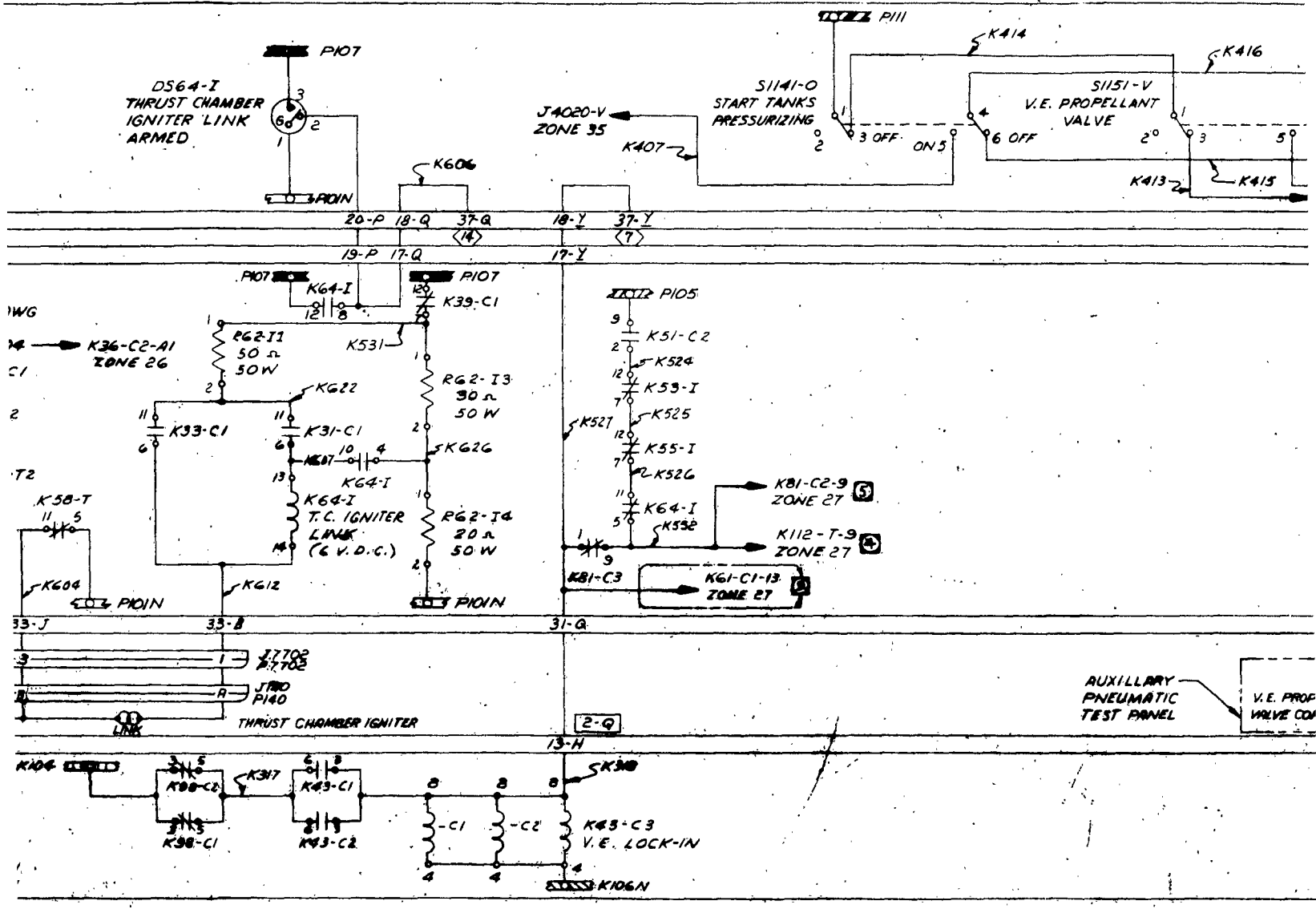
K104
K111

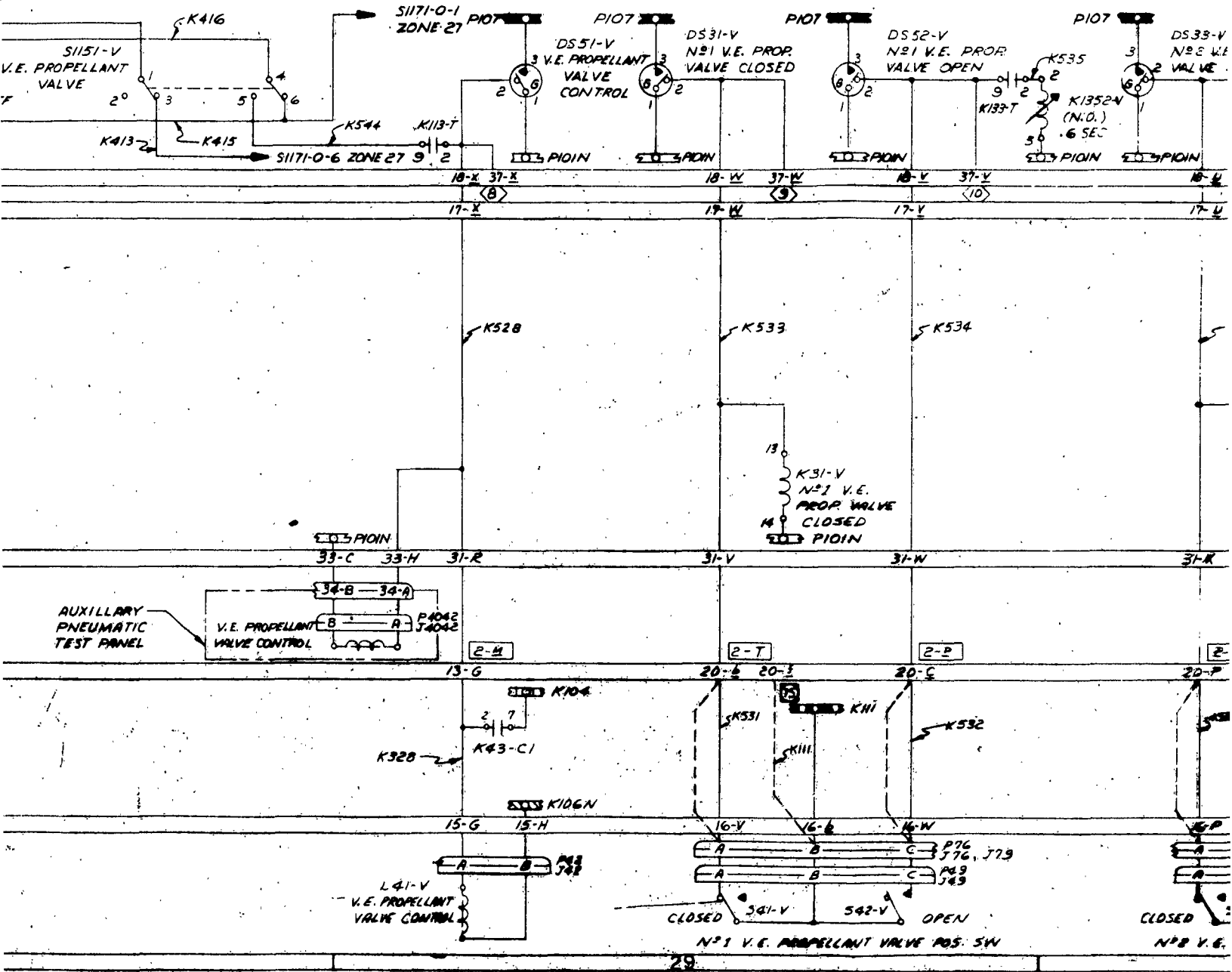
K106N
K106N

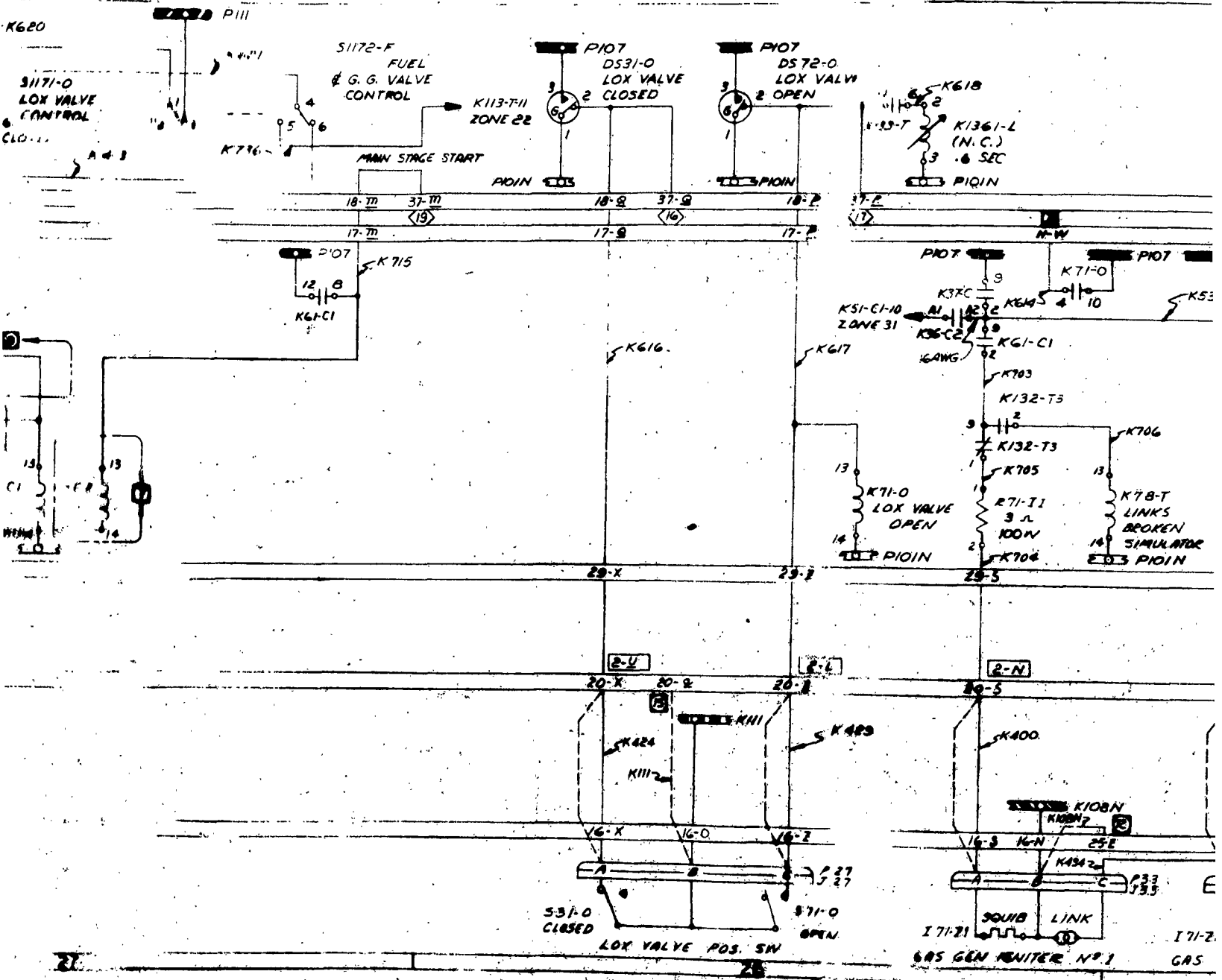
K104
K111

K106N
K106N

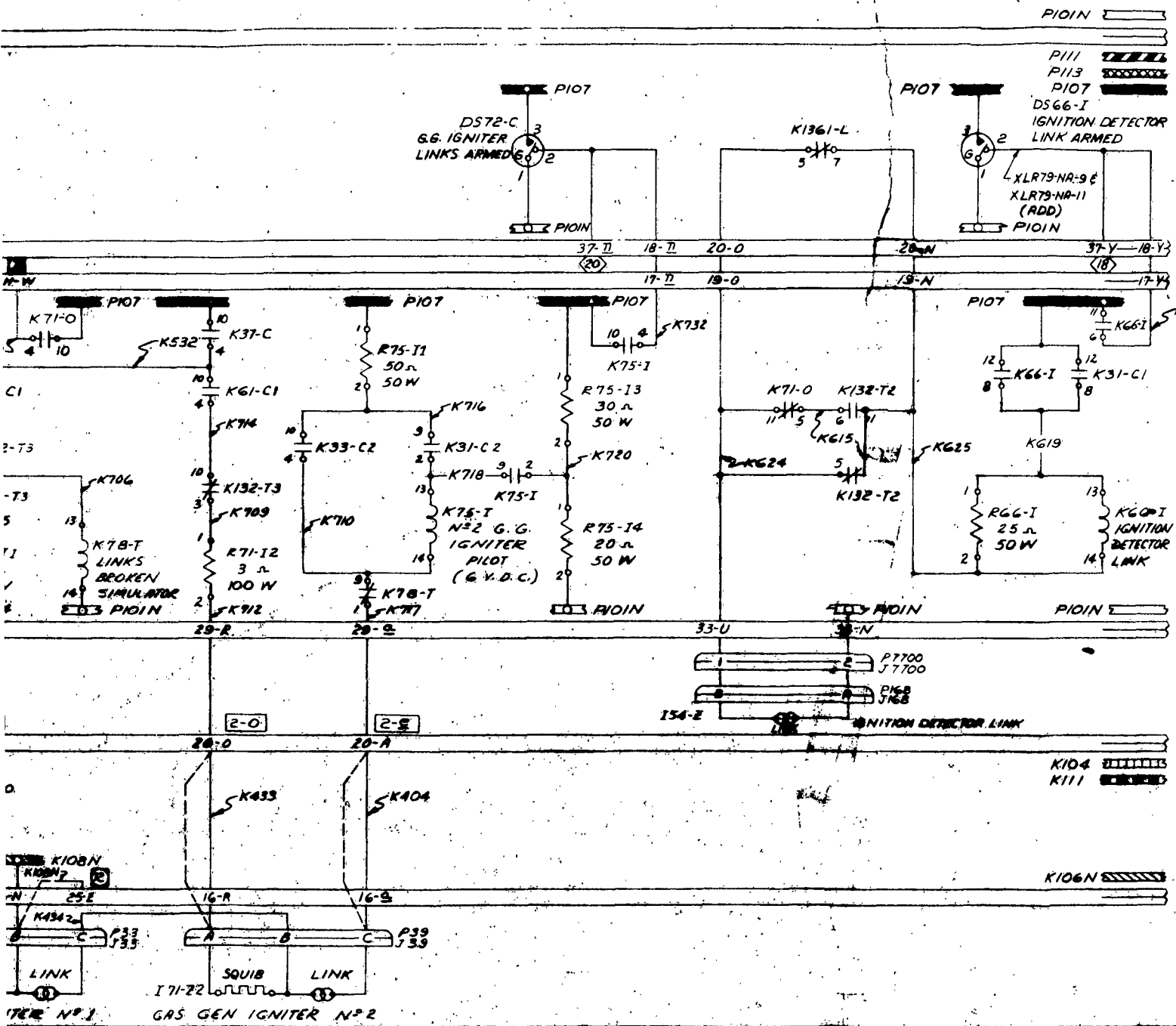
13

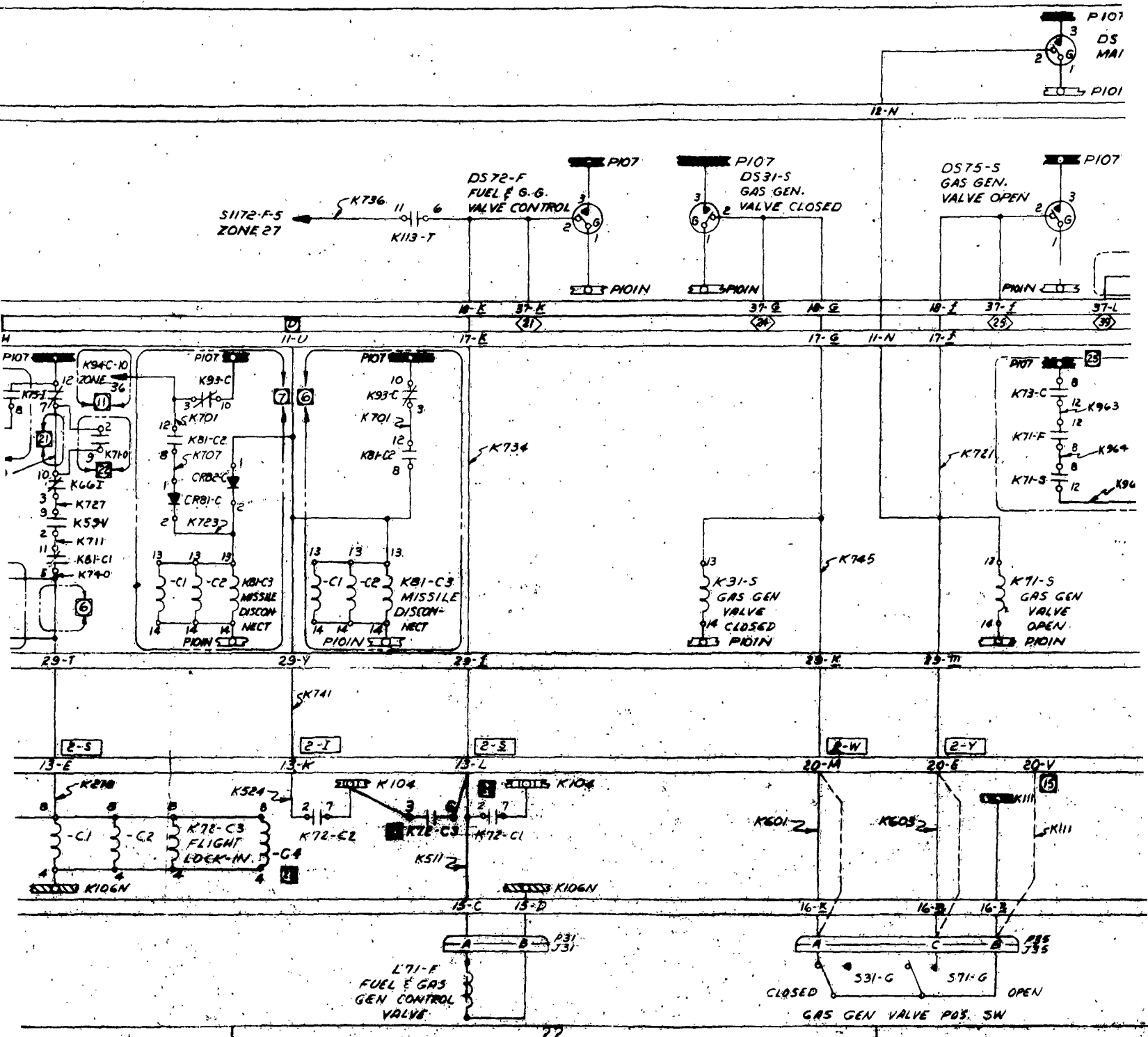


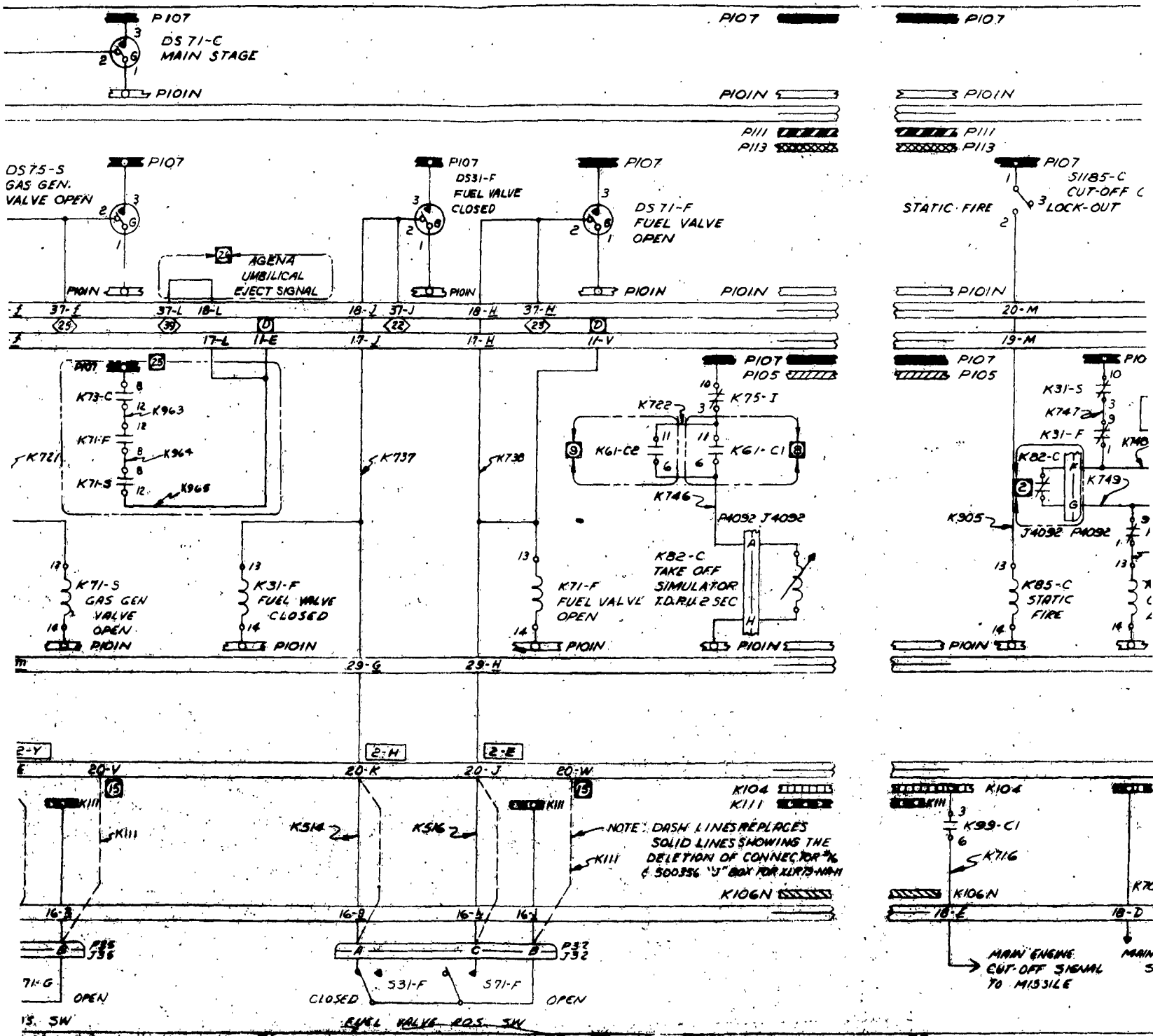


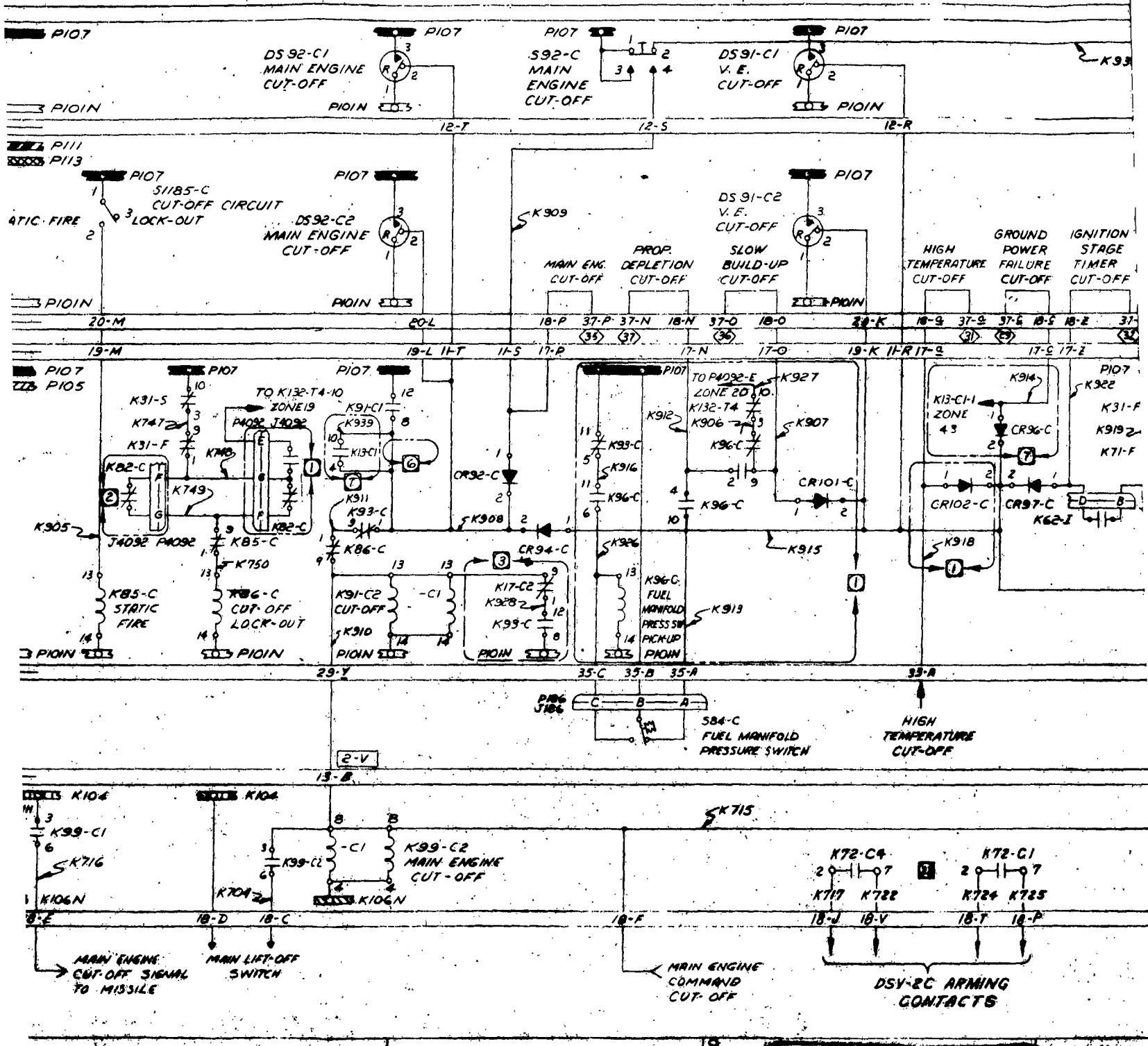


17

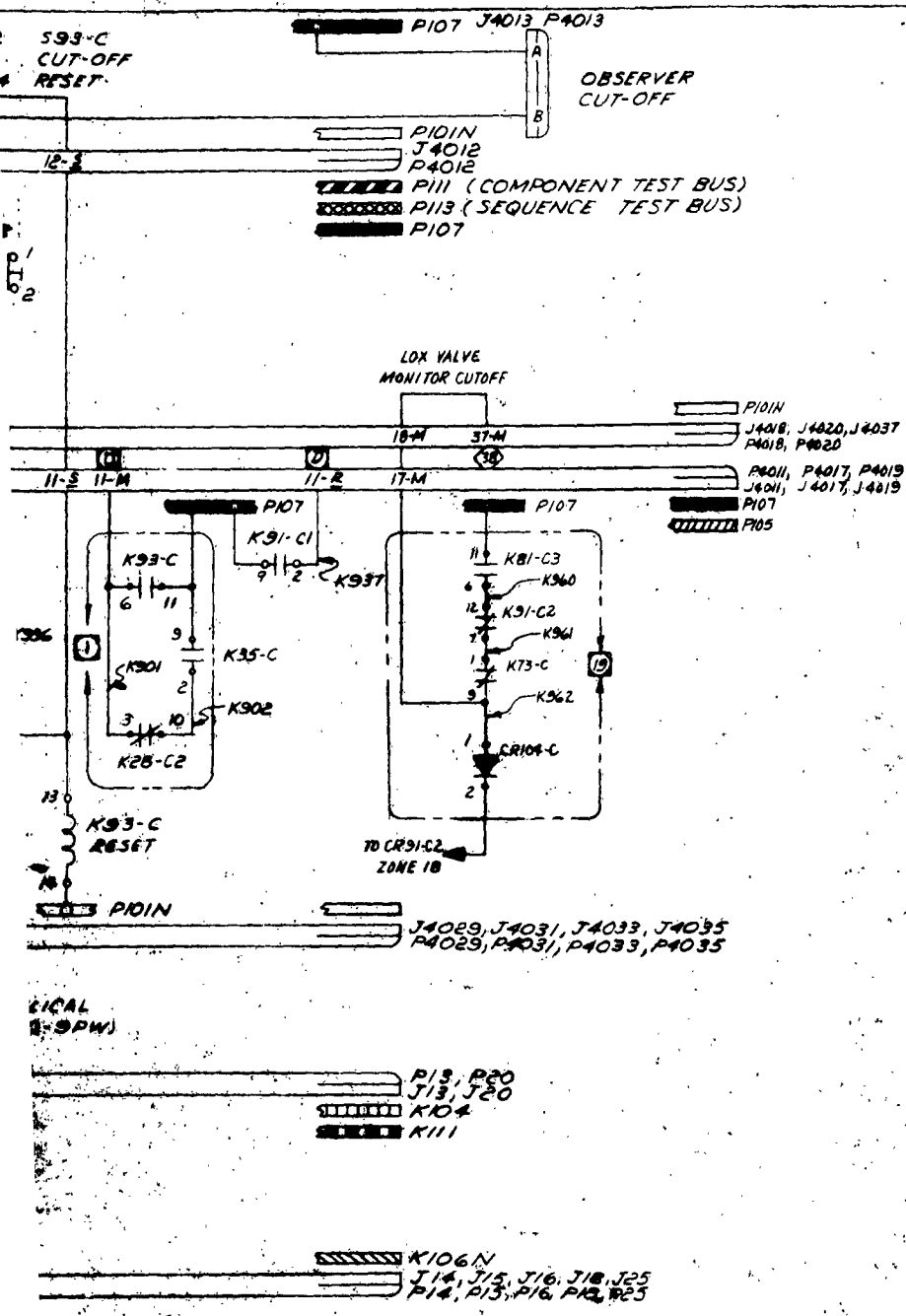








22



CONTROL PANEL

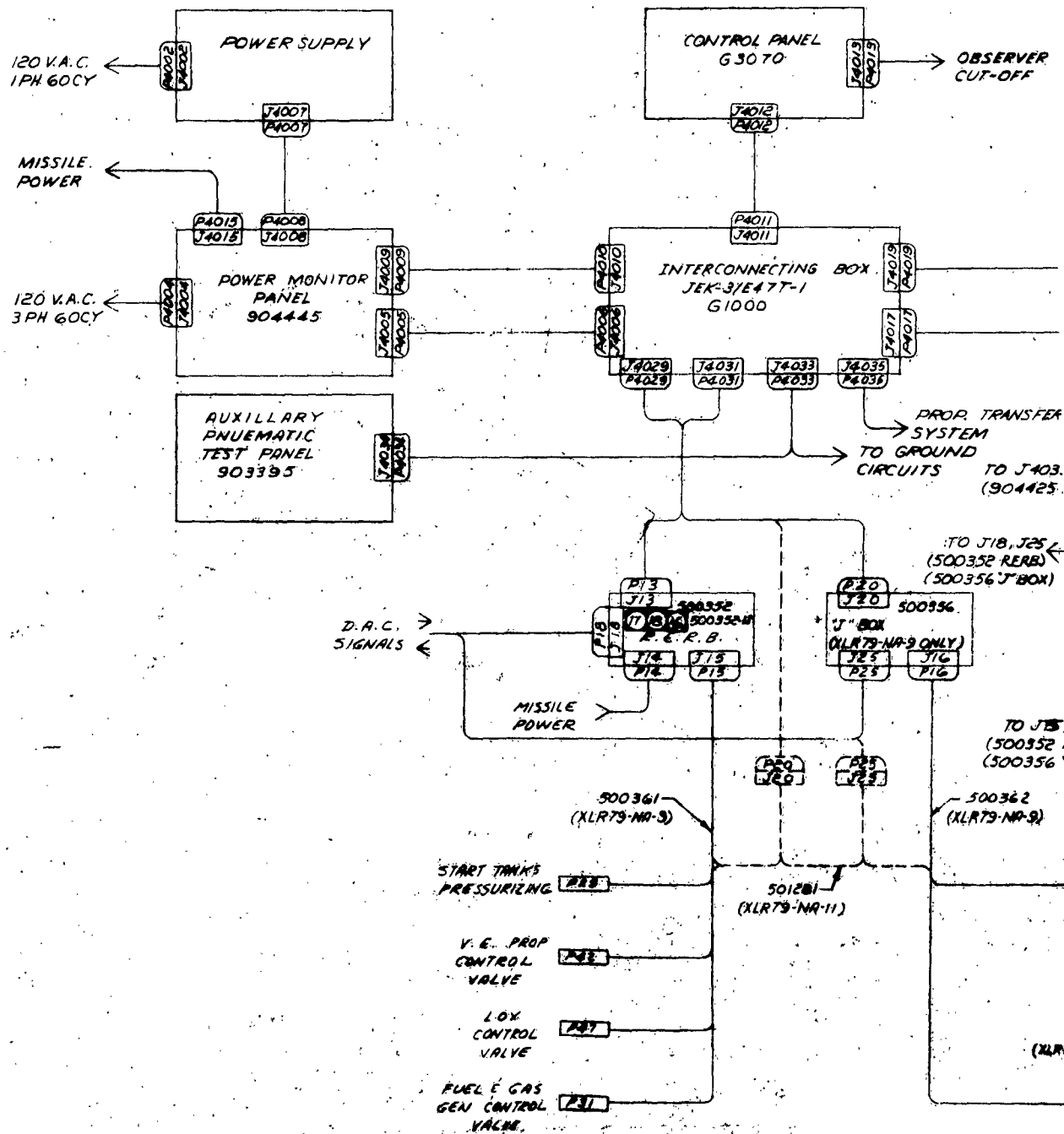
CONTROL-MONITOR

INTERCONNECTING BOX

GROUND & EXTERNAL EQUIPMENT

ENGINE RELAY BOX (REF)
(REF WIRING DIAGRAM 500360)
ENGINE JUNCTION BOX (REF)
(REF WIRING DIAGRAM 500360)

ENGINE ACCESSARY SECTION (REF)

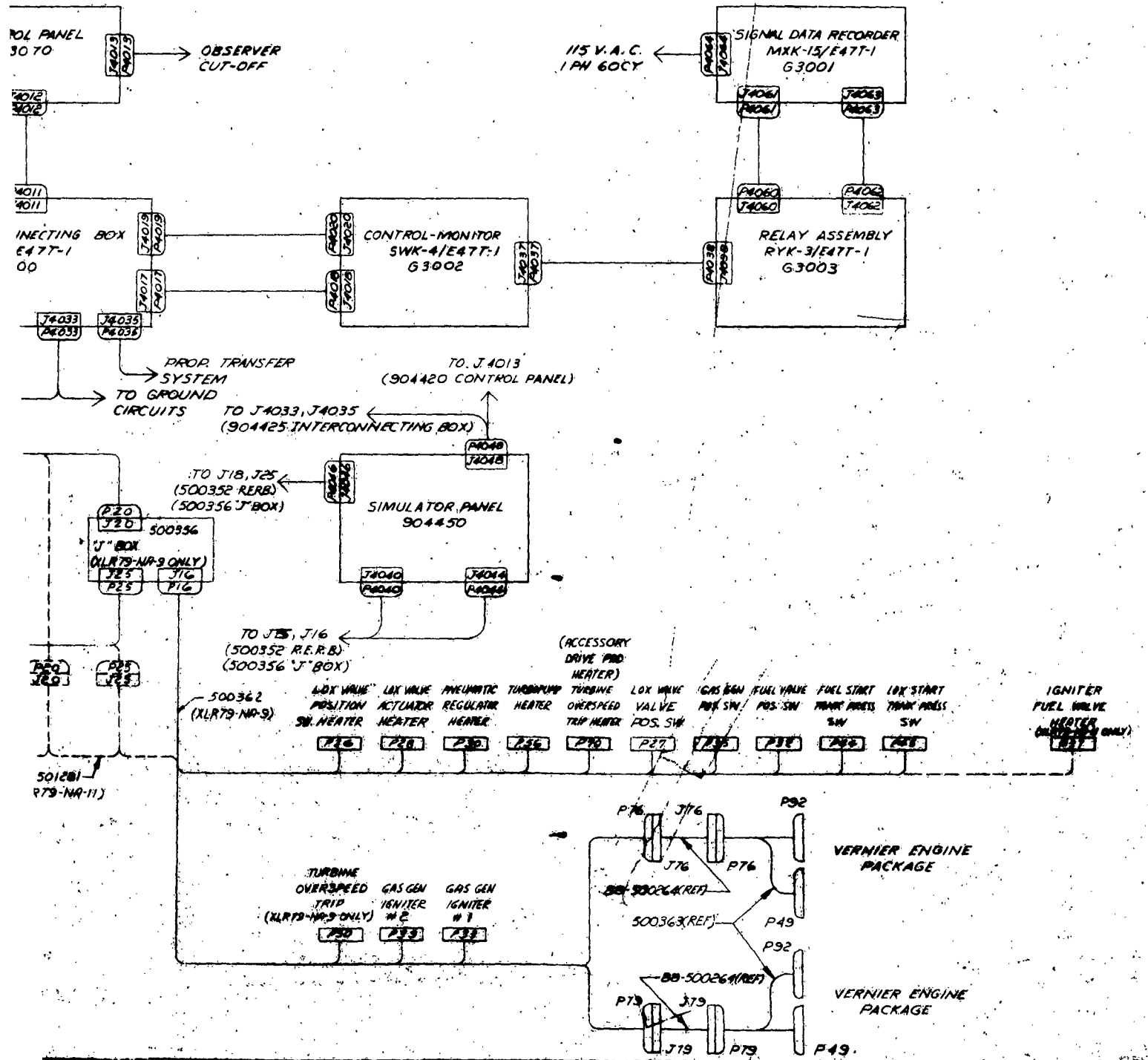


BOX

EQUIPMENT

(REF)
500360)
BOX (REF)
50036B)

SECTION (REF)



| |
|----------|
| TANKS |
| ENGIN |
| VERNI |
| VERNI |
| MAIN |
| VERNI |
| GAS B |
| IGNITI |
| IGNITI |
| VERNI |
| FUEL E |
| FUEL V |
| GAS GE |
| EFFECT |
| CL |
| TANKS |
| MAIN E |
| GAS GEN |
| MAIN LC |
| MAIN FL |
| VERNIER |
| VERNIER |
| CON |
| ARRAN |
| ITEM NO: |
| K401 |
| K402 |
| K403 |
| K42-C |
| K43-C1 |
| K43-C2 |
| K43-C3 |
| K72-C1 |
| K72-C2 |
| K72-C3 |
| K82-C1 |
| K82-C2 |
| K82-C3 |
| K82-C1 |
| K82-C2 |

| CONTACT ARRANGEMENT | | RELAYS | | COIL | | CONTACTS | | | | | | | | | | | |
|---------------------|--|--------------|--------------|------|----|----------|----|----|----|----|----|----|-----|-----|-----|-----|--|
| | | MS24143-1 | MIL-R-6106 | X1 | X2 | X3 | X4 | X5 | X6 | X7 | X8 | X9 | X10 | X11 | X12 | X13 | |
| | | MS24140-1 | MIL-R-6106 | X1 | X2 | | | | | | | | | | | | |
| | | MHYX-4003 | ALLIED | 13 | 9 | 9 | 10 | 10 | 11 | 11 | 12 | 12 | | | | | |
| | | 2112-D-H3 | AGASTAT | 14 | 2 | 1 | 4 | 3 | 6 | 5 | 8 | 7 | | | | | |
| | | HF-01 (N.C.) | 6-V CONTROLS | 2 | 3 | 5 | 6 | | | | | | | | | | |
| | | HF-01 (N.O.) | 6-V CONTROLS | 3 | 5 | 7 | | | | | | | | | | | |

| ITEM NO. | COIL LOC | DESC | PART NO | MFR | SPECIFICATION | NO | NC | NO | NC | NO | NC | NO | NC | NO | NC | NO | NC |
|----------|----------|-------|-----------|---------|---------------|----|----|----|----|----|----|----|----|----|----|----|----|
| K11-C | 45 | 1P 1T | MS24140-1 | | MIL-R-6106 | 45 | | | | | | | | | | | |
| K13-C1 | 44 | 4P 2T | MHYX-4003 | ALLIED | | | 43 | 19 | | | | | | | | | |
| K14-C | 44 | 3P 2T | MS24140-1 | | MIL-R-6106 | 44 | | | | | | | | | | | |
| K15-C | 43 | 3P 2T | MS24143-1 | | | 45 | | 45 | | 45 | | | | | | | |
| K16-C | 43 | 1P 1T | MS24140-1 | | | | | 45 | | 45 | | | | | | | |
| K17-C1 | 43 | 4P 2T | MHYX-4003 | ALLIED | MIL-R-6106 | 44 | | | | | | | | | | | |
| K17-C2 | 43 | | | | | 38 | 38 | 39 | 39 | 39 | 38 | 39 | 39 | | | | |
| K21-C | 41 | | | | | 19 | | 35 | 18 | | | | | | | | |
| K22-F | 38 | | | | | 35 | | 41 | 39 | | | | | | | | |
| K23-C | 34 | | | | | 37 | | | | | | | | | | | |
| K24-C | 37 | | | | | | 34 | 34 | | | | | | | | | |
| K25-C | 40 | | | | | 37 | | | | | | | | | | | |
| K26-C | 39 | | | | | | 40 | | | | | | | | | | |
| | | | | | | 40 | | | | | | | | | | | |
| K28-C1 | 34 | | | | | | 36 | 34 | 41 | 40 | 34 | | | | | | |
| K28-C2 | 34 | | | | | 34 | | 17 | | | | | | | | | |
| | | | | | | 34 | | | | | | | | | | | |
| K31-C1 | 41 | | | | | 33 | | 32 | 31 | 24 | | | | | | | |
| K31-C2 | 41 | | | | | 25 | | | | | | | | | | | |
| K31-F | 21 | | | | | | 20 | 18 | | | | | | | | | |
| K31-S | 22 | | | | | | | | | | | | | | | | |
| K31-V | 29 | | | | | 17 | | | 20 | 18 | | | | | | | |
| K37-C | 36 | | | | | | | | 23 | | | | | | | | |
| K32-O | 39 | | | | | 24 | | 25 | | | | | | | | | |
| K39-C1 | 40 | | | | | 39 | 39 | | | | | | | | | | |
| K39-C2 | 40 | | | | | | 41 | 36 | 31 | 33 | | | | | | | |
| K33-V | 28 | | | | | 32 | | 25 | | 34 | | | | | | | |
| K39-C1 | 38 | | | | | | | | 23 | | | | | | | | |
| K39-C2 | 38 | | | | | 36 | 36 | 33 | 32 | 31 | | | | | | | |
| K35-C | 37 | 4P 2T | MHYX-4003 | ALLIED | | 41 | | | | | | | | | | | |
| K36-C1 | 36 | 1P 1T | MS24140-1 | | MIL-R-6106 | 17 | | 36 | 36 | 34 | | | | | | | |
| K36-C2 | 36 | 1P 1T | MS24140-1 | | MIL-R-6106 | 33 | | | | | | | | | | | |
| K41-C | 36 | 4P 2T | MHYX-4003 | ALLIED | | 26 | | | | | | | | | | | |
| K44-C | 35 | 2P 2T | 2112-D-H3 | AGASTAT | | 36 | | 35 | | 39 | | | | | | | |
| | | | | | | 36 | | | | | | | | | | | |
| K50-C | 35 | 4P 2T | MHYX-4003 | ALLIED | | | | | | | | | | | | | |
| K51-C1 | 34 | | MHYX-4003 | | | 18 | | | | | | | | | | | |
| K51-C2 | 34 | | MHYX-4003 | | | 34 | 31 | 33 | 32 | | | | | | | | |
| | | | | | | 30 | 33 | 23 | 17 | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| K53-Z | 33 | | MHYX-4020 | | | 33 | 33 | 41 | | 30 | | | | | | | |
| K55-Z | 32 | | MHYX-4020 | | | 32 | 32 | 41 | | 30 | | | | | | | |
| K59-T | 33 | | MHYX-4003 | | | | | | | | | | | | | | |
| K59-V | 23 | | | | | 23 | 23 | 32 | 31 | | | | | | | | |
| | | | | | | | | | 39 | | | | | | | | |
| K61-C1 | 27 | | | | | 26 | 25 | 20 | 27 | | | | | | | | |
| K61-C2 | 27 | 4P 2T | MHYX-4003 | ALLIED | | 26 | 25 | 20 | 27 | | | | | | | | |

| CONTACT ARRANGEMENT | | |
|---------------------|----------|---------|
| ITEM NO. | COIL LOC | DESC |
| K62-I | 34 | 2P 2T |
| K64-I | 31 | 4P 2T |
| K66-I | 24 | |
| K71-F | 21 | |
| K71-O | 26 | |
| K71-S | 21 | |
| K73-C | 28 | |
| K75-I | 25 | |
| K78-T | 25 | |
| K81-C1 | 22 | |
| K81-C2 | 22 | 4P 2T M |
| K81-C3 | 22 | 4P 2T M |
| K82-C | 20 | 2P 2T M |
| K83-C | 20 | 4P 2T M |
| K86-C | 20 | |
| K91-C1 | 19 | |
| K91-C2 | 19 | |
| K93-C | 17 | |
| K94-C | 35 | |
| K95-C | 36 | 4P 2T M |
| K96-C | 19 | 4P 2T M |
| K111-T | 43 | 1P 1T M |
| K112-T | 43 | 4P 2T M |
| K113-T | 41 | 4P 2T M |
| K131-T | 42 | 1P 1T M |
| K132-T1 | 42 | 4P 2T M |
| K132-T2 | 42 | |
| K132-T3 | 42 | |
| K132-T4 | 42 | |
| K133-T | 41 | |
| K141-T1 | 42 | |
| K141-T2 | 42 | 4P 2T M |
| K152-V | 23 | 1P 1T M |
| K154-V | 28 | 1P 1T M |
| K161-L | 26 | 1P 1T M |

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| RELAYS | | | | COIL | CONTACTS | | | | | | | | | | | | | | | |
|--------|-------|--------------|--------------|---------------|----------|----|---|----|----|----|----|----|----|----|----|----|---|---|----|----|
| ACT | MENT | PART NO | MFR | SPECIFICATION | N | O | N | C | N | O | N | C | N | O | N | C | N | O | N | C |
| | | MS24140-1 | MIL-R-6106 | | | | | | | | | | | | | | | | | |
| | | MHYX-4003 | ALLIED | | 13 | 9 | 9 | 10 | 10 | 11 | 11 | 12 | 12 | | | | | | | |
| | | MHYX-4020 | ALLIED | | 14 | 2 | 1 | 4 | 3 | 6 | 5 | 0 | 7 | | | | | | | |
| | | 2112-D-H3 | AGASTAT | | A | H | B | C | G | F | | | | | | | | | | |
| | | HF-01 (N.C.) | G-V CONTROLS | | 2 | 3 | | | | | | | | | | | | | | |
| | | HF-01 (N.O.) | G-V CONTROLS | | 3 | 3 | | | | | | | | | | | | | | |
| LOC | DESC | PART NO | MFR | SPECIFICATION | N | O | N | C | N | O | N | C | N | O | N | C | N | O | N | C |
| 4 | 2P 2T | 2112-D-H3 | AGASTAT | | 18 | | | 33 | | | | | | | | | | | | |
| 1 | 4P 2T | MHYX-4020 | ALLIED | | 41 | | | 31 | | | | 30 | 31 | | | | | | | |
| 4 | | MHYX-4003 | | | 41 | | | | 23 | 24 | | 24 | | | | | | | | |
| 1 | | | | | | | | | 18 | | | | | | | | | | 21 | |
| 6 | | | | | | | | | 23 | | 26 | | | | | | | | 25 | |
| 1 | | MHYX-4003 | | | | | | | 17 | | | 18 | | | | | | | 21 | |
| 8 | | MHYX-4003 | | | | | | | 17 | | | | | | | | | | 21 | |
| 5 | | MHYX-4020 | | | | | | | 25 | | | 25 | 20 | 41 | | | | | 23 | 23 |
| 3 | | MHYX-4003 | | | | | | | 25 | | | | | | | | | | | |
| | | | | | | | | | 44 | | 36 | | | 23 | | | | | 38 | |
| 2 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 27 | | 44 | | | 34 | 22 | | | | | |
| 2 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 17 | | 30 | | | 43 | | | | | | |
| 0 | 2P 2T | 2112-D-H3 | AGASTAT | | | | | | 36 | | | | 20 | | | | | | | |
| 0 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 20 | | | | | | | | | | | |
| 2 | | | | | | | | | 20 | | | 18 | | | | | | | | |
| 9 | | | | | | | | | 17 | 44 | | 36 | | 41 | 19 | 34 | | | | |
| 9 | | | | | | | | | 42 | 23 | 17 | | | 35 | | | | | | |
| 7 | | | | | | | | | 20 | | 22 | 17 | 19 | 19 | | | | | | |
| 5 | | | | | | | | | 17 | | | 36 | | 36 | | | | | | |
| 5 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 36 | | 36 | | | 36 | | | | | | |
| 1 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 19 | 19 | 19 | | | 19 | | | | | | |
| 1 | 1P 1T | MS24140-1 | MIL-R-6106 | | 42 | | | | | | | | | | | | | | | |
| 1 | 4P 2T | MHYX-4003 | ALLIED | | | | | | 27 | | | | | | | | | | | |
| | 4P 2T | MHYX-4003 | ALLIED | | | | | | 29 | | 27 | | | 22 | | | | | | |
| | 1P 1T | MS24140-1 | MIL-R-6106 | | 42 | | | | | | | | | | | | | | | |
| | 4P 2T | MHYX-4003 | ALLIED | | 41 | 44 | | | 35 | 33 | 33 | | | 32 | | | | | | |
| | | | | | 23 | | | | 31 | 24 | 24 | 34 | | | | | | | | |
| | | | | | 26 | 26 | | | 25 | 43 | 44 | | | | | | | | | |
| | | | | | 35 | | | | 19 | | | | | | | | | | | |
| | | | | | 29 | | | | 28 | | 26 | | | 41 | | | | | | |
| | 4P 2T | MHYX-4003 | ALLIED | | | | | | | | | | | 40 | | 36 | | | | |
| | 1P 1T | HF-01 | G-V CONTROLS | | 23 | | | | | | | | | | | | | | | |
| | 1P 1T | HF-01 | G-V CONTROLS | | 23 | | | | | | | | | | | | | | | |
| | 1P 1T | HF-01 | G-V CONTROLS | | 24 | | | | | | | | | | | | | | | |

| (RERB) | RESERVED WIRE NUMBERS | | | | | |
|--------|-----------------------|------|------|------|------|------|
| X4 | P101 | K201 | K301 | K401 | K501 | K601 |
| X6 | P102 | K202 | K302 | K402 | K502 | K602 |
| X7 | P103 | K203 | K303 | K403 | K503 | K603 |
| X11 | P104 | K204 | K304 | K404 | K504 | K604 |
| X12 | P105 | K205 | K305 | K405 | K505 | |
| X2N | P106 | K206 | K306 | K406 | K506 | K606 |
| K104 | P107 | K207 | K307 | K407 | K507 | K607 |
| K106N | P108 | K208 | K308 | K408 | K508 | K608 |
| K108N | P109 | | K309 | K409 | K509 | K609 |
| K111 | K110 | K210 | K310 | K410 | K510 | |
| K108 | P111 | K211 | K311 | K411 | K511 | K611 |
| K218 | P112 | K212 | K312 | K412 | K512 | K612 |
| K219 | P113 | K213 | K313 | K413 | K513 | K613 |
| K301 | P114 | | K314 | K414 | K514 | K614 |
| K306 | P115 | | K315 | K415 | K515 | K615 |
| K307 | K116 | | K316 | K416 | K516 | K616 |
| K317 | | | K317 | K417 | K517 | K617 |
| K318 | | | K318 | K418 | K518 | K618 |
| K308 | | K219 | K319 | K419 | K519 | K619 |
| V303 | | K220 | K320 | K420 | K520 | K620 |
| K340 | | K221 | K321 | K421 | K521 | K621 |
| K343 | | K222 | K322 | K422 | K522 | K622 |
| K356 | | K223 | K323 | K423 | K523 | |
| K358 | | K224 | K324 | K424 | K524 | K624 |
| K360 | | K225 | K325 | K425 | K525 | K625 |
| K391 | | K226 | K326 | K426 | K526 | K626 |
| K400 | | K227 | K327 | K427 | K527 | K627 |
| K404 | | K228 | K328 | | K528 | |
| K414 | | K229 | K329 | | K529 | |
| K424 | | | K330 | K430 | K530 | |
| K429 | | K231 | K331 | | K531 | |
| K433 | | | K332 | | K532 | |
| K434 | | | K333 | | K533 | |
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| K704 | | | | | K547 | |
| K711 | | | | | K548 | |
| K715 | | | | | K549 | |
| K716 | | | | | | |
| K721 | | | | | | |
| | | | | | K552 | |

31

RESERVED WIRE NUMBERS

| | | | | | | | |
|------|------|------|------|------|-------|------|------|
| K301 | K401 | K501 | K601 | K701 | K101N | K901 | X1A |
| K302 | K402 | K502 | K602 | K702 | P101N | K902 | X1B |
| K303 | K403 | K503 | K603 | K703 | | K903 | X1C |
| K304 | K404 | K504 | K604 | K704 | | K904 | X1N |
| K305 | K405 | K505 | | K705 | | K905 | X2A |
| K306 | K406 | K506 | K606 | K706 | | K906 | X2B |
| K307 | K407 | K507 | K607 | K707 | | K907 | X2C |
| K308 | K408 | K508 | K608 | | | K908 | X3A |
| K309 | K409 | K509 | K609 | K709 | | K909 | X3B |
| K310 | K410 | K510 | | K710 | | K910 | X3C |
| K311 | K411 | K511 | K611 | K711 | | K911 | X4A |
| K312 | K412 | K512 | K612 | K712 | | K912 | X4B |
| K313 | K413 | K513 | K613 | | | K913 | X4C |
| K314 | K414 | K514 | K614 | K714 | | K914 | X5A |
| K315 | K415 | K515 | K615 | K715 | | K915 | |
| K316 | K416 | K516 | K616 | K716 | | K916 | X5C |
| K317 | K417 | K517 | K617 | K717 | | K917 | X6A |
| K318 | K418 | K518 | K618 | K718 | | K918 | X6B |
| K319 | K419 | K519 | K619 | K719 | | K919 | |
| K320 | K420 | K520 | K620 | K720 | | K920 | |
| K321 | K421 | K521 | K621 | K721 | | K921 | |
| K322 | K422 | K522 | K622 | K722 | | K922 | P10 |
| K323 | K423 | K523 | | K723 | | K923 | P11N |
| K324 | K424 | K524 | K624 | K724 | | K924 | X12 |
| K325 | K425 | K525 | K625 | K725 | | K925 | X13N |
| K326 | K426 | K526 | K626 | | | K926 | X14N |
| K327 | K427 | K527 | K627 | K727 | | K927 | P15 |
| K328 | | K528 | | | | K928 | X16 |
| K329 | | K529 | | | | K929 | X17N |
| K330 | K430 | K530 | | | | K930 | K16 |
| K331 | | K531 | | | | K931 | K19 |
| K332 | | K532 | | K732 | | K932 | K20 |
| K333 | | K533 | | | | K933 | K21 |
| K334 | | K534 | | K734 | | K934 | X22N |
| K335 | | K535 | | | | K935 | X23N |
| | | K536 | | K736 | | K936 | P24 |
| | | K537 | | K737 | | K937 | |
| | | K538 | | K738 | | K938 | |
| | | K539 | | K739 | | K939 | |
| | | K540 | | K740 | | | |
| | | K541 | | K741 | | K941 | |
| | | K542 | | | | K942 | |
| | | K543 | | | | | |
| | | K544 | | | | | |
| | | | | K745 | | | |
| | | | | K746 | | | |
| | | K547 | | K747 | | | |
| | | K548 | | K748 | | | |
| | | K549 | | K749 | | K954 | |
| | | | | K750 | | | |
| | | K552 | | | | | |
| | | | | | | K960 | |
| | | | | | | K961 | |
| | | | | | | K962 | |
| | | | | | | K963 | |
| | | | | | | K964 | |
| | | | | | | K965 | |

SWITCHES

| ITEM NO. | LOC. | DESC. | PART NO. | MFGR. | SPEC. |
|----------|------|-----------|-------------|--------------|------------|
| S11-C | 46 | 1P 2T | AN3021-3 | | MIL-S-6745 |
| S13-C | 44 | | AN3021-3 | | |
| S20-C | 42 | | AN3021-3 | | |
| S21-C | 41 | 1P 2T | AN3021-3 | | |
| S39-C | 38 | 1P 2T | AN3022-3 | | MIL-S-6745 |
| S91-C1 | 18 | 2 CIRCUIT | W103L5-ALR | HETHERINGTON | |
| S91-C2 | 18 | 1 CIRCUIT | MS25089-3FB | | MIL-S-6743 |
| S92-C | 19 | 2 CIRCUIT | MS25089-3FR | | MIL-S-6743 |
| S93-C | 17 | 1 CIRCUIT | MS25089-3FB | | MIL-S-6743 |
| S111-T | 43 | 1P 2T | AN3021-3 | | MIL-S-6745 |
| S131-C | 44 | | AN3021-3 | | |
| S131-T | 42 | | AN3021-3 | | |
| S1121-F | 38 | | AN3021-3 | | |
| S1122-C | 37 | | AN3021-3 | | |
| S1123-F | 38 | | AN3021-3 | | |
| S1124-C | 37 | | AN3021-3 | | |
| S1125-F1 | 40 | | AN3021-3 | | |
| S1125-F2 | 40 | | AN3021-3 | | |
| S1126-D1 | 39 | | AN3021-3 | | |
| S1126-D2 | 39 | | AN3021-3 | | |
| S1127-C | 34 | | AN3021-3 | | |
| S1128-O | 39 | 1P 2T | AN3021-3 | | |
| S1135-C | 37 | 1P 1T | AN3021-11 | | |
| S1141-O | 30 | 2P 2T | AN3027-3 | | |
| S1151-V | 30 | | | | |
| S1177-O | 27 | | | | |
| S1178-F | 27 | 2P 2T | AN3027-3 | | |
| S1185-C | 20 | 1P 2T | AN3021-3 | | MIL-S-6745 |
| S1193-C | 17 | 1 CIRCUIT | MS25089-3FB | | MIL-S-6743 |
| S4101 | 49 | 1P 2T | MS15038-23 | | MIL-S-6745 |

| |
|---------|
| ITEM M |
| DS12-C |
| DS13-C |
| DS14-C |
| DS15-C |
| DS20-C |
| DS21-C |
| DS21-A |
| DS22-C |
| DS22-L |
| DS24-C |
| DS25-C |
| DS26-C |
| DS28-C |
| DS31-A |
| DS31-C |
| DS31-S |
| DS31-Y |
| DS32-O |
| DS33-C |
| DS33-V |
| DS34-C |
| DS42-F |
| DS51-V |
| DS52-V |
| DS53-T |
| DS54-V |
| DS55-T |
| DS59-V |
| DS64-T |
| DS66-T |
| DS71-C |
| DS71-F |
| DS71-O |
| DS72-C |
| DS72-F |
| DS72-O |
| DS75-S |
| DS91-C1 |
| DS91-C2 |
| DS92-C1 |
| DS92-C2 |
| DS111-T |
| DS131-T |
| DS4101 |
| DS4102 |
| DS4103 |

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INDICATING LIGHTS

| ITEM NO. | LOC. | DESC. | PART NO. | MFR | SPEC |
|----------|------|-------|----------------|-------|------|
| DS12-C | 45 | WHITE | 19-902426 | KORRY | |
| DS13-C | 44 | | 19-902401 | | |
| DS14-C | 45 | | 19-902402 | | |
| DS15-C | 43 | WHITE | 19-902403 | | |
| DS20-C | 42 | GREEN | 19-902404 | | |
| DS21-C | 41 | | 19-902405 | | |
| DS21-F | 38 | | 19-902406 | | |
| DS22-C | 38 | | 19-902408 | | |
| DS22-O | 37 | | 19-902407 | | |
| DS24-C | 37 | | 19-902409 | | |
| DS25-C | 40 | | 19-902410 | | |
| DS26-C | 40 | | 19-902411 | | |
| DS28-C | 34 | | 19-902416 | | |
| DS31-F | 21 | | 19-902463 | | |
| DS31-O | 26 | | 19-902464 | | |
| DS31-S | 22 | | 19-902465 | | |
| DS31-Y | 29 | | 19-902466 | | |
| DS32-O | 39 | | 19-902412 | | |
| DS33-C | 40 | | 19-902413 | | |
| DS33-V | 28 | | 19-902414 | | |
| DS34-C | 34 | | 19-902415 | | |
| DS42-F | 35 | | 19-902435 | | |
| DS51-V | 29 | | 19-902418 | | |
| DS52-V | 29 | | 19-902419 | | |
| DS53-J | 33 | | 19-902420 | | |
| DS54-V | 28 | | 19-902421 | | |
| DS55-J | 32 | | 19-902422 | | |
| DS59-V | 23 | | 19-902423 | | |
| DS64-J | 31 | | 19-902443 | | |
| DS66-J | 24 | | 19-902425 | | |
| DS71-C | 21 | | 19-902444 | | |
| DS71-F | 20 | | 19-902427 | | |
| DS71-O | 28 | | 19-902428 | | |
| DS72-C | 25 | | 19-902429 | | |
| DS72-F | 22 | | 19-902430 | | |
| DS72-O | 26 | | 19-902431 | | |
| DS75-S | 21 | GREEN | 19-902432 | | |
| DSS1-C1 | 19 | RED | 19-902434 | | |
| DSS1-C2 | 19 | RED | 19-902434 | | |
| DSS2-C1 | 19 | RED | 19-902436 | | |
| DSS2-C2 | 19 | RED | 19-902445 | | |
| DS111-F | 43 | GREEN | 19-902437 | | |
| DS131-F | 42 | GREEN | 19-902438 | KORRY | |
| DS4101 | 49 | WHITE | RD332-000-0087 | | |
| DS4102 | 48 | GREEN | RD332-000-0087 | | |
| DS4103 | 48 | RED | RD332-000-0087 | | |

MISCELLANEOUS

| ITEM NO. | LOC. | DESC. | PART NO. | MFR | SPEC |
|----------|------|------------|------------|----------------|-----------|
| CB11-C1 | 46 | IP IT | D7271-1-5 | SPENCER-THERMO | |
| CB11-C2 | 46 | | D7271-1-20 | | |
| CB13-C1 | 46 | | D7271-1-25 | | |
| CB13-C2 | 46 | | D7271-1-25 | | |
| CB13-C3 | 46 | IP IT | D7271-1-25 | SPENCER-THERMO | |
| CR50-C | 35 | RECTIFIER | 3DT1 | INTERNATIONAL | |
| CR70-C | 23 | | | | |
| CR81-C | 22 | | | | |
| CR82-C | 22 | | | | |
| CR91-C | 18 | | | | |
| CR92-C | 19 | | | | |
| CR93-C | 18 | | | | |
| CR94-C | 19 | | | | |
| CR95-C | 18 | | | | |
| CR96-C | 20 | | | | |
| CR97-C | 18 | | | | |
| CR98-C | 17 | | | | |
| CR99-C | 18 | | | | |
| CR100-C | 43 | | | | |
| CR101-C | 19 | | | | |
| CR102-C | 19 | RECTIFIER | 3DT1 | INTERNATIONAL | |
| CR103-C | | RECTIFIER | 3NT1 | INTERNATIONAL | |
| CR104-C | | RECTIFIER | 3NT1 | INTERNATIONAL | |
| M11-C1 | 46 | 0-50 VOLTS | WELCH | | MIL-M-101 |
| M11-C2 | 46 | 0-50 AMPS | WELCH | | |
| M12-C1 | 46 | 0-30 AMPS | WELCH | | |
| M12-C2 | 46 | 0-30 AMPS | WELCH | | |
| M12-C3 | 46 | 0-50 AMPS | WELCH | | MIL-M-101 |

| | |
|------------|---|
| ZONE | F |
| 3, 17, 28 | |
| 3, 4, 41 | G |
| 3, 10, 23 | H |
| 17, 22, 38 | J |
| 21 | K |

- 33. CIRCUITRY TO BE ADDED FOR MB3-161 (G1000 MD 6)
- 32. CIRCUITRY TO BE ADDED FOR MB3-160 (G1000 MD 15)
- 31. REMOVED PER MB3-149
- 30. ADDED PER MB3-149
- 29. CIRCUITRY TO BE ADDED FOR MB3-144 (G1000 MD 14)
- 28. CIRCUITRY TO BE REMOVED FOR MB3-144 (G1000 MD 14)
- 27. CIRCUITRY TO BE INSTALLED FOR HYBRID ENGINE FIRING (G1000 MD 13 & G3000 MD 17)
- 26. CIRCUITRY TO BE INSTALLED FOR LOX VALVE MONITOR CUTOFF (G1000 MD 12 & G3002 MD 5)
- 25. MY7002 RELAYS REPLACED ON ALL ENGINE RELAY BOXES BY NAB-27103 TYPE I RELAYS
- 24. CONNECTORS CODED (6) REPLACED ON ALL ENGINE RELAY BOXES BY CONNECTORS CODED (7)
- 23. PINS 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100 ARE BUSSED TOGETHER IN J20 INTERNALLY
- 22. PINS 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100 ARE BUSSED TOGETHER IN J20 INTERNALLY
- 21. PINS 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100 ARE BUSSED TOGETHER IN J25 INTERNALLY
- 20. PINS D, E, F, G, H ARE BUSSED TOGETHER IN J25 INTERNALLY
- 19. CIRCUITRY TO BE ADDED FOR MB3-19. (G1000 MD 11)
- 18. CIRCUITRY TO BE REMOVED FOR MB3-19. (G1000 MD 11)
- 17. CIRCUITRY TO BE ADDED FOR MB3-24 (G1000 MD 11)
- 16. CIRCUITRY TO BE ADDED FOR MB3-24 (G1000 MD 11)
- 15. CIRCUITRY TO BE ADDED FOR START TANKS PRESSURIZING CUT-OFF, GROUND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE (G1000 MD 6 & G3002 MD 5)
- 14. CIRCUITRY TO BE REMOVED FOR START TANKS PRESSURIZING CUT-OFF, GROUND POWER FAILURE CUT-OFF & SEPARATION OF MISSILE (G1000 MD 6 & G3002 MD 5)
- 13. CIRCUITRY TO BE ADDED FOR LAUNCH LOCKOUT. (G1000 MD 6 (UP))
- 12. CIRCUITRY TO BE REMOVED FOR LAUNCH LOCKOUT (G1000 MD 6 (UP))
- 11. CIRCUITRY TO BE ADDED FOR PRESET OF XLR 79-NA-7 (G1000 MD 4 (UP))
- 10. CIRCUITRY TO BE REMOVED FOR STATIC FIRING. (G1000 MD 5)
- 9. CIRCUITRY TO BE INSTALLED FOR STATIC FIRING. (G1000 MD 5, G3002 MD 5)
- 8. UNDERLINED CONNECTOR PIN LETTERS DENOTE LOWER CASE.
- 7. REF DWG 900040 SCHEMATIC.
- 6. REF DWG 900075 BLOCK DIAGRAM
- 5. SYMBOL \square INDICATES RECORDER CONNECTIONS
- 4. REF DWG SCHEMATIC NO. 902500 FOR ENGINE SIMULATOR
- 3. SYMBOL \square DENOTES DOUGLAS AIRCRAFT COMPANY CONNECTIONS.
- 2. WIRES ARE #20 AWG FOR ALL PANELS & WIRES ARE #16 AWG FOR ALL CABLES
- 1. THE COMPLETE REFERENCE SYMBOL DESIGNATION FOR CONNECTORS IS IN 4000 SERIES (EXAMPLE: J37 IS J 4037) EXCEPT THOSE IN ENGINE RELAY BOX, ENGINE JUNCTION BOX, & ENGINE ACCESSORY SECTION.

NOTE: UNLESS OTHERWISE SPECIFIED

| |
|------------------|
| ENR. TOL. |
| .0136 TO .186 TO |
| .254 TO .516 TO |
| .762 TO 1.524 TO |

OPERATING REQUIREMENTS AND LIMITATIONS

Frequently reviewed specifications and limitations applicable to operation of the LV-2A propulsion system are contained in this section.

FUEL PUMP INLET (RJ-1)

The minimum required NPSH for starting at 0 to 120 F is 80 feet. The minimum required NPSH for nominal rated thrust operation at 0 to 120 F is 34 feet. The maximum allowable surge pressure at 0 to 120 F is 160 psig.

OXIDIZER PUMP INLET

At saturation temperature, (1) the minimum required net positive suction head (NPSH) for starting is 55 feet, (2) the minimum NPSH required for nominal rated thrust operation is 55 feet, and (3) the maximum allowable surge pressure is 160 psig.

GROUND AND FLIGHT LOADING CONDITIONS

Handling Load

The main and vernier engines shall withstand a maximum of 4 g handling loads applied in any direction.

Flight Operation

The engine system shall operate satisfactorily without permanent deformation or failure under the following specified loads:

1. Load of 15 g parallel to the direction of flight and 1 g perpendicular to the direction of flight
2. Load of 12 g parallel to the direction of flight and 1.25 g perpendicular to the direction of flight
3. Load of 10 g parallel to the direction of flight and 1.5 g perpendicular to the direction of flight
4. Load of 2.5 g parallel to the direction of flight and 3 g perpendicular to the direction of flight

Critical Customer Connect Point Maximum Loading

The customer connect point maximum loading is as follows:

| <u>Attach Point*</u> | <u>Allowable Loads</u> |
|-----------------------------------|-------------------------------------|
| Mount Attach to Missile (Pt. 1) | $F_y = 63,000$ lb 5930-lb side load |
| Mount Attach to Missile (Pt. 2) | $F_y = 63,000$ lb 5930-lb side load |
| Mount Attach to Missile (Pt. 3) | $F_y = 63,000$ lb 5930-lb side load |
| LOX Inlet Duct | $F_y = 3,200$ lb |
| Fuel Inlet Duct | $F_y = 7,200$ lb |
| Actuator Attach Point | $\pm 10,000$ lb axial force |
| Aft End of Heat Exchanger | 300 lb any direction |
| Forward Attach Lug Heat Exchanger | 380 lb any direction |
| Aft Attach Lug Heat Exchanger | $F_y = \pm 380$ lb |
| | $F_x = \pm 50$ lb |
| | $F_z = \pm 380$ lb |
| Main Oil Discharge | 100 lb any direction |
| LOX Seal Drain | 50 lb any direction |
| Oil Seal Drain | 50 lb any direction |

*Refer to coordinate system

PNEUMATIC SUPPLY

The pneumatic supply as delivered to the main engine manifold will be MIL-N-6011 nitrogen, liquid and gas. The flows quoted are for the propulsion system requirements only. No allowance has been made for other applications.

1. Standby: high-pressure nitrogen, 0.150 lb/min maximum is required at 3000 to 1000 psi for oxidizer pump seal purge and the engine control system bleed and leakage. Nitrogen temperature range is -65 to +160 F.
2. Starting: high-pressure nitrogen, 4.0 lb maximum is supplied at 3000 to 1500 psi and at a temperature range of -65 to +160 F for oxidizer pump seal purge, engine start tank pressurization, and pneumatic control.
3. Flight operation: high-pressure nitrogen, 2.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for oxidizer pump seal purge, controls, and engine lubrication tank pressurization. Maximum flowrate is 0.0115 lb/sec.
4. Vernier engine solo flight: high-pressure nitrogen, 8.0 lb maximum is supplied at 3000 to 800 psia and at a temperature range of -65 to +160 F for vernier tank pressurization and pneumatic control. Maximum flowrate is 0.89 lb/sec.

The regulated pneumatic pressure at the customer supply connect-point is 660 psia.

A nitrogen supply temperature of 70 F was assumed for the above computations.

SECTION II: PROPULSION SYSTEM PERFORMANCE

STEADY-STATE PERFORMANCE

Steady-state performance values presented in this section were obtained from production engine test results. Run-to-run deviations include random instrumentation errors and run-to-run nonrepeatability. The actual component differences are depicted in the engine-to-engine deviations.

RATED MAIN ENGINE PERFORMANCE

The main engine nominal performance values and attendant variations at sea-level standard temperature and pressure, rated thrust and rated mixture ratio appear in Table 5 . The vernier performance values were analytically determined using a typical vernier system downstream of the customer connect points. Since vernier performance depends upon the pressure supplied by the main engine, it will not exactly agree with rated values obtained from vernier production testing. A performance schematic depicting relative positions of flow and pressure data is presented in Fig. 6 .

Run-to-run deviations in engine thrust and mixture ratio, and run-to-run and engine-to-engine deviations in specific impulse for the main engine are presented in Table 6 .

Information regarding effects of nitrogen dilution on engine performance is included for application for analysis in the event of a suspected occurrence. Performance shifts of sea-level engine specific impulse and thrust due to nitrogen dilution of LOX presented in Fig. 7 and 8 were based on test results conducted on an engine system other than, but considered sufficiently descriptive of, the Thor. Empirically determined effects on c^* , C_F , gas generator temperature and LOX density due to nitrogen dilution were imposed on nominal engine data to generate the figures.

TABLE 5

NOMINAL MAIN ENGINE PERFORMANCE VALUES
AT SEA-LEVEL RATED THRUST AND MIXTURE RATIO

| Parameter | Nominal Value | Standard Deviation | |
|---------------------------------------------------------|---------------|-------------------------------|-------------------------|
| | | Engine-to-Engine (S_{EE}) | Run-to-Run (S_{RR}) |
| Engine | | | |
| Oxidizer (LOX) Density, lb/cu ft | 71.38* | | |
| Fuel (RJ-1) Density, lb/cu ft | 53.17* | | |
| Thrust, pounds | 170,000* | | |
| Specific Impulse, seconds | 252.4 | 0.62 | 0.30 |
| Mixture Ratio (o/f), including vernier flow | 2.15* | --- | --- |
| Thrust Chamber | | | |
| Thrust, pounds | 169,500 | --- | --- |
| Specific Impulse, seconds | 257.5 | 0.62 | 0.31 |
| Characteristic Velocity (c^*), injector end, ft/sec | 5958 | 15.4 | 9.5 |
| Thrust Coefficient (C_F), injector end | 1.391 | 0.0038 | 0.0021 |
| Chamber Pressure, injector end, psia | 594.3 | 1.53 | 0.92 |
| Characteristic Velocity, nozzle stagnation, ft/sec | 5517. | --- | --- |
| Thrust Coefficient, nozzle stagnation | 1.502 | --- | --- |
| Chamber Pressure, nozzle stagnation, psia | 550.3 | --- | --- |
| c^* Efficiency, % | 95.5 | 0.25 | 0.15 |
| C_F Efficiency, % | 101.2 | 0.25 | 0.15 |
| Propellant Flowrates, lb/sec | | | |
| Oxidizer | 456.3 | 1.11 | 0.54 |
| Fuel | 201.9 | 0.48 | 0.26 |
| Mixture Ratio (o/f) | 2.260 | 0.0016 | 0.0008 |
| Main Fuel Orifice Pressure Drop, psi | | | |
| at 190 lb/sec and 53.17 lb/cu ft | 55.6 | | |
| Orifice Diameter, inches | 49.2 | 10.3 | 1.8 |
| | 2.74 | | |

TABLE 5
(Continued)

| Parameter | Nominal Value | Standard Deviation | |
|----------------------------------------------------------|---------------|-------------------------------|-------------------------|
| | | Engine-to-Engine (S_{EE}) | Run-to-Run (S_{RR}) |
| Propellant Pumps | | | |
| LOX Pump | | | |
| Inlet Pressure (total), psia | 53.0* | --- | --- |
| Discharge Pressure (total), psia | 862. | 14.8 | 2.9 |
| Developed Head, feet | 1641. | 11.8 | 6.7 |
| Weight Flow, lb/sec | 469.9 | 1.14 | 0.56 |
| Volume Flow, gpm | 2955. | 7.2 | 3.5 |
| Speed, rpm | 6252. | 26.8 | 8.4 |
| Shaft Power, bhp | 1772. | 16.2 | 8.6 |
| Efficiency, % | 79.1 | --- | --- |
| Fuel Pump | | | |
| Inlet Pressure (total), psia | 48.0* | --- | --- |
| Discharge Pressure (total), psia | 902. | 14.8 | 2.9 |
| Developed Head, feet | 2307. | 39.8 | 7.8 |
| Weight Flow, lb/sec | 217.2 | 0.53 | 0.26 |
| Volume Flow, gpm | 1833 | 4.50 | 2.18 |
| Speed, rpm | 6252. | 26.8 | 8.4 |
| Shaft Power, bhp | 1272. | 22.0 | 5.24 |
| Efficiency, % | 71.6 | --- | --- |
| Turbine | | | |
| Turbine Shaft Power, bhp | 3136. | 31. | 13 |
| Turbine Inlet Temperature, F | 1203. | 10.6 | 3.0 |
| Turbine Gas Flow, lb/sec | 15.21 | 0.16 | 0.05 |
| Turbine Exhaust Pressure (static), psia | 23.6 | 1.69 | 0.25 |
| Turbine Inlet Pressure (total), psia | 515.6 | 4.8 | 2.3 |
| Turbine Pressure Ratio (total psia inlet/static exhaust) | 21.8 | --- | --- |

TABLE 5
(Continued)

| Parameter | Nominal Value | Standard Deviation | |
|-------------------------------------------------------------------|---------------|-------------------------------|-------------------------|
| | | Engine-to-Engine (S_{EE}) | Run-to-Run (S_{RR}) |
| Gas Generator | | | |
| Gas Generator Chamber Pressure, injector end, psia | 541.4 | 5.5 | 1.6 |
| LOX Bleed Pressure, psia | 788. | ---- | ---- |
| Fuel Bleed Pressure, psia | 888. | ---- | ---- |
| Total Propellant Flow **, lb/sec | 15.21 | 0.16 | 0.05 |
| LOX Flow**, lb/sec | 3.73 | 0.04 | 0.01 |
| Fuel Flow**, lb/sec | 11.48 | 0.14 | 0.04 |
| Mixture Ratio (o/f) | 0.325 | 0.004 | 0.001 |
| Fuel Orifice Pressure Drop, psi at 10.5 lb/sec and 53.17 lb/cu ft | 167.3 | ---- | ---- |
| Orifice Diameter, inch | 139.9 | ---- | ---- |
| LOX Orifice Pressure Drop, psi at 3.5 lb/sec and 71.38 lb/cu ft | 0.530 | --- | ---- |
| Orifice Diameter, inch | 86.3 | --- | ---- |
| | 75.9 | 14.5 | 1.3 |
| Verniers (Pump-Fed) | | | |
| LOX Flow, lb/sec | 6.56 | 0.054 | 0.019 |
| Fuel Flow, lb/sec | 3.61 | 0.035 | 0.011 |
| Vernier Total Flow, lb/sec | 10.17 | 0.070 | 0.026 |
| Mixture Ratio (o/f) | 1.82 | 0.019 | 0.006 |
| LOX Customer Connect Pressure, psia | 762. | 9.0 | 3.3 |
| Fuel Customer Connect Pressure, psia | 701. | 7.9 | 2.6 |
| Heat Exchanger LOX Flow, lb/sec | 3.17 | 0.045 | 0.046 |

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TABLE 5
(Continued)

| Parameter | Nominal Value | Standard Deviation | |
|-----------------------------------------|---------------|-------------------------------|-------------------------|
| | | Engine-to-Engine (S_{EE}) | Run-to-Run (S_{RR}) |
| Verniers (Solo) | | | |
| LOX Flow, lb/sec | 5.38 | 0.028 | 0.014 |
| Fuel Flow, lb/sec | 3.01 | 0.018 | 0.006 |
| Vernier Total Flow, lb/sec | 8.39 | 0.046 | 0.020 |
| Mixture Ratio (o/f) | 1.78 | 0.007 | 0.006 |
| LOX Customer Connect Pressure, psia | 575. | 4.40 | 2.1 |
| Fuel Customer Connect Pressure, psia | 530. | 4.20 | 1.20 |
| Engine Regulator Pressure Setting, psia | 660. | ---- | ---- |

NOTE: All pressures were measured with a static tap, unless designated as total. Pressure designated as total were calculated from a static measurement.

* Rated value

**Calculated from turbine inlet temperature and pressure

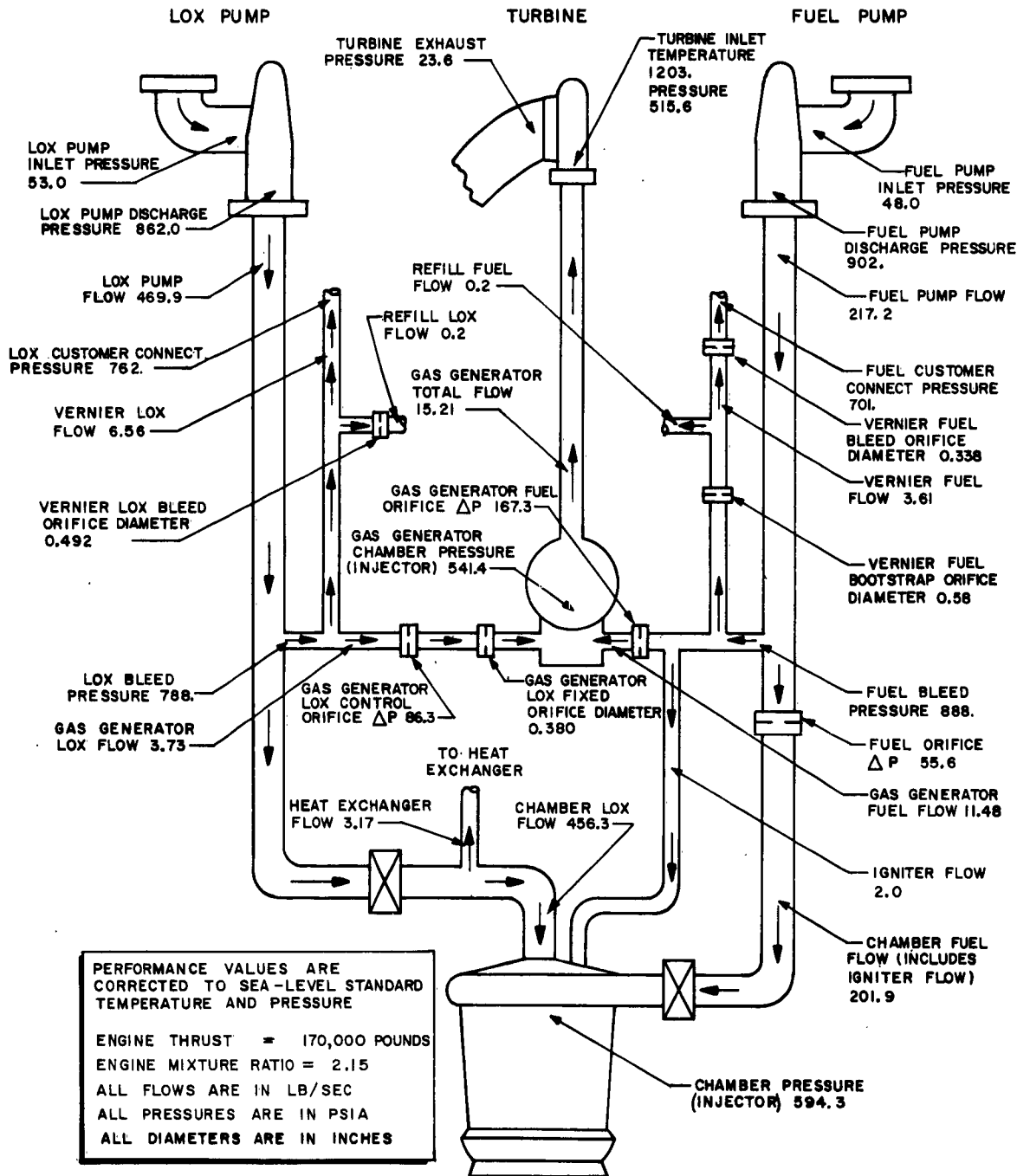


Figure 6. Main Engine Performance Schematic

TABLE 6

PERFORMANCE DEVIATIONS, YLR79-NA-13 THOR MAIN ENGINES
(Data Based on 47 Runs Involving 23 Engines)

| Parameter | Specified or
Mean Value | Deviation, % |
|---------------------------------|----------------------------|--------------|
| <u>Engine Thrust</u> | | |
| Specified, pounds | 170,000. ±3% | |
| Run-to-Run Deviation* | | 0.25 |
| Run-to-Run, 95% Tolerance | | 0.61 |
| <u>Mixture Ratio</u> | | |
| Specified | 2.15 ±1.02% | |
| Run-to-Run Deviation* | | 0.23 |
| Run-to-Run, 95% Tolerance | | 0.56 |
| <u>Specific Impulse**</u> | | |
| Specified Minimum, seconds | 249. | |
| Mean | 252.4 | |
| Run-to-Run Deviation* | | 0.12 |
| Run-to-Run, 95% Tolerance | | 0.29 |
| Engine-to-Engine Deviation | | 0.25 |
| Engine-to-Engine, 95% Tolerance | | 0.61 |
| Over-all Standard Deviation*** | | 0.27 |
| Over-all, 95% Tolerance | | 0.63 |

* Run-to-run standard deviation

** Specific impulse values are quoted at rated thrust and mixture ratio

*** Run-to-run and engine-to-engine standard deviation. This method of combination allows a conservative estimation.

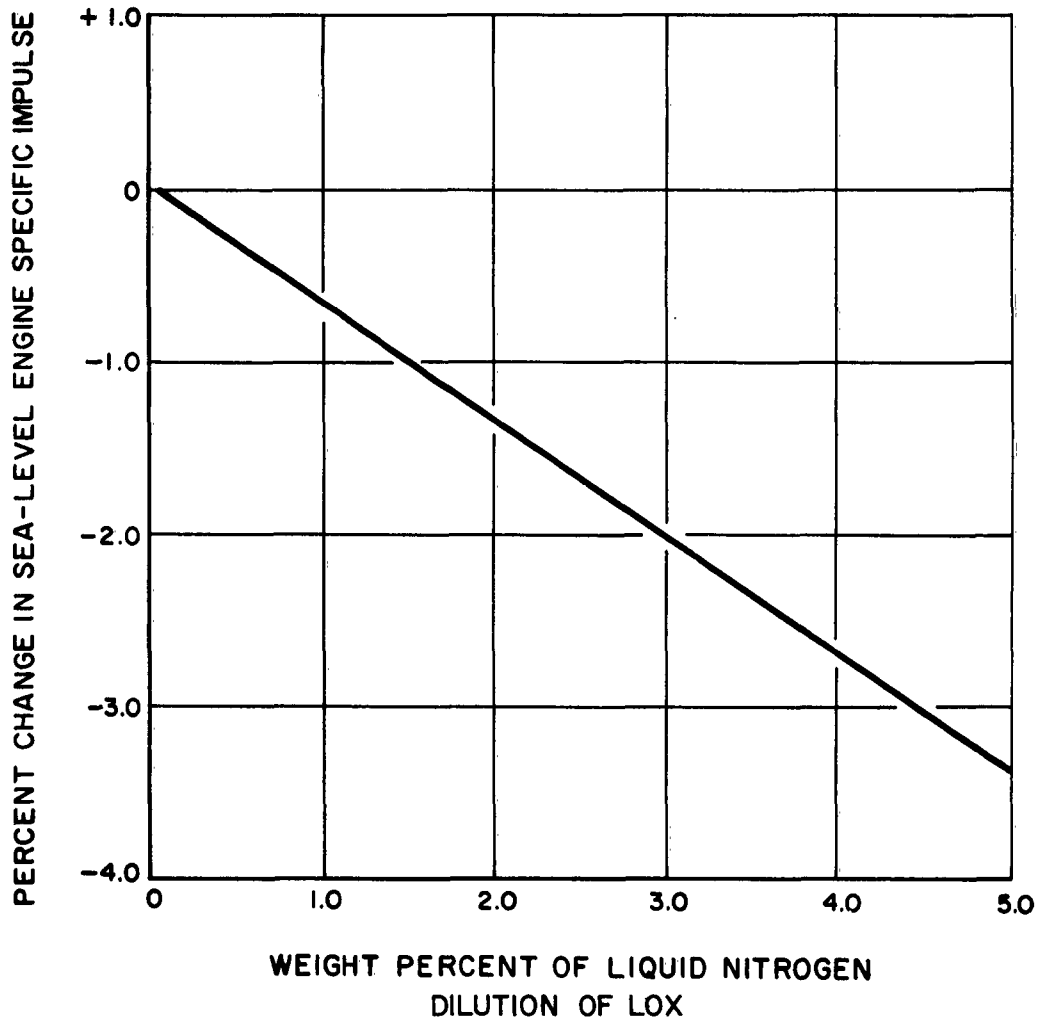


Figure 7. Effects of Liquid Nitrogen Dilution on Sea Level Engine Specific Impulse

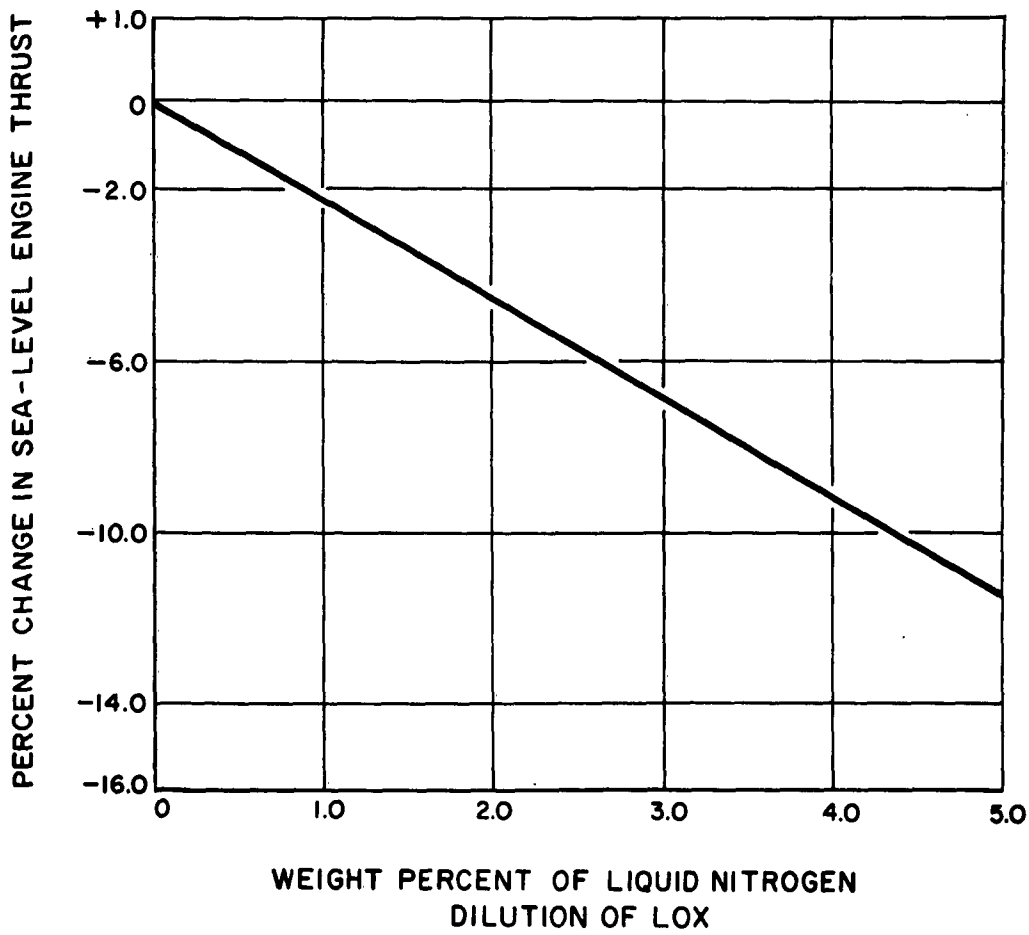


Figure 8. Effects of Liquid Nitrogen Dilution on Sea-Level Engine Thrust.

RATED VERNIER ENGINE PERFORMANCE

Statistical analyses of LR101-NA-11 vernier engine data are presented in Table 7 , covering mean performance, run-to-run, and engine-to-engine variations. The data are based on 94 tests on 47 acceptance engines. RP-1 was used for all tests. Data were reduced to sea-level standard temperature and pressure rated thrust, mixture ratio, and propellant inlet pressures prior to statistical analysis. The data reduction program computes orifices required to give rated thrust and mixture ratio at tank-fed conditions. With these orifices, the program then computes what thrust and mixture ratio would be under pump-fed conditions.

The following standard conditions are used by the data reduction program:

| <u>Rated Parameter</u> | <u>Tank-Fed</u> | <u>Pump-Fed</u> |
|---------------------------------|-----------------|-----------------|
| Thrust, pounds | 830 | --- |
| Mixture Ratio | 1.80 | --- |
| LOX Inlet Pressure, psia | 540 | 660 |
| Fuel Inlet Pressure, psia | 510 | 636 |
| LOX Specific Gravity, lb/cu ft | 66.27 | 70.73 |
| Fuel Specific Gravity, lb/cu ft | 50.48 | 50.48 |

A schematic of vernier operation under pump-fed conditions (with RJ-1 fuel) appears in Fig. 9..

TABLE 7

NOMINAL LR101-NA-11 VERNIER ENGINE PERFORMANCE
AND PERFORMANCE DEVIATIONS

| Parameter | Mean Value | S_{EE} | C_{VEE} | S_{RR} | C_{VRR} |
|------------------------------------------------------------|------------|----------|-----------|----------|-----------|
| <u>Tank-Fed</u> | | | | | |
| Specific Impulse, seconds | 198.7 | 1.92 | 0.97 | 1.12 | 0.56 |
| Characteristic Velocity (c^*),
Injector End, ft/sec | 4942 | 69.9 | 1.41 | 29.1 | 0.59 |
| Thrust Coefficient (C_F),
Injector End | 1.294 | 0.007 | 0.55 | 0.005 | 0.35 |
| Chamber Pressure, Injector End, psia | 305.4 | 2.64 | 0.86 | 0.85 | 0.28 |
| Chamber Pressure, Nozzle, psia | 298. | -- | -- | -- | -- |
| LOX Weight Flow, lb/sec | 2.68 | -- | -- | -- | -- |
| Fuel Weight Flow, lb/sec | 1.49 | -- | -- | -- | -- |
| LOX Orifice Differential
Pressure, psi | 39.8 | 7.96 | 20.0 | 2.97 | 7.44 |
| Fuel Orifice Differential
Pressure, psi | 27.6 | 7.68 | 27.8 | 3.33 | 12.05 |
| <u>Pump-Fed</u> | | | | | |
| Thrust, pounds | 1017 | 5.64 | 0.55 | 4.19 | 0.41 |
| Mixture Ratio | 1.803 | 0.010 | 0.54 | 0.011 | 0.61 |
| Specific Impulse, seconds | 209.8 | 2.21 | 1.05 | 0.83 | 0.39 |
| c^* , Injector End, ft/sec | 5054. | 51.5 | 1.02 | 21.0 | 0.42 |
| C_F , Injector End | 1.336 | 0.005 | 0.39 | 0.005 | 0.37 |

TABLE 7
(Continued)

| Parameter | Mean Value | S_{EE} | C_{VEE} | S_{RR} | C_{VRR} |
|--------------------------------------|------------|----------|-----------|----------|-----------|
| Chamber Pressure, Injector End, psia | 362.5 | 3.39 | 0.93 | 1.70 | 0.47 |
| Chamber Pressure, Nozzle, psia | 353. | -- | -- | -- | -- |
| LOX Weight Flow, lb/sec | 3.12 | -- | -- | -- | -- |
| Fuel Weight Flow, lb/sec | 1.73 | -- | -- | -- | -- |

S_{EE} Engine-to-engine standard deviation

C_{VEE} Engine-to-engine coefficient of variation (standard deviation expressed as percentage of the mean)

S_{RR} Run-to-run standard deviation

C_{VRR} Engine-to-engine coefficient of variation (standard deviation expressed as percentage of the mean)

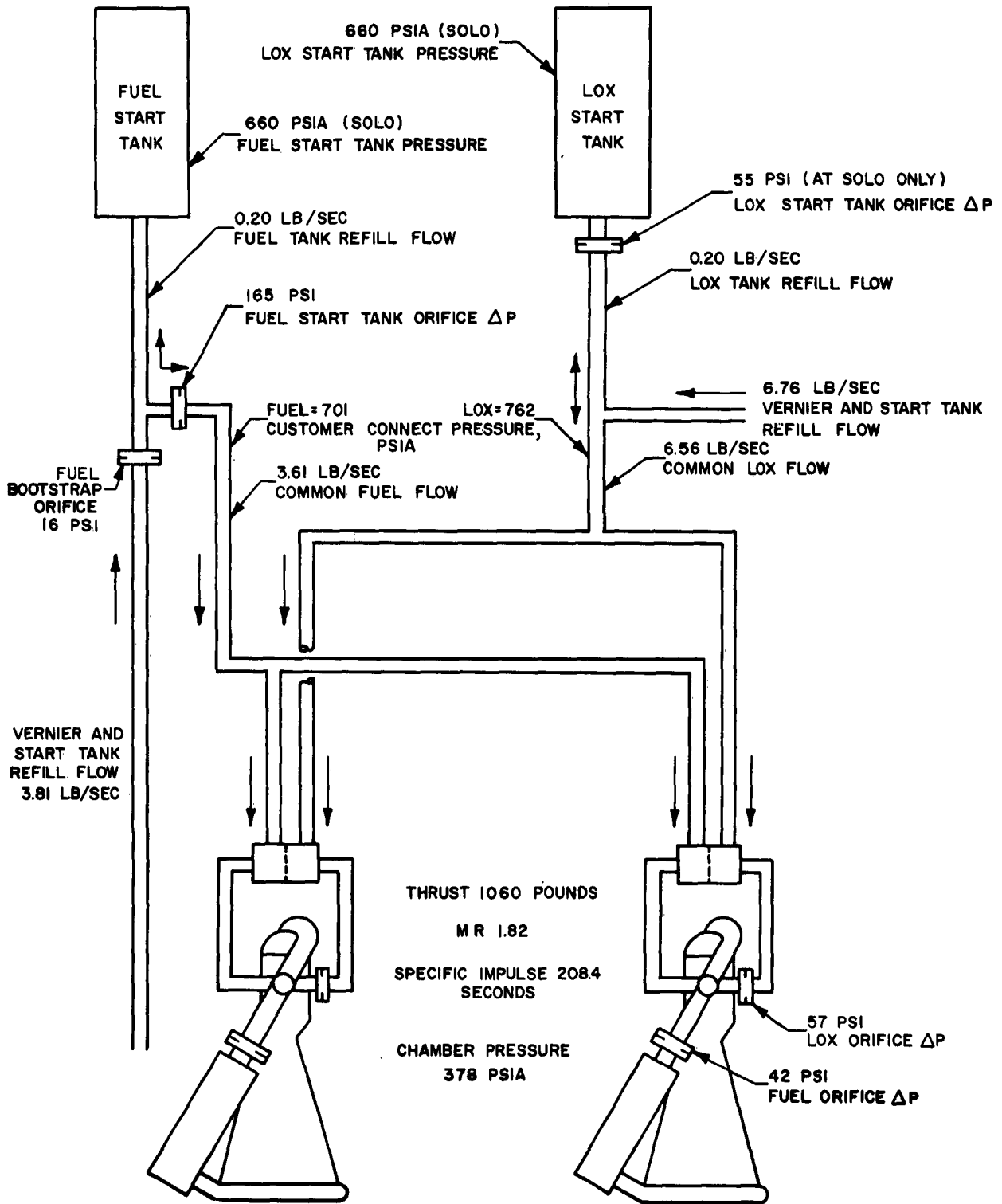


Figure 9. LR79-NA-11 Vernier Pump-Fed Performance Schematic

INFLUENCE COEFFICIENTS

LINEARIZED SOLUTIONS

Engine influence coefficients result from a linearized solution of a set of steady-state equations which describe the operation of an engine. Each influence coefficient is expressed in percentage form, and represents the effect that a 1% increase in an engine independent variable will have on an engine dependent variable. A coefficient preceded by a positive (+) sign (or no sign) indicates that an increase in the independent variable results in an increase in the dependent variable; a coefficient preceded by a negative (-) sign indicates that an increase in the independent variable results in a decrease in the dependent variable.

ILLUSTRATION

Figure 10 is a portion of a typical table of engine influence coefficients. This table is in the form as printed by a high-speed digital computer. The symbols E 01, E 04, etc., placed after the nominal values in the table represent powers of 10. Hence 1.4696E 01 is equivalent to 14.696; 6.0000E 04 is equivalent to 60,000; etc.

APPLICATION

These influence coefficients may be applied to two different situations; (1) calculations involving an engine type, or (2) calculations involving a specific engine.

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A ONE-PERCENT INCREASE IN ANY ONE OF THE INDEPENDENT VARIABLES CAUSES THE FOLLOWING PERCENTAGE CHANGE IN ANY ONE OF THE DEPENDENT VARIABLES.

| -INDEPENDENT VARIABLES- | | | | | | |
|---------------------------------|------------|---------|---------|--------|----|---------|
| 1. ATMOSPHERIC PRES - - - - - | 1.4696E 01 | | | | | |
| 2. FUEL DENSITY - - - - - | 5.0450E 01 | | | | | |
| 3. OXID DENSITY - - - - - | 7.1380E 01 | | | | | |
| 4. FUEL PUMP INLET PRES - - - - | 7.7000E 01 | | | | | |
| 5. OXID PUMP INLET PRES - - - - | 5.3000E 01 | | | | | |
| 6. C* CORRECTION - - - - - | | | | | | |
| | 1- | 2- | 3- | 4- | 5- | 6- |
| -DEPENDENT VARIABLES- | | | | | | |
| ENGINE THRUST - - 6.0000E 04 | | | | | | |
| | -0.4556 | 0.5326 | 0.0703 | 0.0576 | 0 | 0.6494 |
| ENGINE ISP - - - 2.3000E 02 | | | | | | |
| | -0.4426 | 0.1462 | 0.0341 | 0.0182 | 0 | 1.1677 |
| ENGINE MR - - - - 2.2700E 00 | | | | | | |
| | -0.0039 | -0.4054 | 0.3016 | 0.0200 | 0 | -0.4134 |
| ENGINE FUEL FLOW- 7.9770E 01 | | | | | | |
| | -0.0096 | 0.6588 | -0.1688 | 0.0243 | 0 | -0.2268 |
| ENGINE OXID FLOW- 1.8110E 02 | | | | | | |
| | -0.0145 | 0.2674 | 0.1256 | 0.0461 | 0 | -0.6462 |

Figure 10 . Sample Table of Influence Coefficients
as Printed by High-Speed Digital Computer

Calculations Involving an Engine Type

Suppose it were desired to determine the thrust of the engine described by the sample table of influence coefficients when operated under the following conditions:

- | | |
|---------------------------------|------------------|
| 1. Atmospheric pressure | = 1.40 psia |
| 2. Fuel density | = 50.45 lb/cu ft |
| 3. Oxidizer density | = 69.55 lb/cu ft |
| 4. Fuel pump inlet pressure | = 69.30 psia |
| 5. Oxidizer pump inlet pressure | = 59.55 psia |

Because the influence coefficients are linear, the total effect of several influences acting simultaneously on an engine can be determined by adding the individual effects of each influence. The change in engine thrust would be

$$\begin{aligned}
 \frac{F_E - F_{E_i}}{F_{E_N}} &= \frac{P_a - P_{a_i}}{P_{a_N}} (F_{P_a}) + \frac{\rho_F - \rho_{F_i}}{\rho_{F_N}} (F_{\rho_F}) \\
 &+ \frac{\rho_o - \rho_{o_i}}{\rho_{o_N}} (F_{\rho_o}) + \frac{P_F - P_{F_i}}{P_{F_N}} (F_{P_F}) \\
 &+ \frac{P_o - P_{o_i}}{P_{o_N}} (F_{P_o}), \tag{1}
 \end{aligned}$$

Where F_E , P_a , ρ_F , ρ_o , etc., are the actual values of these parameters for the problems considered.

$F_{E_i}, P_{a_i}, \rho_{F_i}, \rho_{o_i}$, etc., are the initial or base values of these parameters.

$F_{E_N}, P_{a_N}, \rho_{F_N}, \rho_{o_N}$, etc., are the nominal values of these parameters, listed in the table of influence coefficients.

$F_{P_a}, F_{\rho_F}, F_{\rho_o}$, etc., are the influence coefficients for engine thrust found in the appropriate columns of the table of influence coefficients.

For calculations involving an engine type, the initial values would be the same as the nominal values, and $F_{E_i} = F_{E_N}, P_{a_i} = P_{a_N}, \rho_{F_i} = \rho_{F_N}, \rho_{o_i} = \rho_{o_N}$, etc.

The calculation for the example stated above would be as follows:

$$\begin{aligned} \frac{F_E - 60,000}{60,000} &= \left(\frac{1.40 - 14.696}{14.696} \right) (-0.4556) + \left(\frac{50.45 - 50.45}{50.45} \right) (+0.5326) \\ &+ \left(\frac{69.55 - 71.38}{71.38} \right) (+0.0703) + \left(\frac{69.30 - 77.00}{77.00} \right) (+0.0576) \\ &+ \left(\frac{59.55 - 53.00}{53.00} \right) (0) \end{aligned}$$

$$\begin{aligned} \frac{F_E - 60,000}{60,000} &= -0.9047 \cdot (-0.4556) + 0(+0.5326) \\ &- 0.0256 (+0.0703) - 0.1000 (+0.0576) \\ &+ 0.1236 (0) = +0.4046 \text{ or } +40.46\% \end{aligned}$$

Therefore:

$$F_E = +0.4046 (60,000) + 60,000$$

$$F_E = +24,276 + 60,000 = 84,276 \text{ pounds}$$

The incremental thrust change has been found to be +24,276 pounds for the conditions stated, yielding a final engine thrust of 84,276 pounds.

Calculations Involving a Specific Engine.

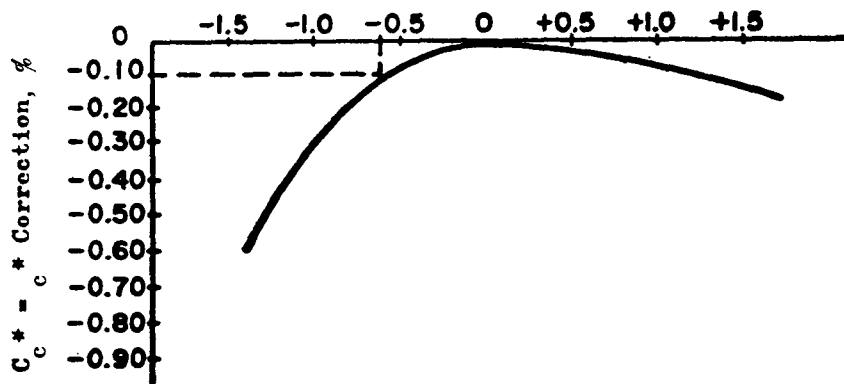
When the values of actual engine parameters differ from those used as nominal values in the table of influence coefficients, the "delta method" of application of influence coefficients is used. This procedure consists of computing an incremental change of variables rather than a percentage change of these variables. The incremental change is then applied to the actual engine value. This effect can be accomplished by using Eq. (1) if the quantities F_{E_i} , P_{a_i} , ρ_{F_i} , ρ_{O_i} , etc., are defined as the actual engine values of these parameters. All other quantities are as defined previously.

NONLINEAR CORRECTIONS

A special computational procedure has been devised to extend the usefulness of engine influence coefficients. This technique is used to allow nonlinear corrections to be made for certain parameters where the linear approximation is not sufficiently accurate. An example of this method is the c^* correction (C_{c^*}). In this case, a plot of C_{c^*} vs the change in engine mixture ratio is included with the table of influence coefficients. Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

A typical plot of these parameters is shown below:

$$\left(\frac{\mu_E - \mu_{EN}}{\mu_{EN}} \right) 100 = \left(\frac{\text{Change in Engine Mixture Ratio}}{\text{Nominal Engine Mixture Ratio}} \right) 100\%$$



The change in engine mixture ratio is computed for the changes in atmospheric pressure, propellant densities, etc., and with the assumption that the c^* correction is zero. With this change in engine mixture ratio, the c^* correction is read from the curve. This value of c^* correction is used with the other independent variables to compute the changes in the remaining dependent variables.

For example, if the change in engine mixture ratio accompanying the +40.46% thrust change in the preceding example were -0.62%, then the c^* correction from the curve is -0.10%. The true change in engine thrust is therefore:

$$(\% \text{ change in } F_E = +40.46 - 0.10 (+0.6494) = +40.40\%)$$

Similarly, other nonlinear corrections would be applied as additional terms in the summation of effects.

LV-2A INFLUENCE COEFFICIENTS

Current influence coefficients for the LV-2A propulsion system are presented in Tables 8 and 9. Table 8 includes the additional effect of fuel temperature on system performance while considering fuel density a constant. Any density change, therefore, is considered independently.

The effects of engine mixture ratio on c^* in terms of a correction appear in Fig. 11.

TABLE 8

INFLUENCE COEFFICIENTS FOR THE YLR79-N/
AND LR101-NA-11 VERNIER ENGINE

A 1% increase in any one of the independent variables
following percentage change in any one of the

| | <u>Independent Variables</u> | |
|--|-----------------------------------|--------|
| | 1. Atmospheric Pressure, psia | 14.696 |
| | 2. Fuel Density, lb/cu ft | 53.170 |
| | 3. Oxidizer Density, lb/cu ft | 71.380 |
| | 4. Fuel Pump Inlet Pressure, psia | 48.000 |

| <u>Dependent Variables</u> | <u>Nominal Values</u> | <u>1</u> |
|---------------------------------------------------|-----------------------|----------|
| Engine Thrust Without Verniers, pounds | 170,000. | -0.1472 |
| Engine Specific Impulse Without Verniers, seconds | 252.26 | -0.1404 |
| Engine Mixture Ratio With Verniers | 2.1500 | -0.0001 |
| Engine Fuel Flow With Verniers, lb/sec | 217.13 | -0.0067 |
| Engine Oxidizer Flow With Verniers, lb/sec | 466.83 | -0.0068 |
| Vernier Oxidizer Flow, lb/sec | 6.4860 | -0.0056 |
| Vernier Fuel Flow, lb/sec | 3.5637 | -0.0058 |
| Vernier Thrust, pounds | 2112.0 | -0.1702 |
| Thrust Chamber Nozzle Stagnation Pressure, psia | 551.53 | -0.0069 |
| Fuel Pump Outlet Pressure, psia | 901.35 | -0.0091 |
| Oxidizer Pump Outlet Pressure, psia | 861.27 | -0.0089 |
| Pump Speed, rpm | 6260.8 | -0.0051 |



TABLE 8

FOR THE YLR79-NA-13 THOR MAIN ENGINE
11 VERNIER ENGINES (PUMP-FED)

By one of the independent variables causes the
change in any one of the dependent variables

Independent Variables

| | | |
|--------|----------------------------------------------|--------|
| 14.696 | 5. Oxidizer Pump Inlet Pressure, psia | 53.000 |
| 53.170 | 6. c* Correction | 1.0000 |
| 71.380 | 7. Fuel Temperature (at constant density), F | 60.000 |
| 48.000 | | |

| Partial
Derivatives | <u>1</u> | <u>2</u> | <u>3</u> | <u>4</u> | <u>5</u> | <u>6</u> | <u>7</u> |
|------------------------|----------|----------|----------|----------|----------|----------|----------|
| 100. | -0.1472 | -0.6862 | 1.8030 | -0.0178 | 0.0685 | 1.0844 | -0.0039 |
| 16 | -0.1404 | -0.0736 | 0.2228 | -0.0017 | 0.0085 | 1.1346 | -0.0001 |
| 0 | -0.0001 | -1.6245 | 1.6197 | -0.0533 | 0.0614 | -0.0374 | -0.0256 |
| 3 | -0.0067 | 0.5003 | 0.4707 | 0.0204 | 0.0179 | -0.0178 | 0.0138 |
| 3 | -0.0068 | -1.1242 | 2.0903 | -0.0329 | 0.0794 | -0.0552 | -0.0119 |
| 0 | -0.0056 | -0.7031 | 1.6793 | -0.0193 | 0.0563 | 0.4534 | -0.0060 |
| 7 | -0.0058 | 0.3569 | 0.6199 | 0.0085 | 0.0256 | 0.3638 | 0.0076 |
| 0 | -0.1702 | -0.6315 | 1.7772 | -0.0176 | 0.0604 | 0.5157 | -0.0046 |
| 3 | -0.0069 | -0.5675 | 1.5463 | -0.0145 | 0.0588 | 0.9510 | -0.0029 |
| 5 | -0.0091 | -0.3755 | 1.3415 | 0.0044 | 0.0509 | 0.5976 | 0.0077 |
| 7 | -0.0089 | -1.0884 | 2.0517 | -0.0304 | 0.0897 | 0.6184 | -0.0093 |
| 8 | -0.0051 | -0.6687 | 0.6730 | -0.0189 | 0.0256 | 0.2659 | -0.0061 |



TABLE 9

INFLUENCE COEFFICIENTS FOR THE IR101-NA-11 VERNIER ENGINE OPERATING AT SOLO CONDITIONS

A 1% increase in any one of the independent variables causes the following percentage change in any one of the dependent variables.

| | | <u>Independent Variables</u> | | | | |
|-----------------------------------|-----------------------|------------------------------|----------|----------|----------|----------|
| | | <u>1</u> | <u>2</u> | <u>3</u> | <u>4</u> | <u>5</u> |
| <u>Dependent Variables</u> | <u>Nominal Values</u> | | | | | |
| 1. Atmospheric Pressure, psia | 14.696 | | | | | 510.00 |
| 2. Fuel Density, lb/cu ft | 50.480 | | | | | 540.00 |
| 3. Oxidizer Density, lb/cu ft | 66.270 | | | | | |
| Vernier Thrust, pounds | 830.00 | -0.2082 | 0.0358 | 0.3285 | 0.0897 | 0.7599 |
| Vernier Specific Impulse, seconds | 198.27 | -0.2082 | -0.1051 | 0.1767 | -0.2635 | 0.4086 |
| Vernier Mixture Ratio | 1.8000 | 0. | -0.4947 | 0.5237 | -1.2400 | 1.2114 |
| Vernier Fuel Flow, lb/sec | 1.4951 | 0. | 0.4589 | -0.1848 | 1.1503 | -0.4275 |
| Vernier Oxidizer Flow, lb/sec | 2.6912 | 0. | -0.0358 | 0.3389 | -0.0897 | 0.7839 |

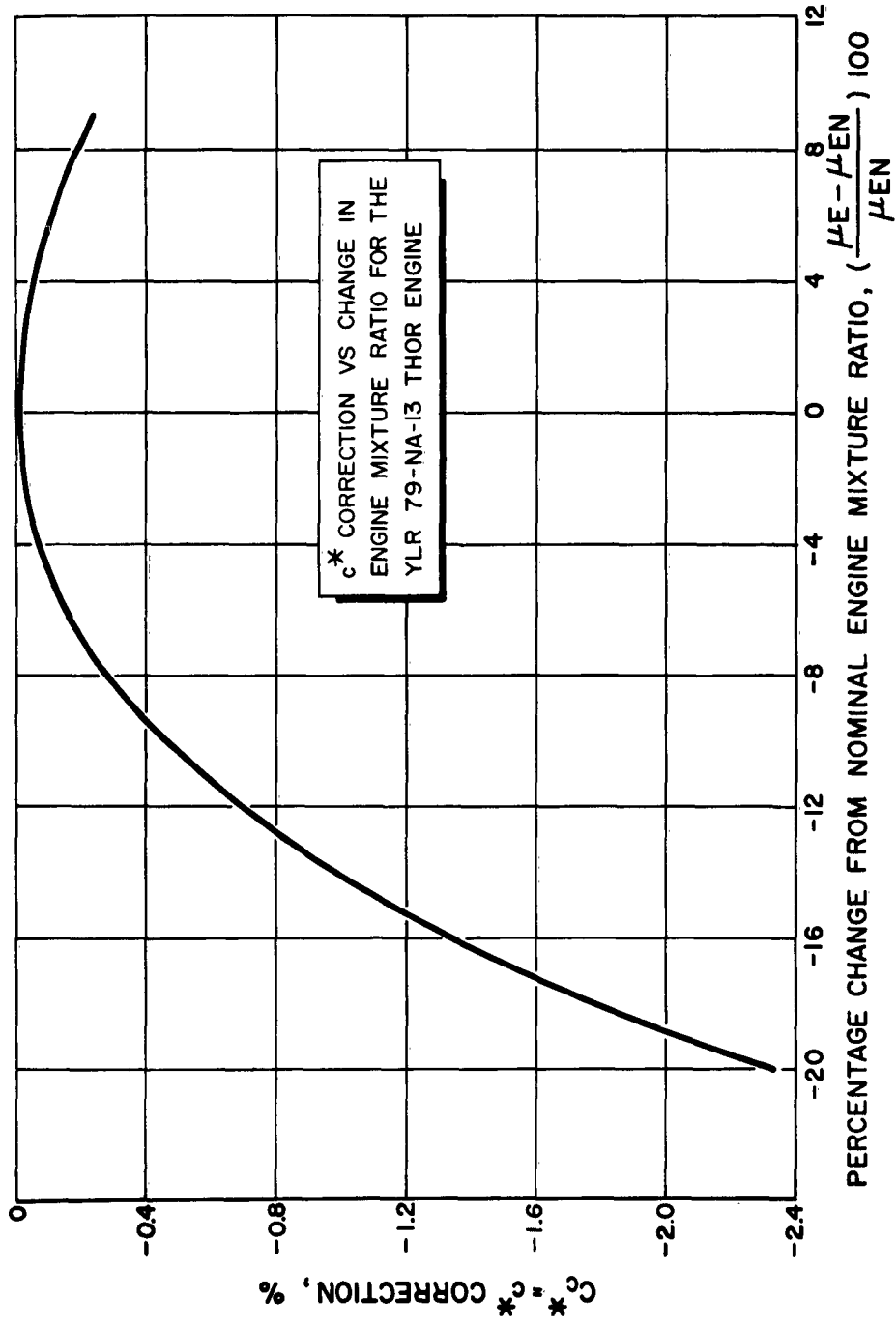


Figure 11. c^* Correction vs Change in Engine Mixture Ratio for the YLR79-NA-13 Thor Main Engine

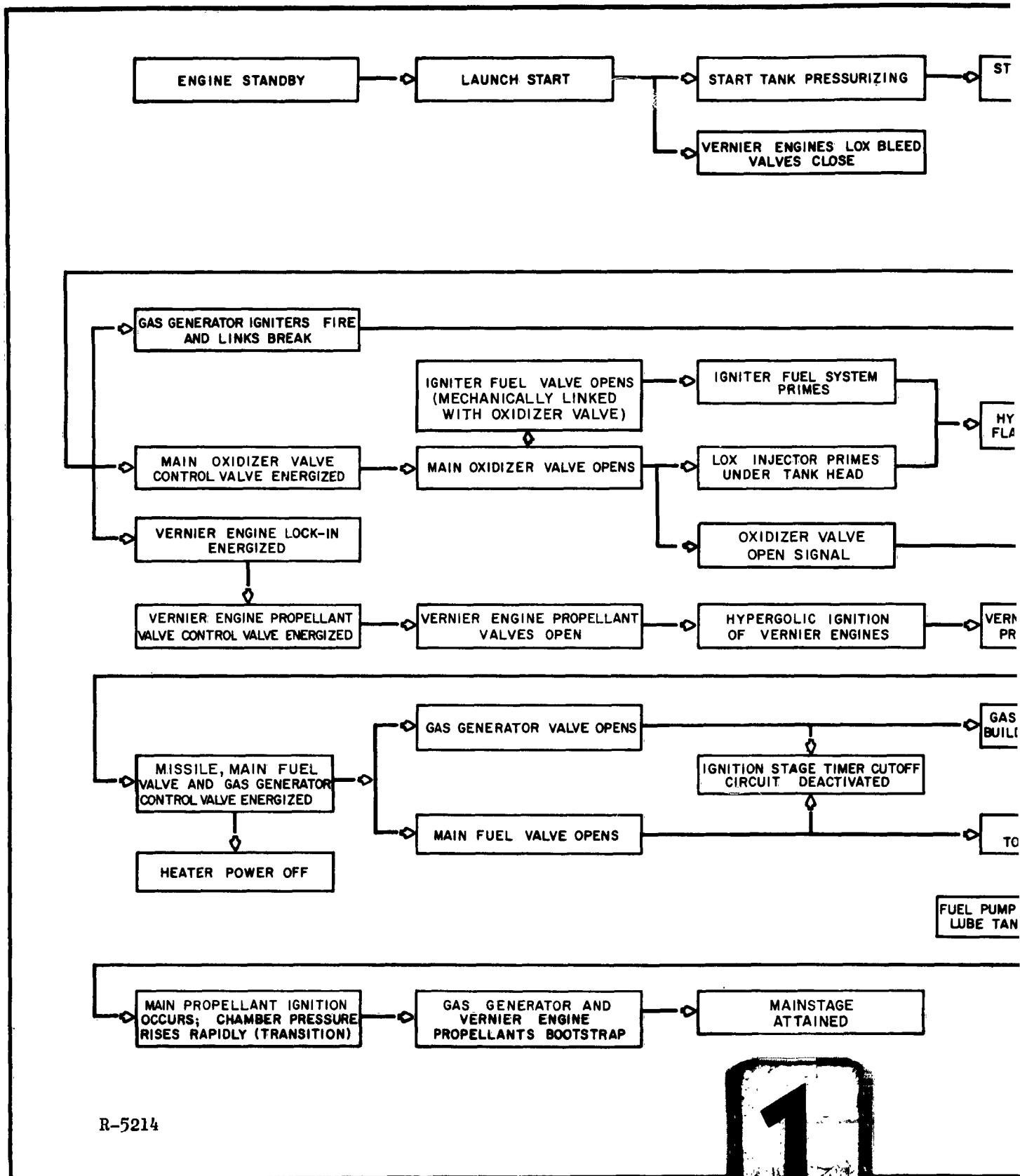
TRANSIENT CHARACTERISTICS

The following portion of this report is devoted to a detailed description of YLR79-NA-13 main engine and LR101-NA-11 vernier engines transient operating characteristics during starting, stabilization, and cutoff. Considered are electromechanical sequencing, engine systems major flows and pressures, and start tanks refill operation. It should be noted that all relationships are typical of static firing operation but are considered good approximations of missile launching conditions as well. Data from simulated missile starts were used where available.

START AND CUTOFF SEQUENCE

The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are electrically sequenced for appropriate start and cutoff operation. All valves are pneumatically operated with a 660 psia regulated gaseous nitrogen supply. Pneumatic restrictors (orifices) are used in conjunction with the valves to provide desired actuation delay and movement times.

Figures 12 and 13 schematically represent electromechanical start and cutoff sequence requirements. Figure 14 displays the average time function of the sequence of events during start and cutoff.



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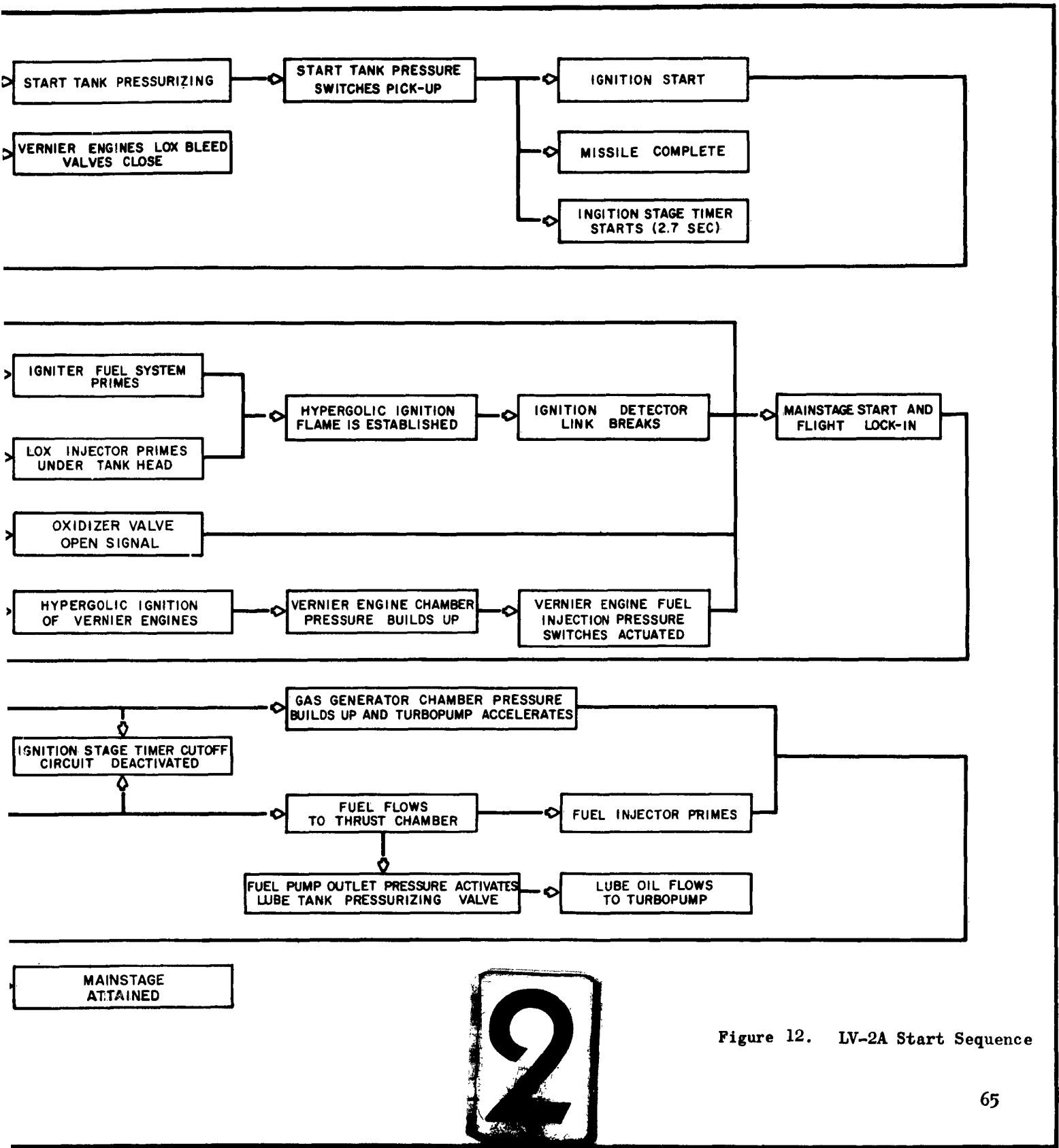


Figure 12. LV-2A Start Sequence

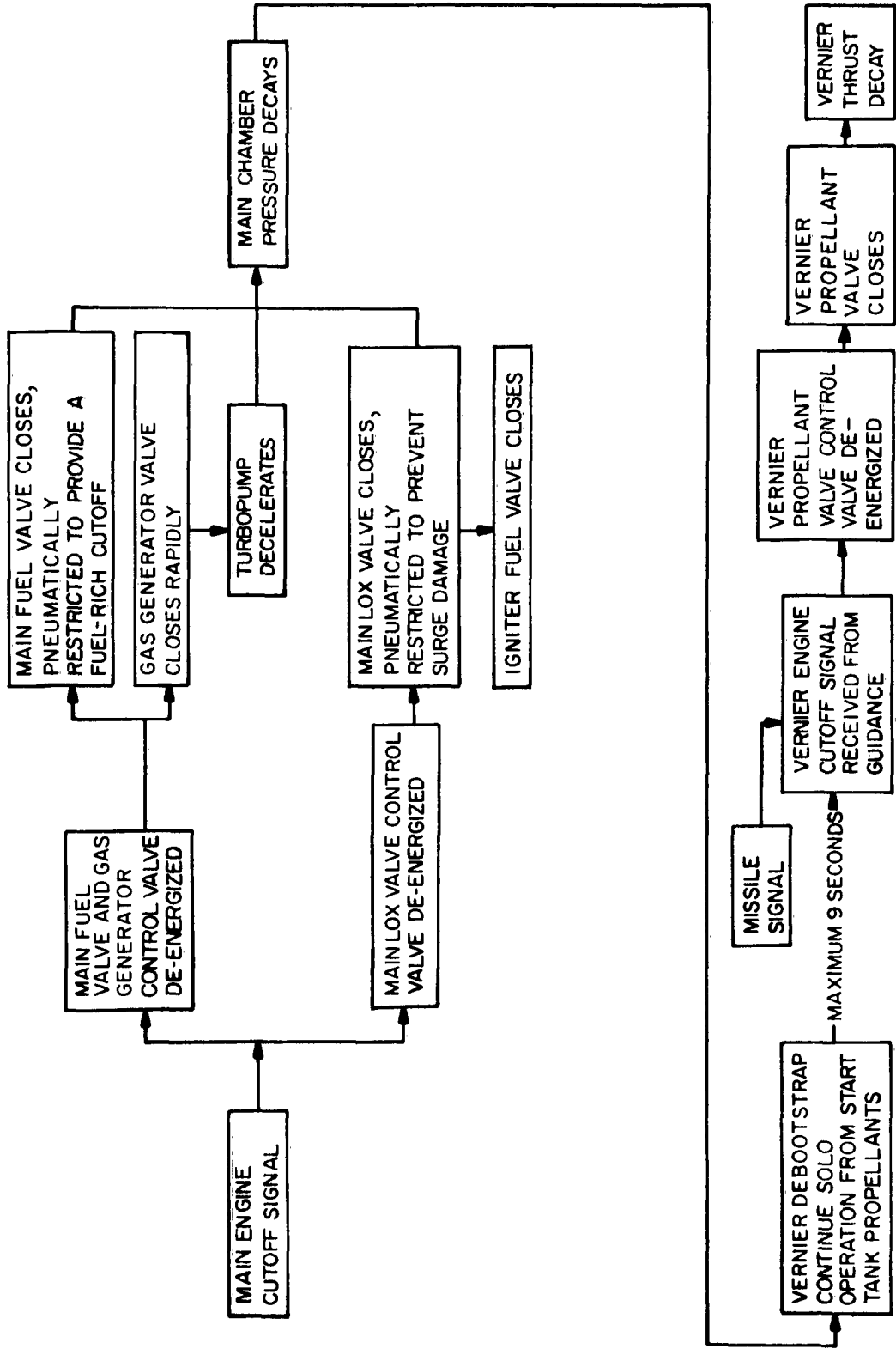


Figure 13. IV-2A Cutoff Sequence

START SEQUENCE

▲ LAUNCH START

▲ START TANKS PRESSURIZED

▲ IGNITION START

■ MAIN LOX VALVE IGNITION AND FUEL VALVE OPEN

■ VERNIER ENGINE PROPELLANT VALVES OPEN, HYPER

▲ GAS GENERATOR IGNITERS FIRE

▲ MAIN CHAMBER HYPERGOLIC IGNITION OCCURS

▲ GAS GENERATOR LINKS BREAK

▲ IGNITION DETECTOR LINK BRE

▲ VERNIER ENGINES FUEL

▲ MAINSTAGE START

■ GAS GENERATOR B

■ MAIN

CUTOFF SEQUENCE

▲ MAIN ENGINE CUTOFF SIGNAL

■ GAS GENERATOR BLADE VALVE CLOSES

■ MAIN LOX VALVE CLOSES

■ MAIN FUEL VALVE CLOSES

▲ 90% CHAMBER PRESSURE

0 0.2 0.4 0.6 0.8 1.0 1.2 1.4 1.6

TIME, SECON

FORM R 18-G-18

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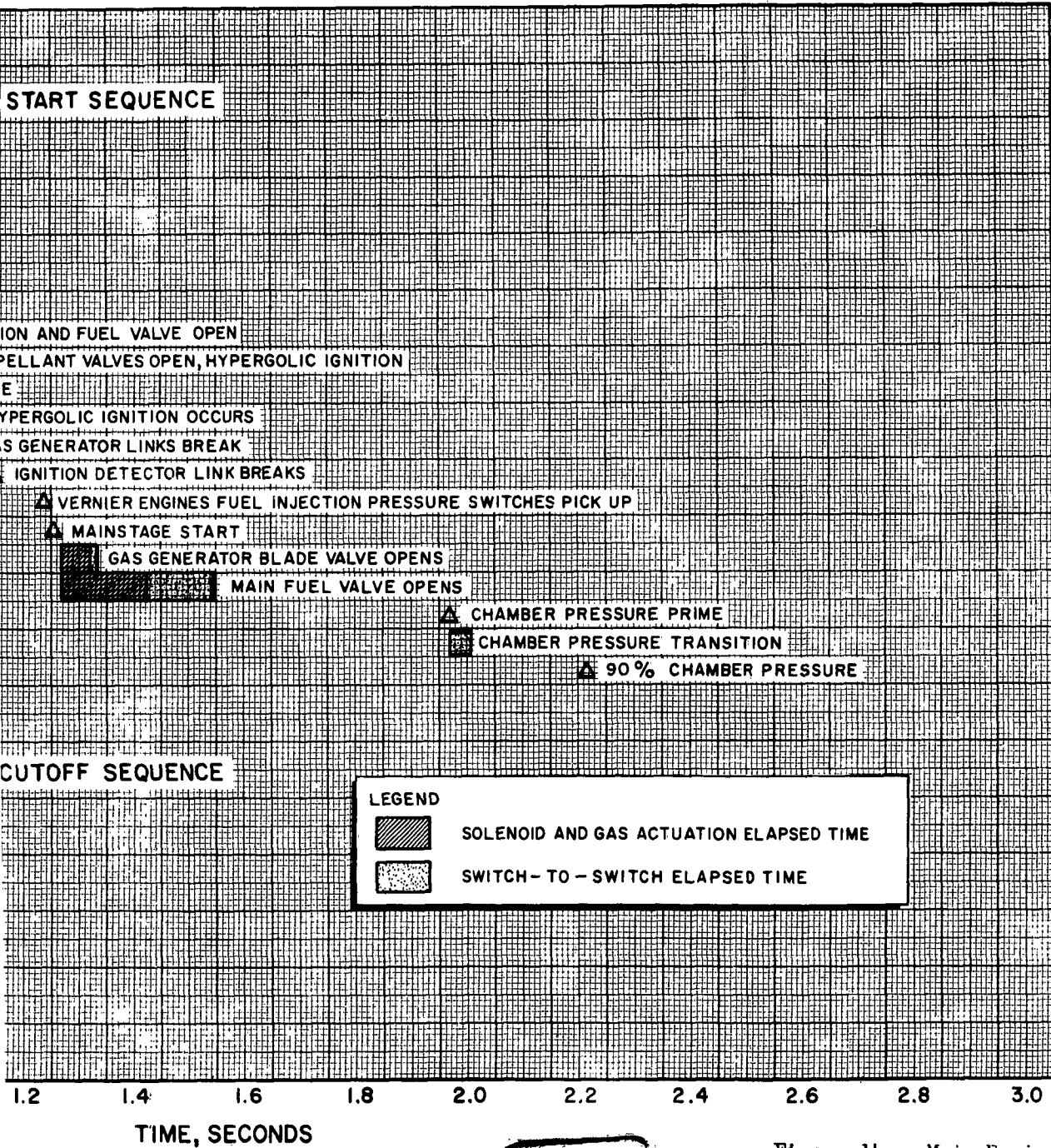


Figure 14. Main Engine Electromechanical Start and Cutoff Time Sequence



START AND CUTOFF TRANSIENT CHARACTERISTICS

The YLR79-NA-13 main engine and LR101-NA-11 vernier engines are ignited by pyrophoric cartridges with an integrated start-vernier solo tank system. Main chamber ignition flame is established by LOX supplied to the injector under tank head, along with start-tank-supplied igniter fuel to spray disks located in each of the six baffled compartments. No chamber fuel jacket prefill is used. Gas generator igniters are pyrotechnic.

Figures 15 through 17 portray typical start characteristics (primarily propellant flows) of the pump main chamber, and auxilliary systems. Figures 18 and 19 are typical oscillographic recordings (primarily pressures) of an engine start and cutoff, respectively. Vernier engines were simulated during this test. Estimated prelaunch propellant consumption (ignition start to 90% chamber pressure) and start tank refill operation are presented in Tables 10 and 11.

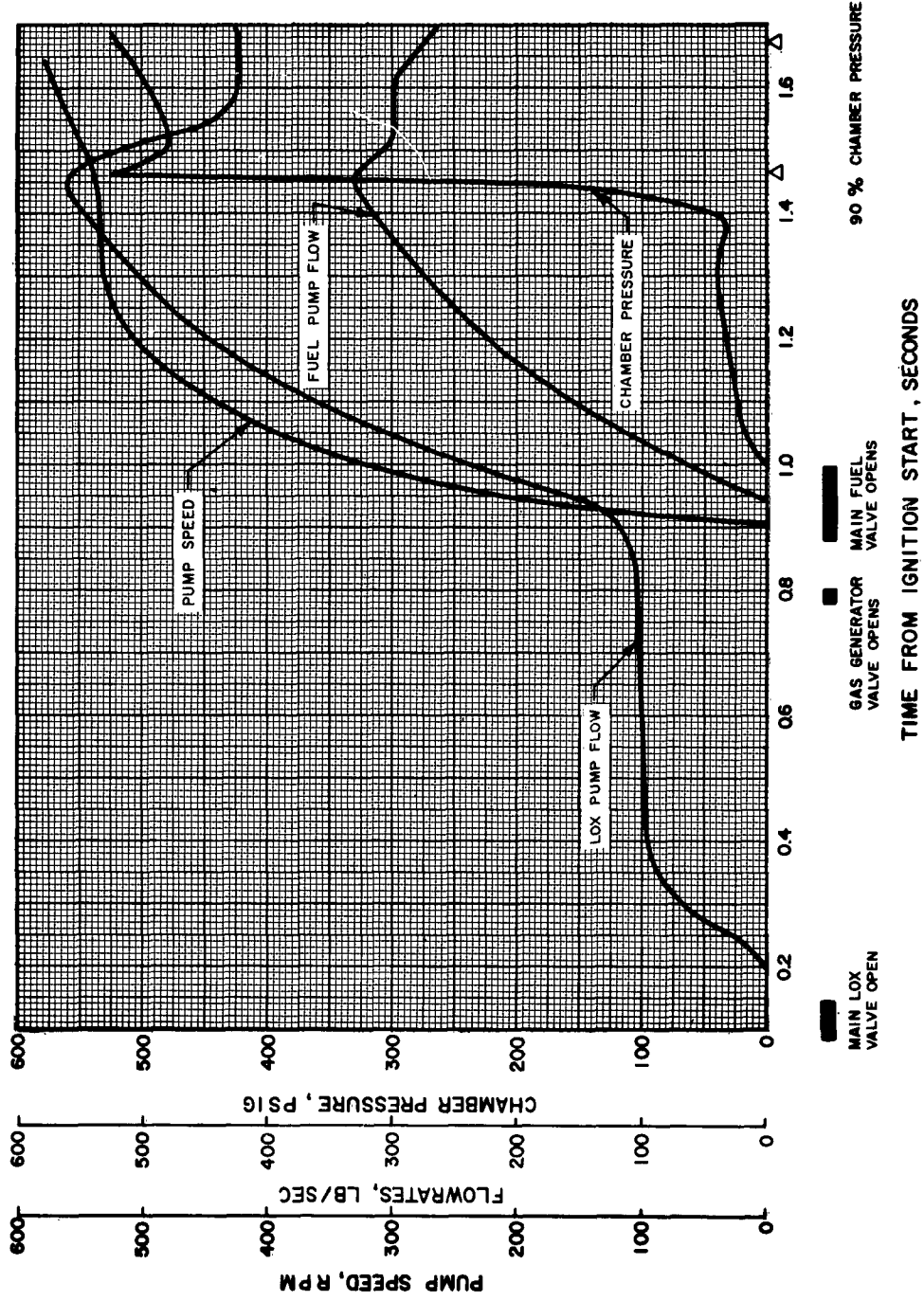
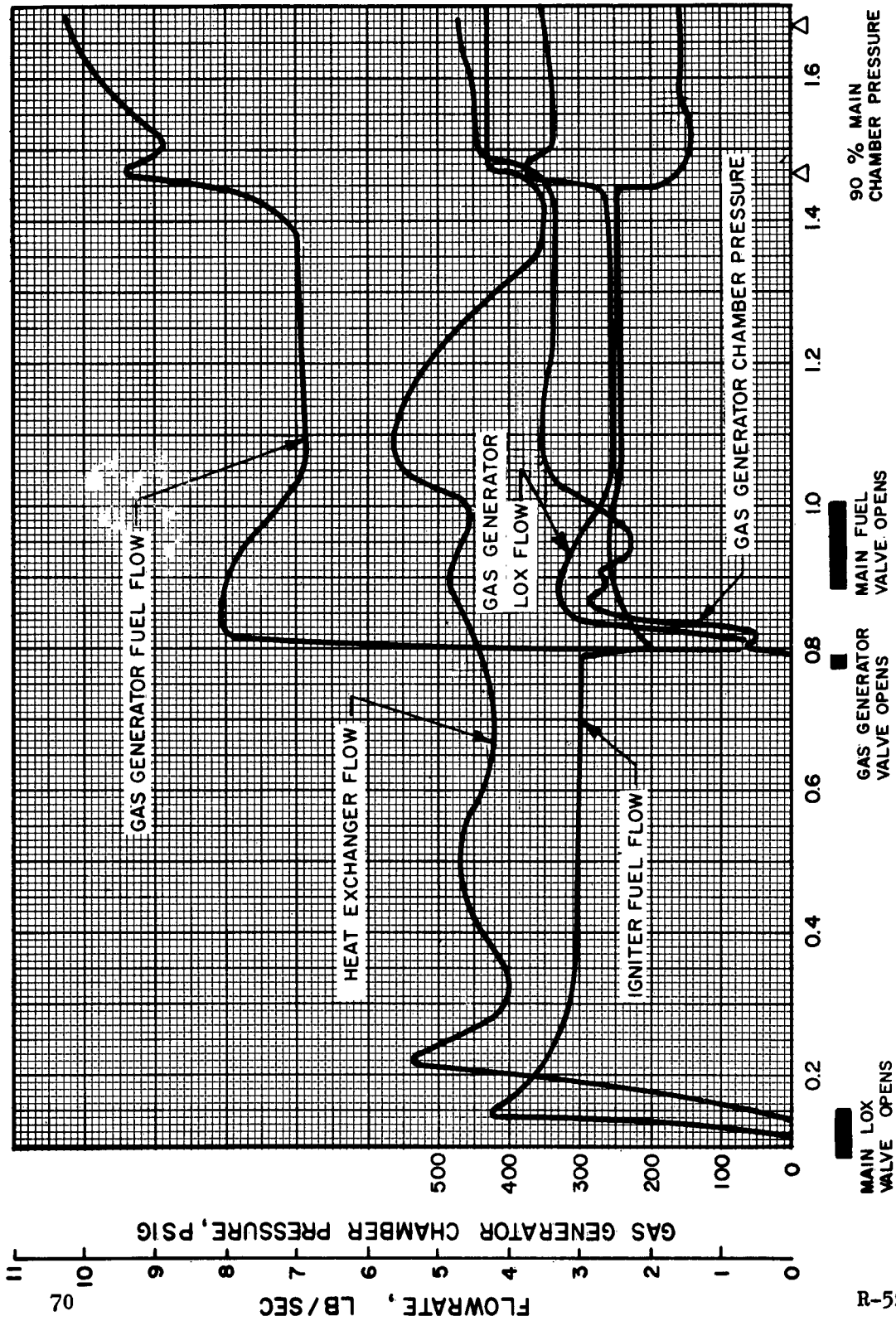


Figure 15. Main Engine System Start Characteristics



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TIME FROM IGNITION START, SECONDS

Figure 16. Gas Generator and Auxiliary Flows Start Characteristics

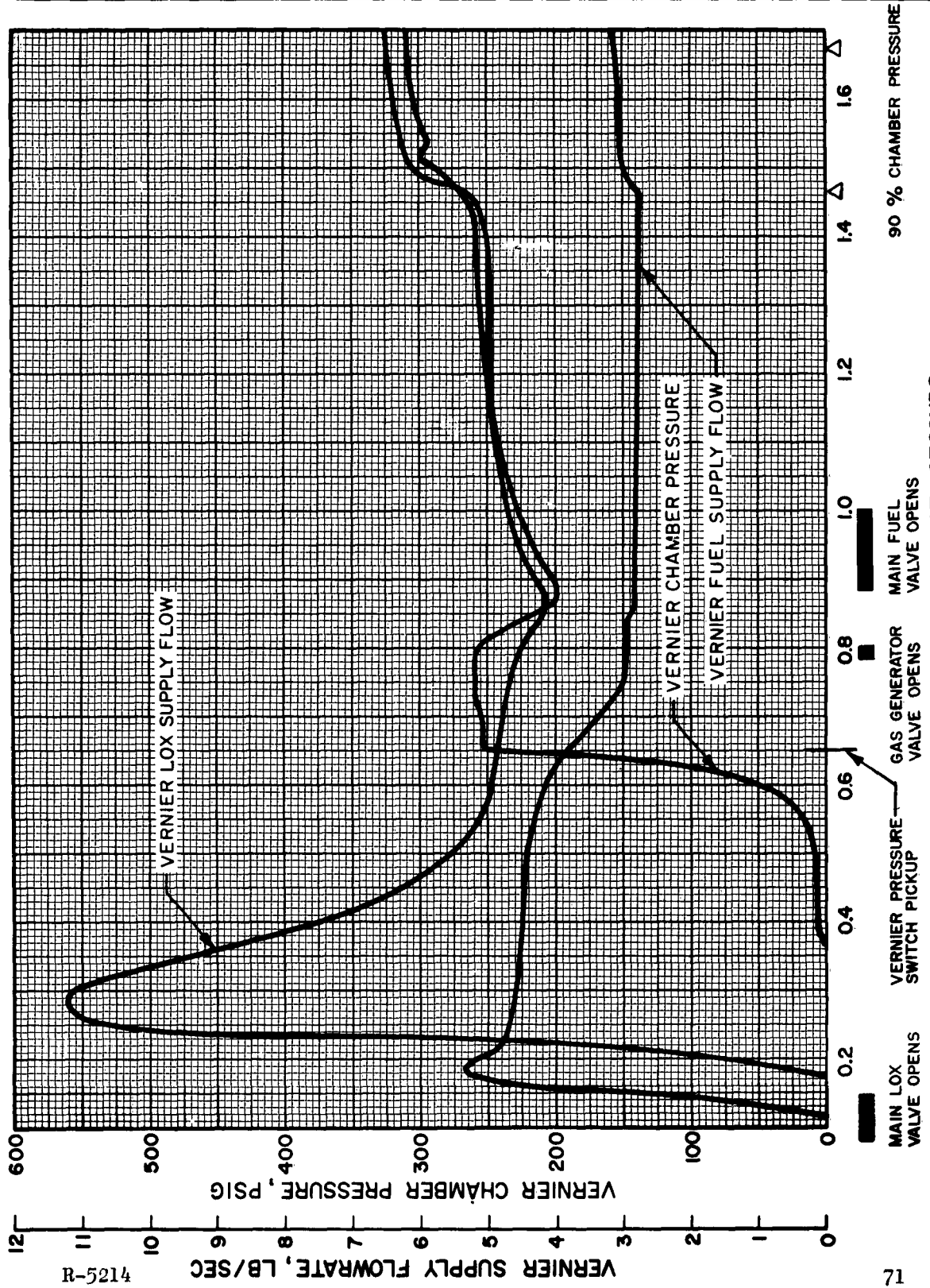
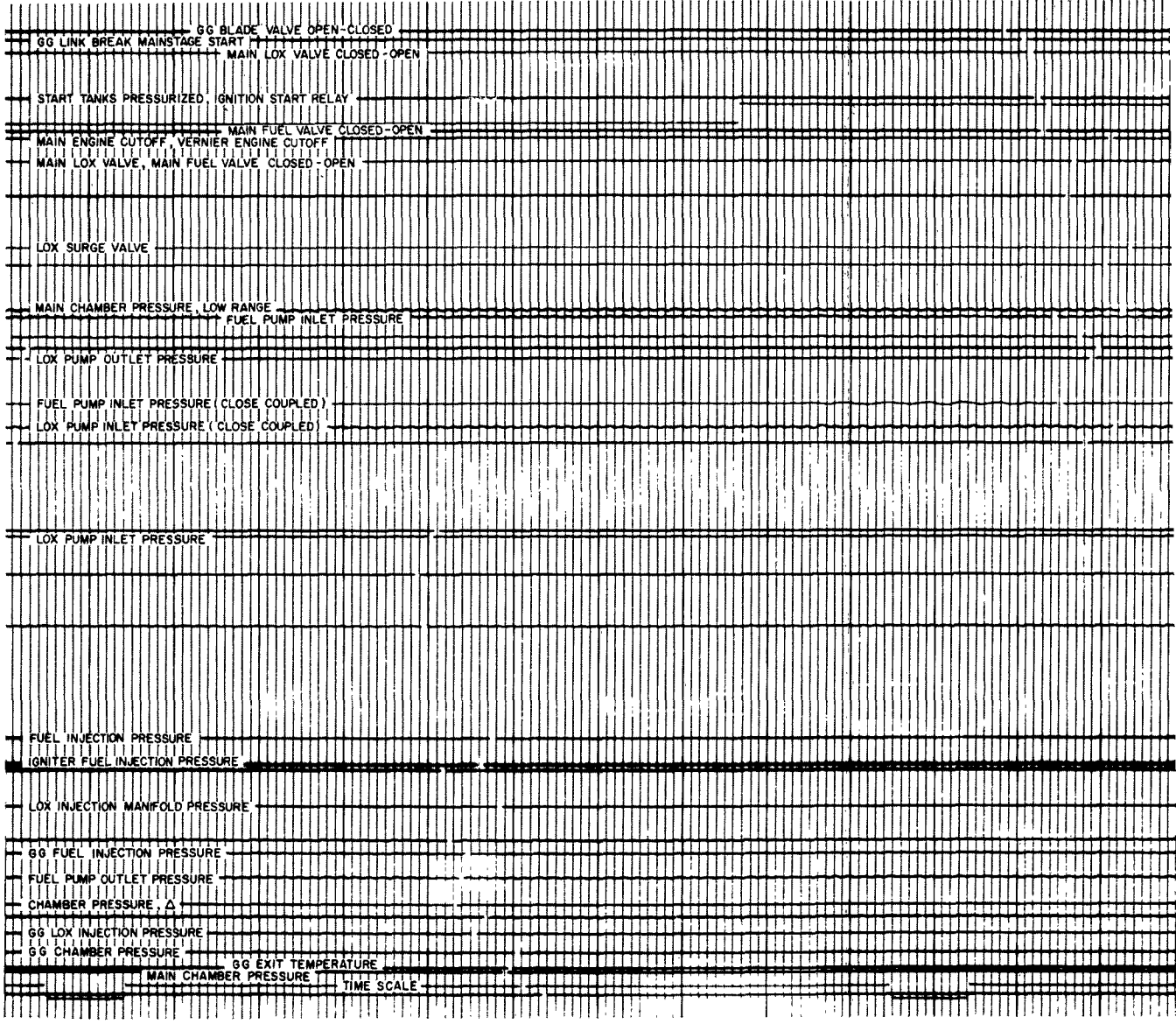
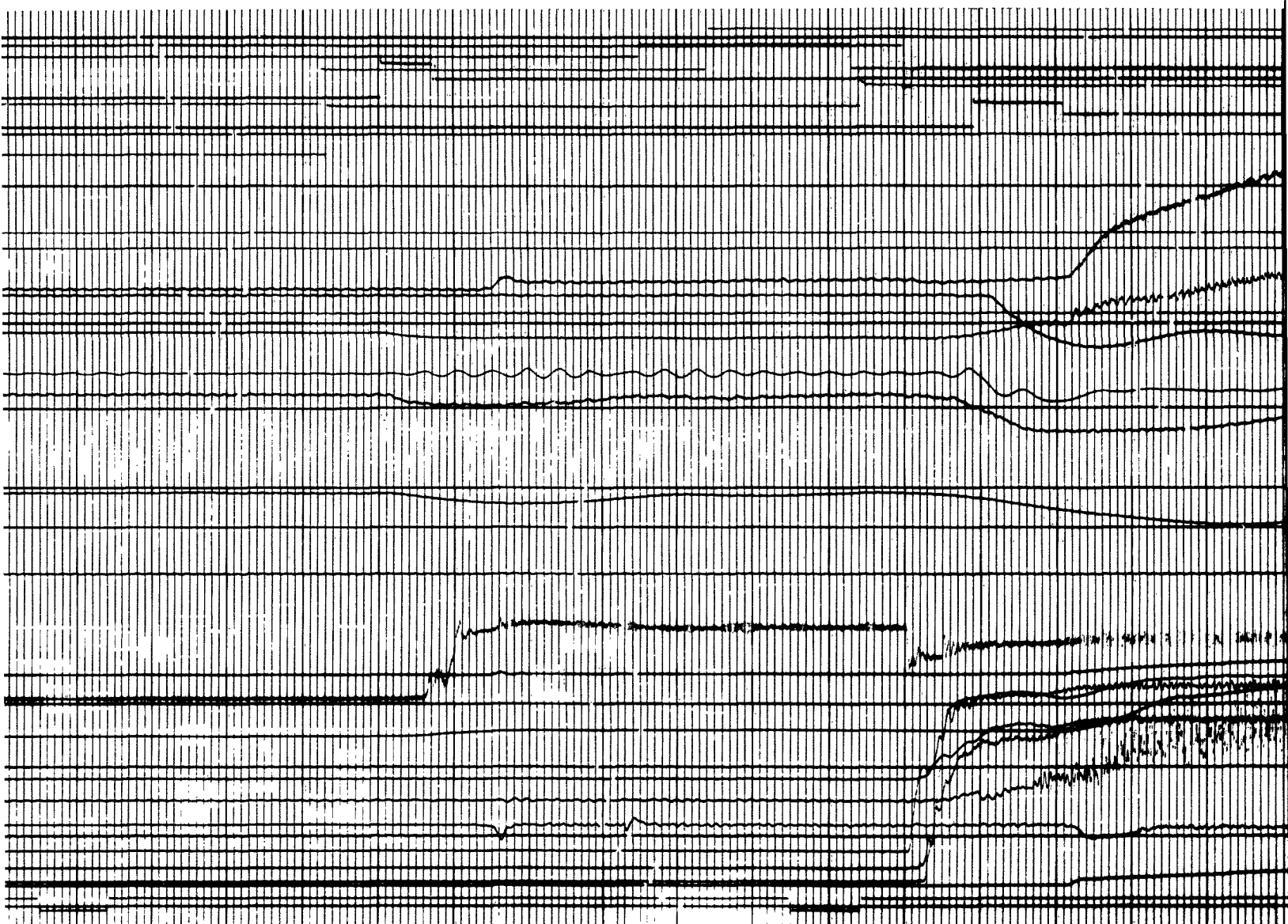


Figure 17. Vernier System Start Characteristics

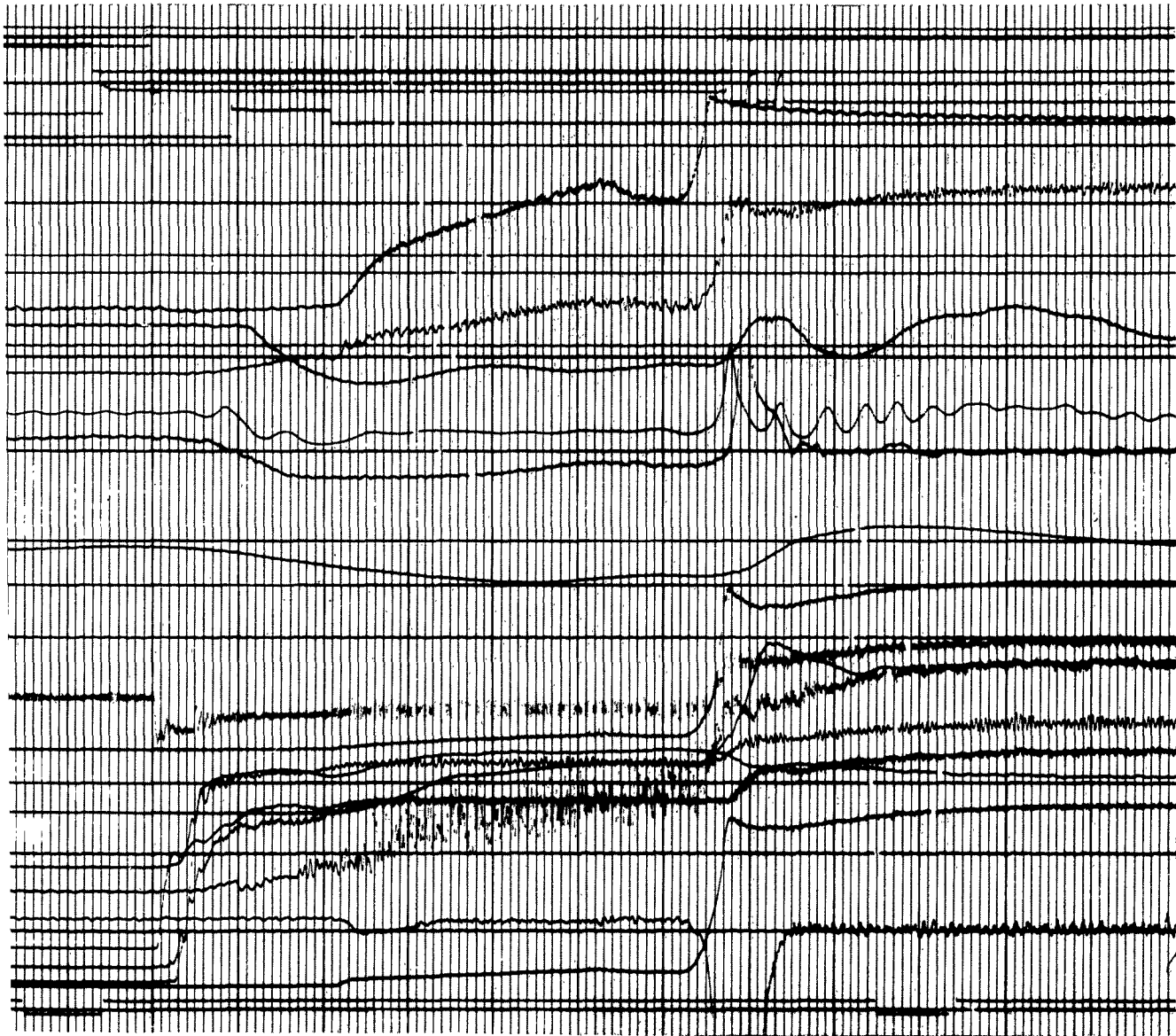


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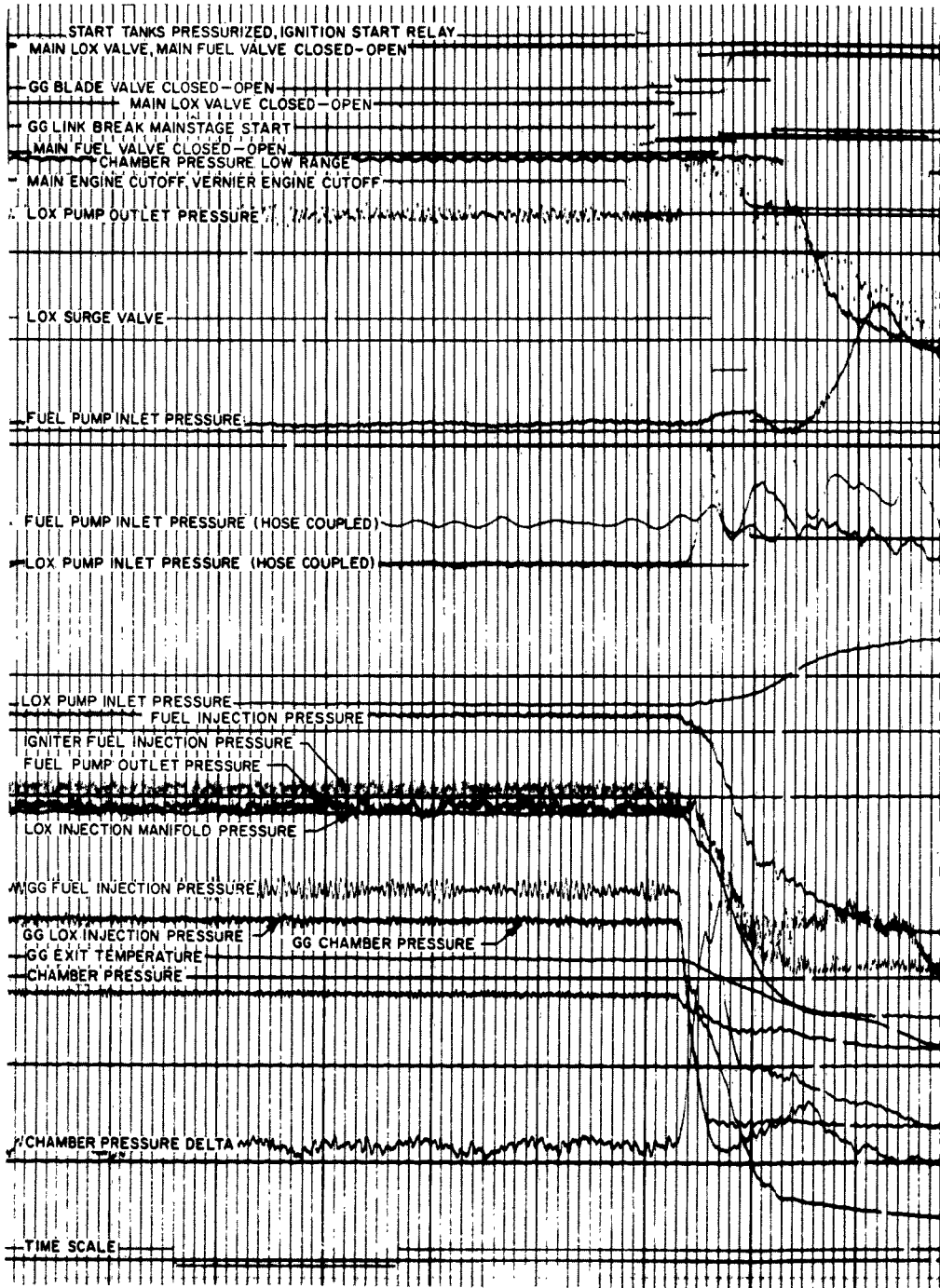
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3

Figure 18 . Main Engine Typical Start
Oscillographic Recording

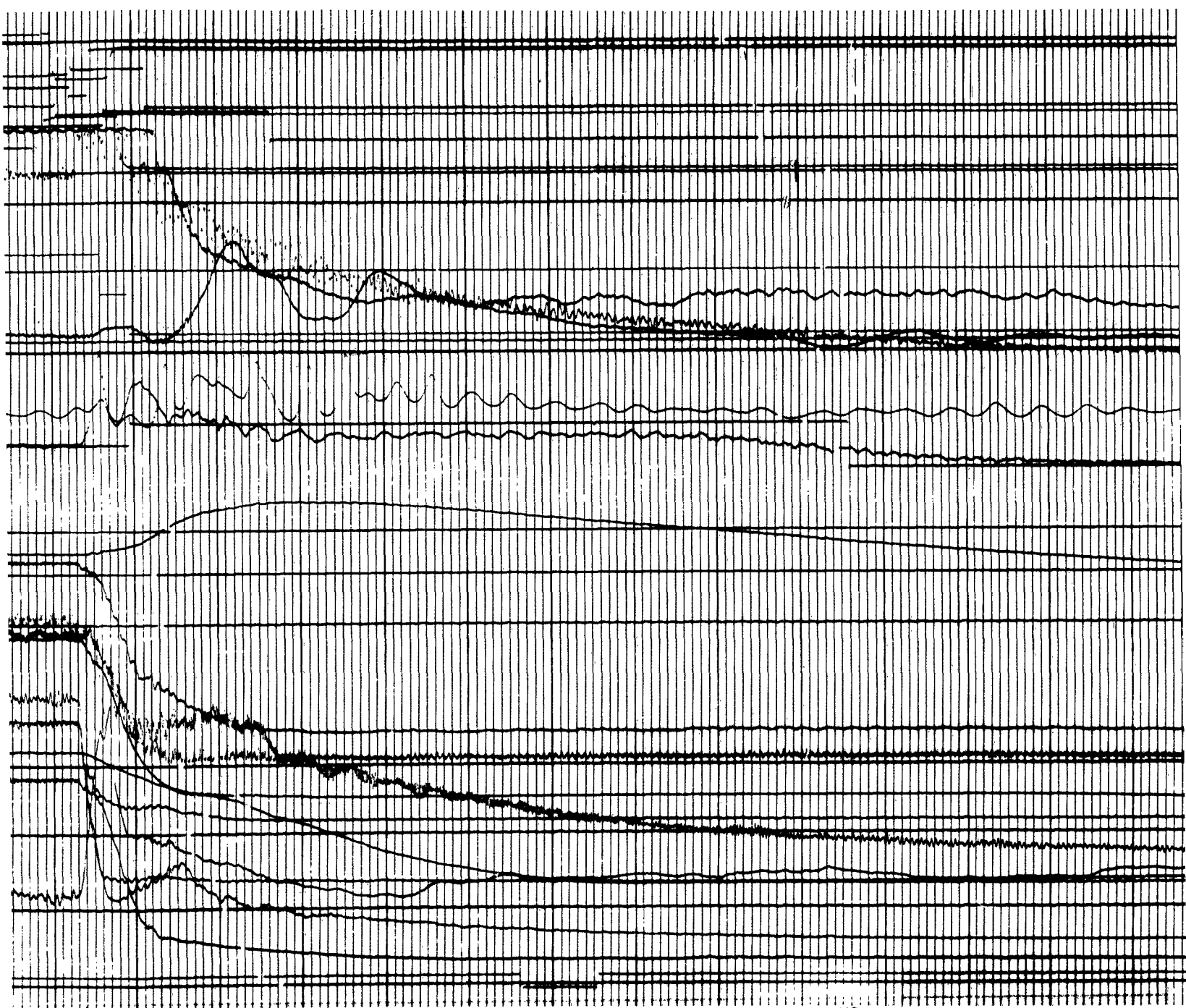
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Figure 19 . Main Engine Typical Cutoff
Oscillographic Recording

ROCKETDYNE
A DIVISION OF NORTH AMERICAN AVIATION, INC.

TABLE 10

PRELAUNCH PROPELLANT CONSUMPTION*

| System | Propellant | |
|------------------|-------------|--------------|
| | LOX, pounds | Fuel, pounds |
| Vernier | 6.17 | 4.52 |
| Gas Generator | 1.94 | 5.38 |
| Ignition | -- | 3.12 |
| Total Start Tank | 8.11 | 13.02 |
| Heat Exchanger | 6.53 | |
| Main Chamber | 305 | 130 |

*Based on static test performance with 15 to 30
minute LOX chilldown

TABLE 11

START TANK REFILL CHARACTERISTICS

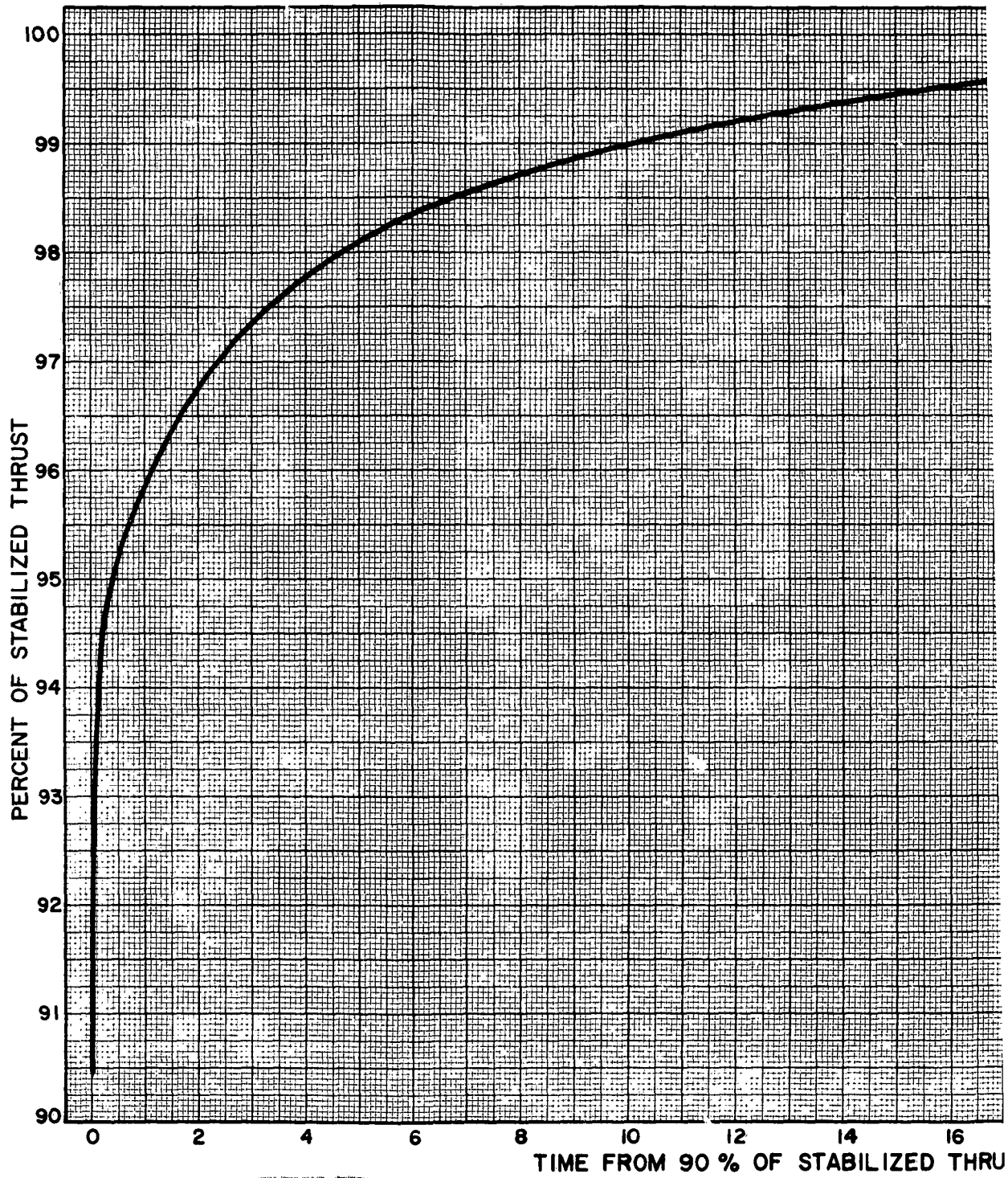
| Start Tank | Normal Test Stand Start | | Missile Simulated Start | | Overboard Flowrate, lb/sec |
|------------|-------------------------|---------------------|-------------------------|---------------------|----------------------------|
| | Refill Time*, seconds | Refill Rate, lb/sec | Refill Time*, seconds | Refill Rate, lb/sec | |
| Oxidizer | 22 | 0.37 | 50 | 0.19 | 0.20 |
| Fuel | 60 | 0.20 | 60 | 0.20 | 0.02 |

*Time from 90% chamber pressure to refill indication

STABILIZATION CHARACTERISTICS

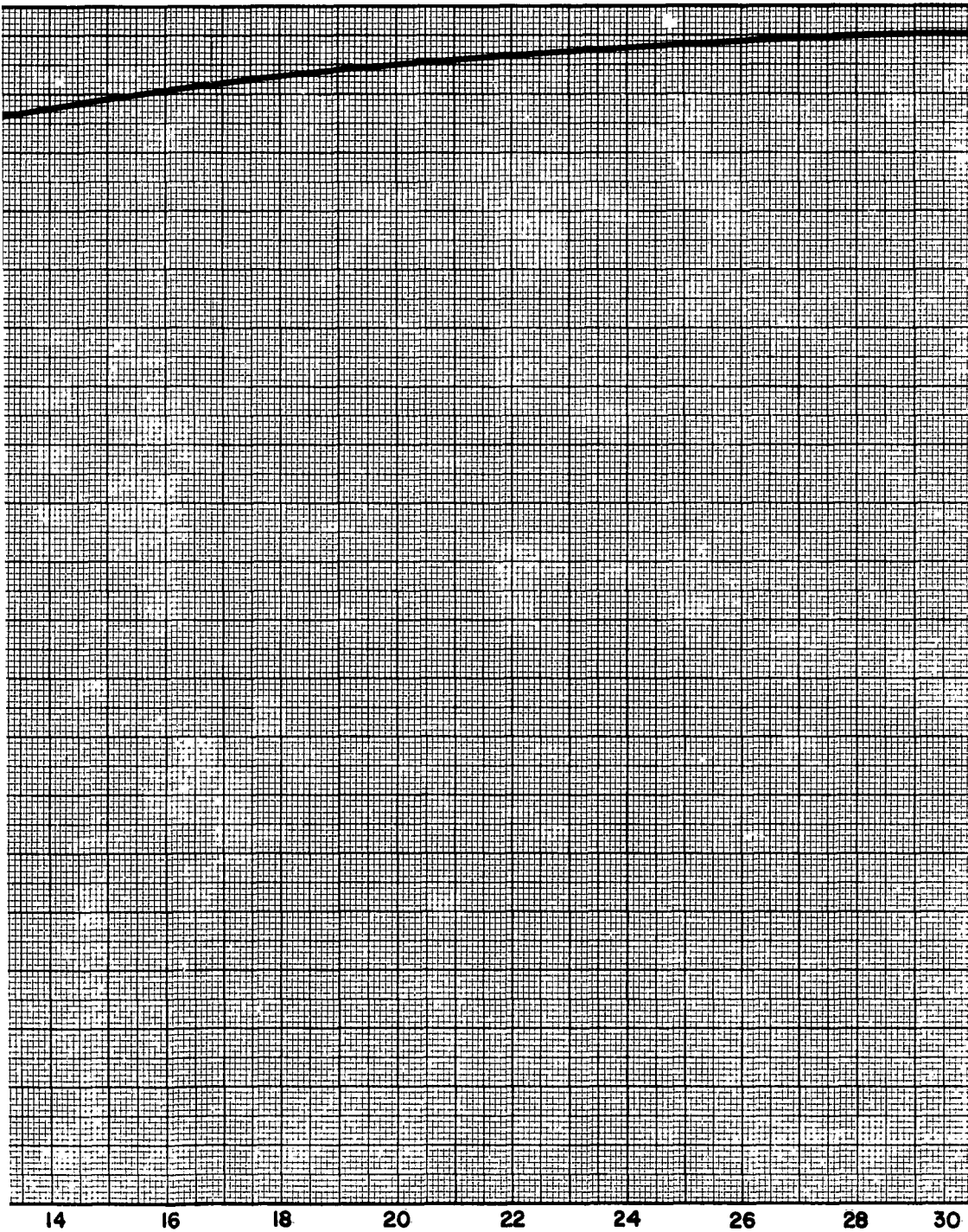
Gradual stabilizing of pressure-flow parameters under self-sustained operating conditions (bootstrapped power package) is a characteristic of liquid propellant engines with orificed control of gas generator propellant supply flows. The main engine generally attains stabilized operation 30 seconds from 90%. Varying test conditions and random engine hardware influences can, however, result in stabilization times ranging from 15 to 35 seconds from 90%.

The average thrust buildup from 90% to stabilized operation is shown in Fig. 20. Figures 21 through 23 present typical pump, chamber, and auxiliary systems stabilization characteristics (including vernier engines). The test from which the latter relationships were obtained stabilized in 20 seconds, which is not an abnormal condition.



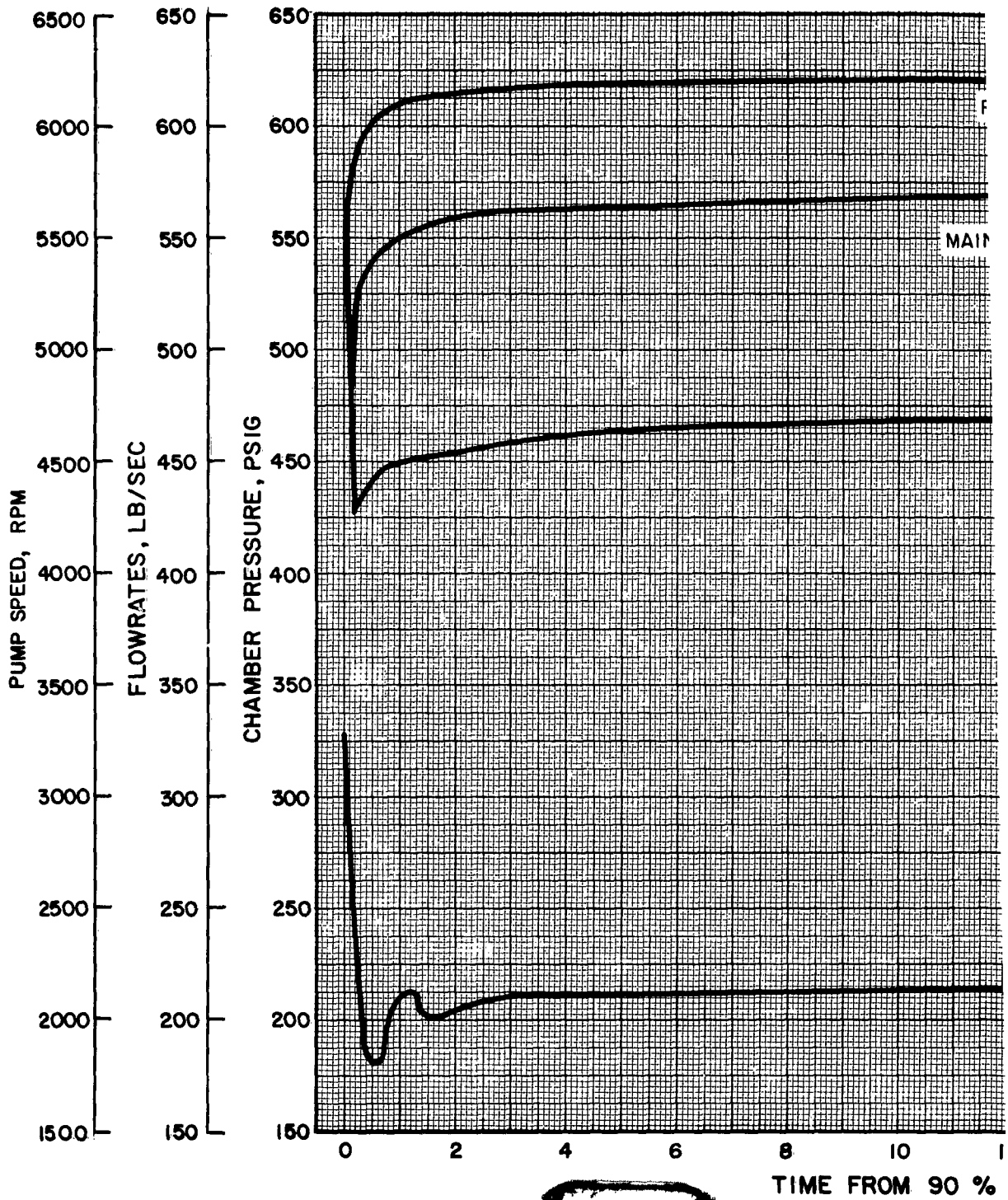
FORM R 18-G-18





14 16 18 20 22 24 26 28 30
STABILIZED THRUST, SECONDS

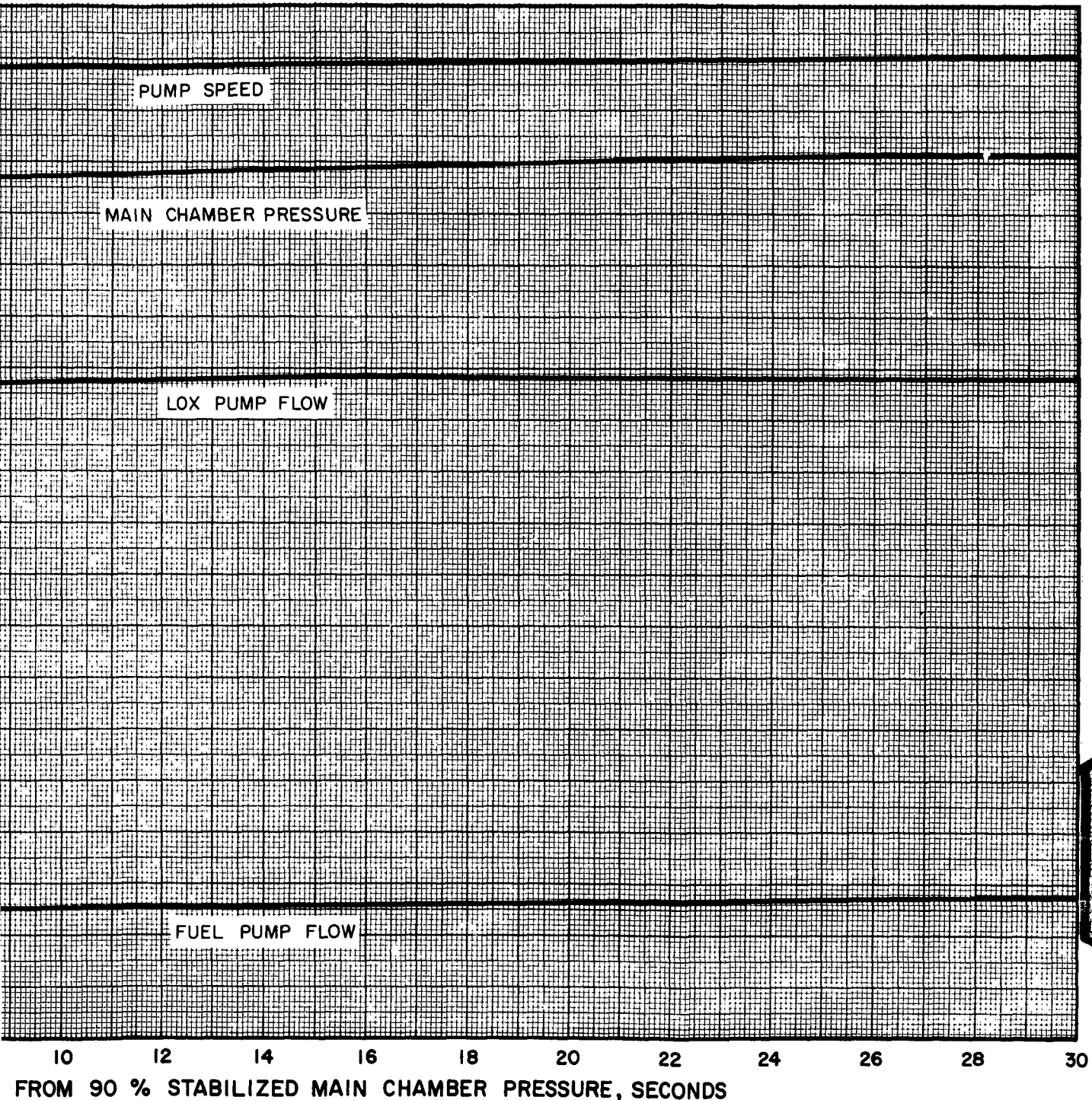
Figure 20. Main Engine Thrust Stabilization Characteristics



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Figure 21. Main Engine System Stabilization Characteristics

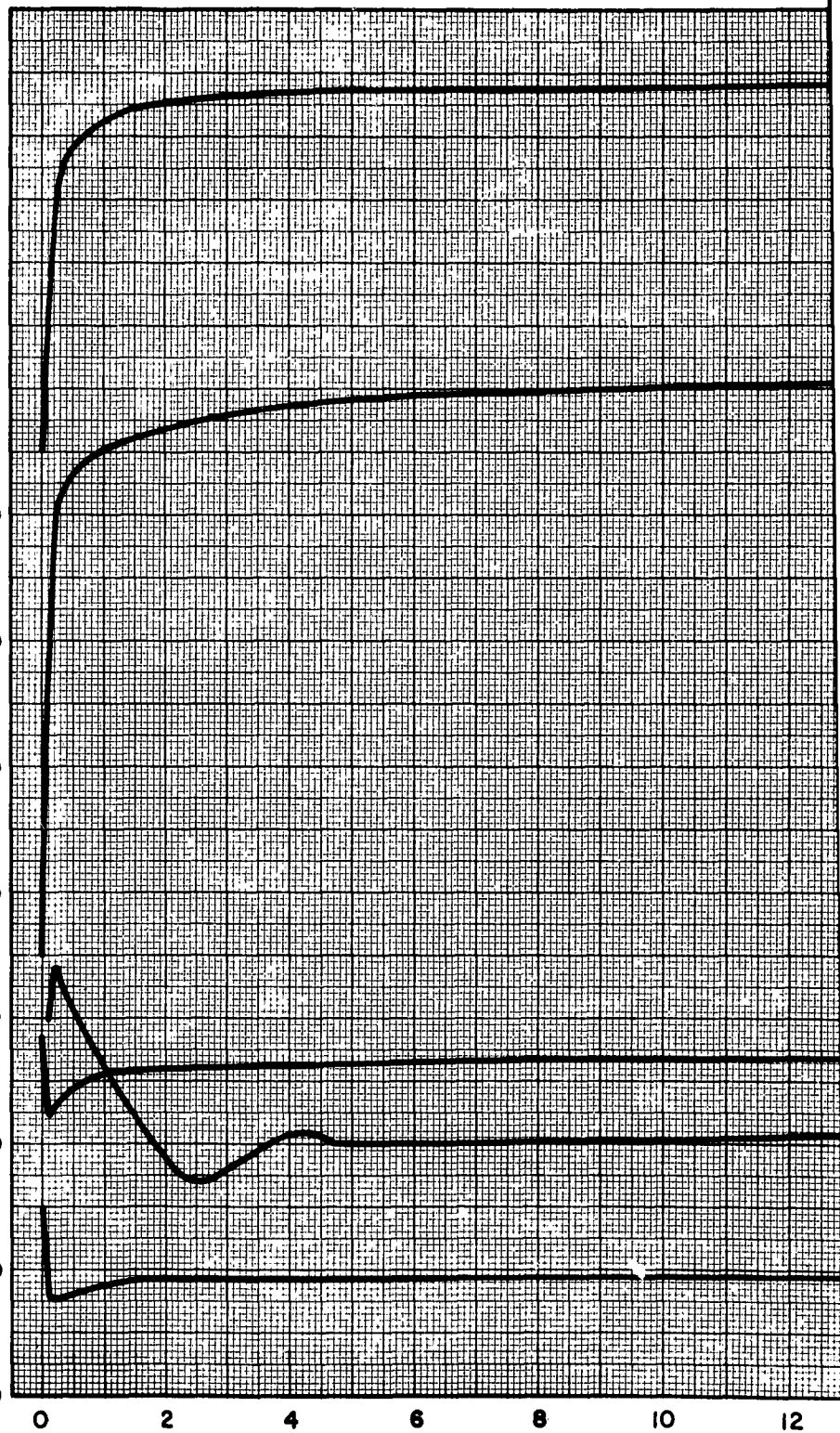


FLOWRATES, LB/SEC

12
11
10
9
8
7
6
5
4
3
2
1

PRESSURE, PSIG

520
480
440
400
360
320
280
240
200



TIME FROM 90% MA

GAS GENERATOR FUEL FLOW

GAS GENERATOR CHAMBER PRESSURE

GAS GENERATOR LOX FLOW

HEAT EXCHANGER LOX FLOW

IGNITER FUEL FLOW

10 12 14 16 18 20 22 24 26 28 30

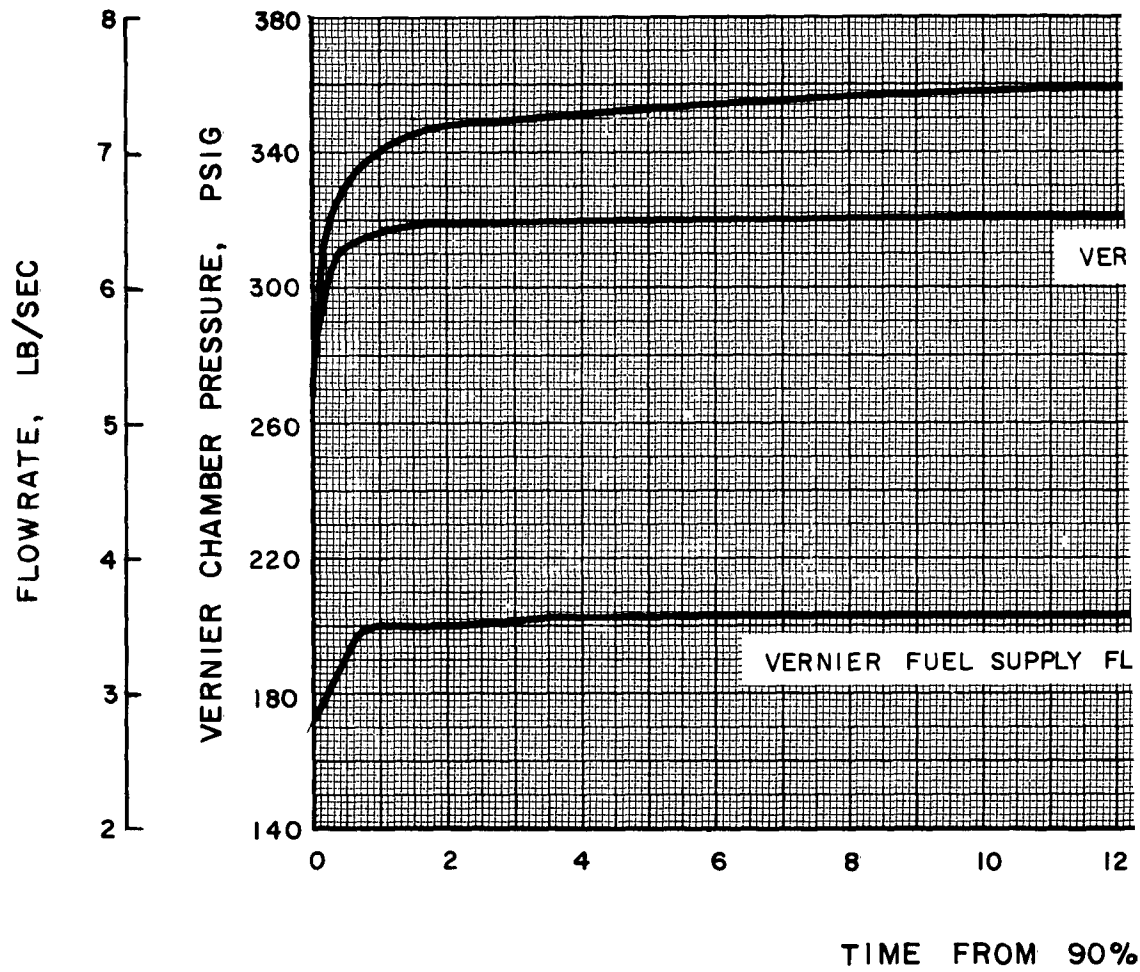
FROM 90% MAIN CHAMBER PRESSURE, ~ SECONDS

Figure 22. Gas Generator and Auxiliary Flows
Stabilization Characteristics

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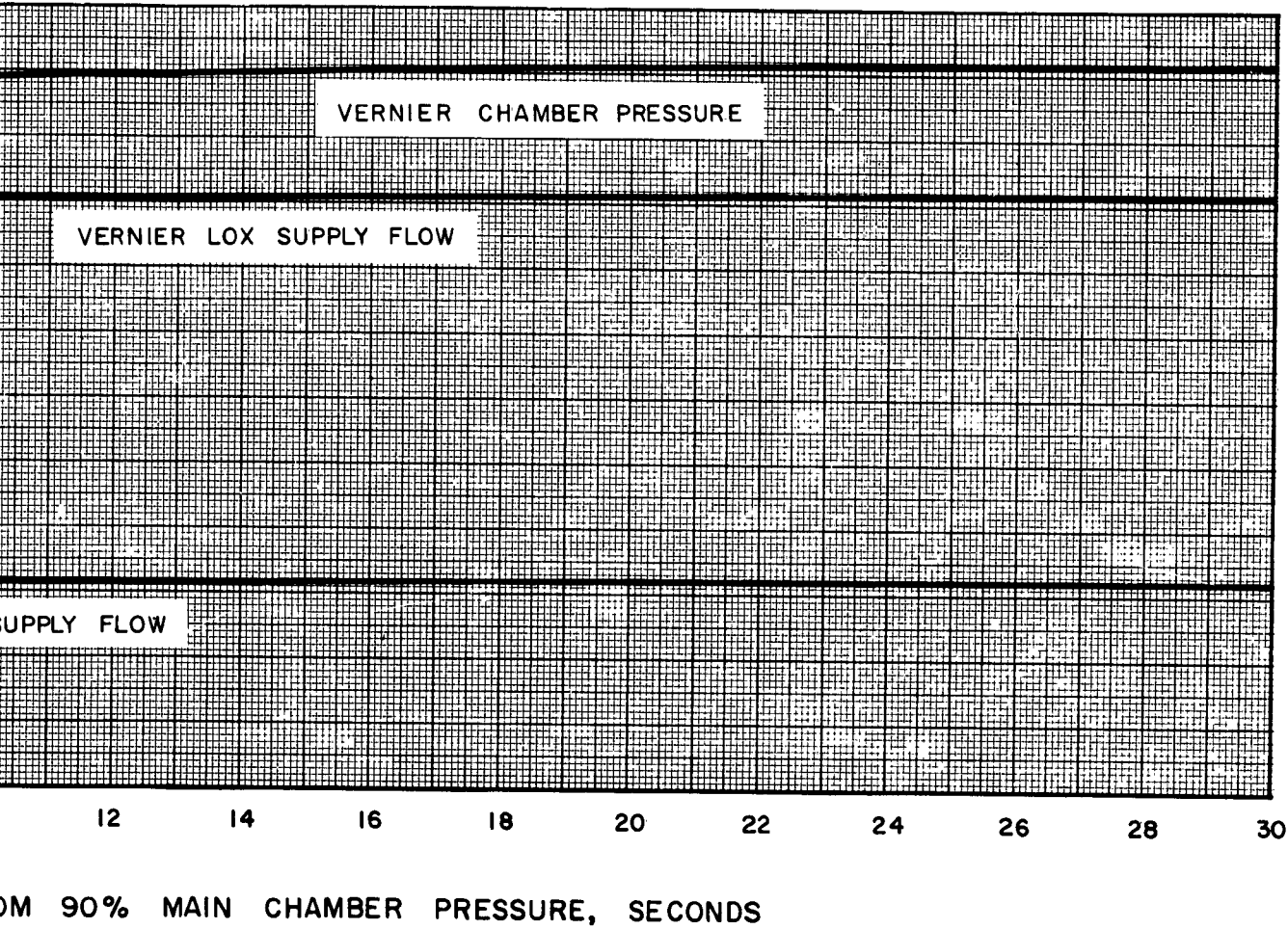


Figure 23. Vernier System Stabilization Characteristics